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A THREE-DIMENSIONAL SOLUTION OF FLOWS OVER WINGS WITH LEADING-EDGE VORTEX SEPARATION PARTIL

Program Description Document

Ronald G. Coleman, Forrester T. Johnson, and Paul Lu

September 1975

Prepared under contracts NAS1-12185 and NAS1-13833 by Boeing Commercial Airplane Company P.O. Box 3707 Seattle, Washington 98124

Langley Research Center
NATIONAL AERONAUTICS AND SPACE ADMINISTRATION

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NASA CR-132710	2. Government Accession No.	3. Recipient's Catalog No.
	OLUTION OF FLOWS OVER	5. Report Date September 1975
WINGS WITH LEADING-ED Part II—Program Description	6. Performing Organization Code	
Ronald G. Coleman, Forreste	r T. Johnson, and Paul Lu	8. Performing Organization Report No. D6-41789
9 Performing Organization Name and Address Boeing Commercial Airplane	10. Work Unit No	
P.O. Box 3707 Seattle, Washington 98124	11. Contract or Grant No. NAS1-12185, NAS1-13833	
12. Sponsor ag Agency Name and Address National Aeronautics and Space Administration		13. Type of Report and Period Covered Contractor Report May 1973 — June 1975
Washington D.C. 20546		14. Sponsoring Agency Code

15. Supplementary Notes

16. Abstract

A method of predicting forces, moments, and detailed surface pressures on thin, sharp-edged wings with leading-edge vortex separation in incompressible flow is presented. The method employs an inviscid, incompressible flow model in which the wing and the rolled-up vortex sheets are represented by piecewise continuous quadratic doublet sheet distributions. The Kutta condition is imposed on all wing edges.

Computed results were compared to experimental data and with the predictions of the leading-edge suction analogy for a selected number of wing planforms over a wide range of angle of attack. These comparisons show the method to be very promising, capable of producing not only force predictions but also accurate predictions of detailed surface pressure distributions, loads, and moments.

Experience with the present computer program, however, is limited, and operational limitations related to doublet panel spacing and panel density requirements, behavior at large planform breaks, convergence characteristics, etc., have yet to be extensively explored.

17. Key Words (Suggested by Author(s)*) Doublet singularity Incompressible Iteration Leading edge	Nonlinear Panel method Potential flow Three-dimensional Separation	18. Distribution Statem Unclassified		
19. Security Classif. (of this report) Unclassified	20. Security Classif. (Unclassifie	. •	21. No. of Pages 182	22. Price'

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A THREE-DIMENSIONAL SOLUTION OF FLOWS OVER WINGS WITH LEADING-EDGE VORTEX SEPARATION Part II—Program Description Document

Ronald G. Coleman, Forrester T. Johnson, and Paul Lu Boeing Commercial Airplane Company

SUMMARY

A computer program has been developed for the solution of the subsonic, three-dimensional flow over wings with leading-edge vortex separation. The documentation is divided into two volumes, Part I and Part II.

This volume is Part II of the documentation containing the description of the computer program. It consists of three sections presenting the Program Logic, the Description of Subroutines, and the Program Listing.

INTRODUCTION

A computer program has been developed for the solution of the subsonic, three-dimensional flow over wings with leading-edge vortex separation (ref. 1). The program provides capabilities for calculating forces, moments, and detailed surface pressures on thin, sharp-edged wings of an arbitrary planform. The wing geometry is arbitrary in the sense that leading and trailing edges may be curved or kinked and the wing may have arbitrary camber and twist. The computer program includes a recently developed potential flow computational technique based on the advanced aerodynamic panel method (ref. 2). The numerical method employs an inviscid flow model in which the wing and the rolled-up vortex sheets are represented by piecewise continuous quadratic doublet sheet distribution. The Kutta condition is imposed along all wing edges. An iterative scheme is applied to find the strengths of the doublet distributions as well as shape and position of the free vortex sheet spirals satisfying the nonlinear boundary conditions of the flow problem.

The computer program is written in FORTRAN IV for a SCOPE 3.0 or KRONOS 2.1 operating system of the CDC 6400/6600 computer. The program uses overlay structure and eight disk files (including input and output files), and it requires approximately 120 000 (Octal) central memory words. This program has been designed with the primary objective of verifying new concepts and ideas.

The documentation of the program is divided into two parts:

Part I: Engineering Document

Part II: Program Description Document

The Engineering Document (bound separately) contains a detailed description of the theoretical method and, in particular, a thorough discussion of the following items: flow model as a nonlinear boundary value problem, geometry definition, numerical method, solution procedure, and verification of the method. A user's guide of the computer program is also included in the Engineering Document.

This volume, the Program Description Document, consists of three sections:

- Program logic describing the basic program structure and listing the names of overlay programs and all subroutines. It includes descriptions and flowcharts of overlay programs, along with a discussion of file usages and common blocks.
- 2: Purpose, input and output, and a brief discussion of processing performed by the routine for all subroutines.
- 3: A complete program listing.

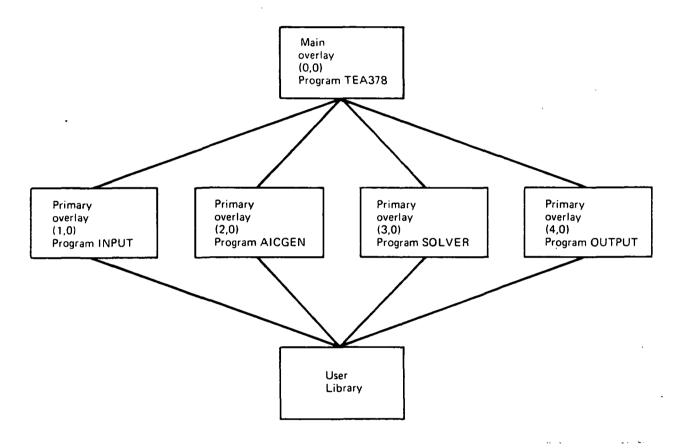
The Program Description Document is written for the purpose of maintaining an experimental-type computer program.

PROGRAM LOGIC

BASIC PROGRAM STRUCTURE

The computer program consists of one main overlay, four primary overlays, and one user library. A description and flowchart of each overlay program are given.

The flowchart of main overlay program TEA378 illustrates the overall functions the program performs. A schematic diagram of basic program structure follows:



NAMES OF PROGRAMS AND SUBROUTINES

The names of programs and subroutines used in each overlay and of those routines included in the user library are given as follows:

Main

OVERLAY(VORTEX,0,0)

Program

TEA378

Subroutines

ITFLOW, FUNC, FGCAL, UPDATE, AJGEN, DFGMU, DFGDT

Primary

OVERLAY(VORTEX,1,0)

Program

INPUT

Subroutines

DWNET, AWNET, GWNET, SWEPTE, SHEGEN

Primary

OVERLAY(VORTEX,2,0)

Program

AICGEN

Subroutines

EDGEIN, KSORT, TGEOMC, GEOMC, SURFIT, TSING, SING, LSQSF, TCNTRL, CONTRL, SURPRO, VINFCC, EIVC, PIVC, GCPCAL, GRDIND, PIDENT, CCAL, ECAL, DPIV, FKCAL, FMNCAL, FNKCAL, INTCAL, SIDECL

Primary

OVERLAY(VORTEX,3,0)

Program

SOLVER

Primary

OVERLAY(VORTEX,4,0)

Program

OUTPUT

Subroutines

SNGCAL, SINFCC

User Library Subroutines IPTRNS, PTRNS, TRNSFR, TRANS, ZERO, CROSS, UVECT, MMULT, CMAB, LINEQS, TDECOM, BSUBSM, PDSEQS, VIP, VIPA,

VIPS

DESCRIPTION AND FLOWCHART OF OVERLAY PROGRAMS

Main

OVERLAY(VORTEX,0,0)

Program

TEA378

Purpose

To call various overlays to perform the following tasks:

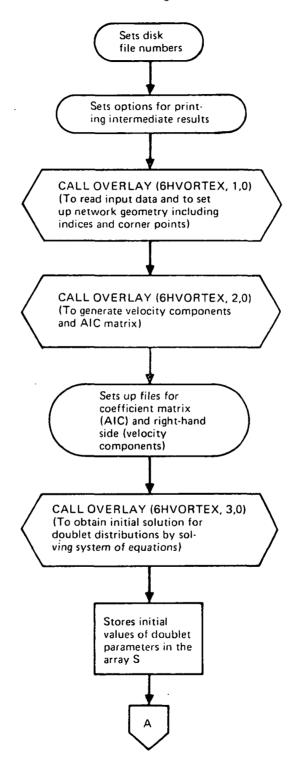
- Reading the input data and setting up geometry definition
- Generating the AIC matrix using an advanced panel-type method
- Solving a system of equations with the generated AIC to obtain initial doublet distributions
- Using the routine ITFLOW to find an iterative solution to the flow problem with nonlinear boundary conditions

Subroutines Called INPUT(OVERLAY-1,0), AICGEN(OVERLAY-2,0), SOLVER (OVERLAY-3,0), OUTPUT(OVERLAY-4,0), ITFLOW

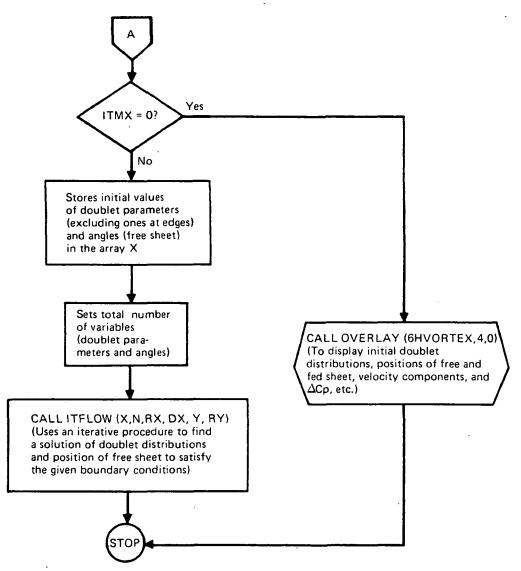
Discussion

Program TEA378 is the main overlay. It sets disk file numbers and options for printing intermediate results. The printing options are for checkout purposes. First the program calls INPUT to read input data cards and to set up network panel corner points, including an initial guess for the shape and position of free sheet. Then AICGEN is called to generate velocity components and AIC matrix using a panel-type influence coefficients method (see description of program AICGEN). An initial guess for doublet distributions is obtained by calling SOLVER to solve a system of equations with the generated velocity components and AIC matrix.

Flowchart of Program TEA378



Flowchart of Program TEA378 (Continued)



If the user sets the number of iterations to zero in order to check the input data, initial guesses for doublet distributions, and position of free sheet, the program will call OUTPUT to display initial doublet distributions, positions of free sheet and fed sheet, velocity components, Δc_p , etc. Otherwise, the program proceeds to call the subroutine ITFLOW to find a solution for doublet distributions and the position of free sheet to satisfy the nonlinear boundary conditions.

Primary

OVERLAY(VORTEX,1,0)

Program

INPUT

Purpose

To read and print user input data, calculate freestream velocity, calculate all panel corner point coordinates, calculate the initial length and angle of inclination of panels in the Free Vortex and Fed Sheet networks.

Input

See Engineering Document—User's Guide

Output

Common block

/DAT3/-AR, NTR, XTR, MSP, YSP, NTC, NLE, YLE, NTE, YTE, MSF

/FSVEL/-FSV, FSVM, ALPHA, XPITCH, RCHORD

/INDEX/-NT, NM, NN, NP, NZ, NPA, NZA, NNETT, NPANT, NZMPT

/MSPNTS/-ZM, ZL

/SOLN/-ZA

Subroutines Called AWNET, DWNET, GWNET, SHEGEN

_ .

Discussion

c is set equal to the cosine of the angle of attack in radians, and s is set equal to the sine. They form the components of a freestream velocity vector whose magnitude is calculated by taking the square root of the sum of the squares of c and s.

The wing panel corner points may be input by the user following a "\$INPUT WING NETWORK" data card or the program will calculate them following a "\$DELTA," "\$ARROW," or "\$GOTHIC WING PREPROCESSOR" data card.

Subroutine SHEGEN calculates the Y and Z coordinates of panel corner points on the Free Vortex and Fed Sheet networks. The distance between adjacent panel corner points on each transverse cut in the Free Vortex and Fed Sheet is calculated along with the panel inclination angle with respect to the flat wing.

Primary

OVERLAY(VORTEX,2,0)

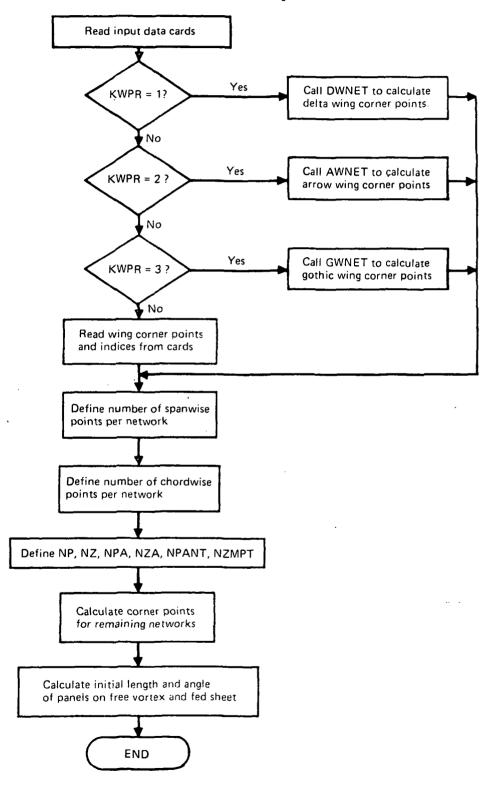
Program

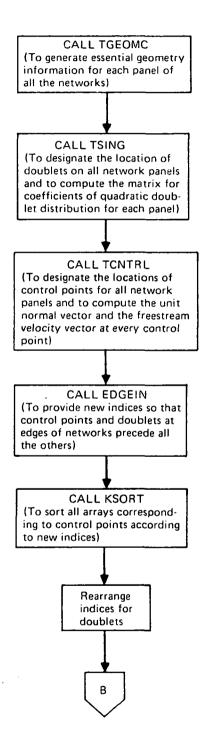
AICGEN

Purpose

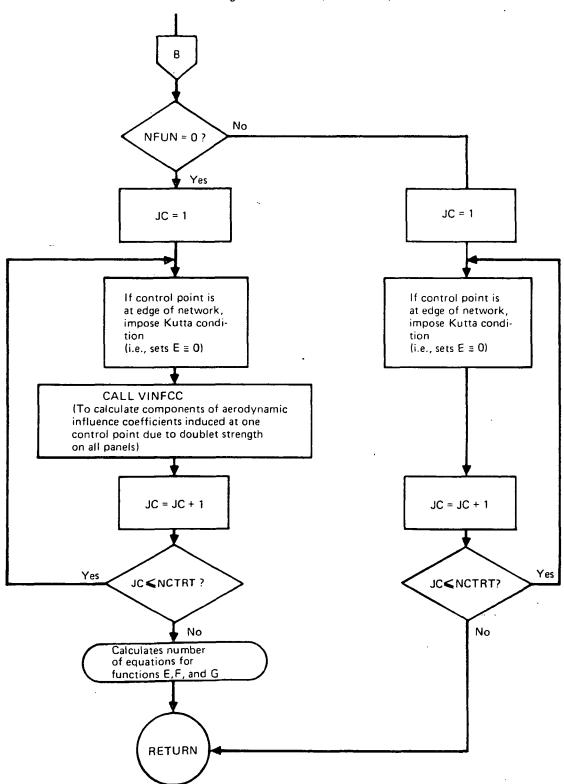
To calculate essential geometry information for each panel and the locations of doublets and control points for each network and to generate the aerodynamic influence coefficients using an advance panel-type method.

Flowchart of Program INPUT





Flowchart of Program AICGEN (Continued)



Input

Common block

/INDEX/-NT, NM, NN, NP, NZ, NPA, NZA, NNETT, NPANT, NZMPT

/NITF/-NFUN

/IPRINT/-IPGEOM, IPSING, IPCNTR, IPEIVC

Output

Common block

/CM03/-NPIF, NAIC3, NAIC

/BDYCS/-AC, ZCC, ZCR, ZDC, IPC, ITC

/INDEX/-NS, NC, NSA, NCA, NSNGT, NCTRT

/NINDX/-NEQ, NJC, ITC

Subroutines Called TGEOMC, TSING, TCNTRL, EDGEIN, KSORT, PTRNS, IPTRNS,

VINFCC, VIP

Discussion

The program first calls TGEOMC to provide least squares surface fit for each panel and to generate essential geometry information such as local coordinates of panel corner points and center, coordinate transformations, moments, etc. The subroutines TSING and TCNTRL are called to designate the locations of doublets and control points for each network according to different network types. The coefficients of quadratic doublet distribution for each panel are computed by using least squares method. The unit normal vector and the freestream velocity normal to the panel surface at each control point are also calculated.

As discussed in the Engineering Document, equation (46), the stream surface boundary condition at edge points of networks where the Kutta condition has to be satisfied, gives a linear relation between the set of doublets (μ_c) at the edges of the network and the set of all remaining doublets (μ_r). Hence, doublets μ_c can be expressed in terms of all remaining doublets μ_r , and only μ_r will have to be treated as the explicit unknown parameters in the iterative procedure. For the convenience of computation, indices of doublets are rearranged so that μ_c 's precede μ_r 's. Indices of control points are also rearranged in a similar way.

The components of aerodynamic influence coefficients (AIC) induced at each control point, due to doublet distributions of all panels, are computed by calling VINFCC. This process is repeated first for the control points at the edges of networks and then for all other control points. The program provides an option for skipping the last part of the computation. Thus, when subroutine ITFLOW in the main overlay calls AICGEN to update AIC at every KIT iteration, it sets NFUN=0, and the new AIC is generated. Otherwise, NFUN≠0 and the computation of new AIC is skipped.

Primary

OVERLAY(VORTEX,3,0)

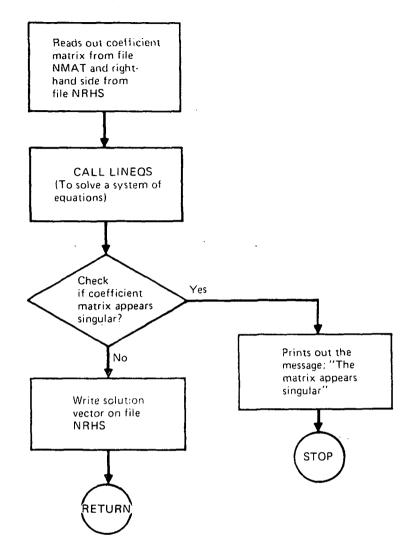
Program

SOLVER

Purpose

To solve a linear system of equations A·X=B

Flowchart of Program SOLVER



Input

Common block

/NEQS/-NE, NR, NMAT, NRHS

Output

Common block /NEQS/-NRHS

Subroutines Called LINEQS

Discussion

The program reads out coefficient matrix and right-hand side from two separate files and stores them in two different arrays A and B. The routine LINEQS is then called to solve the system of equations. If the coefficient matrix is not singular, the solution vector is written on the file that originally stores the right-hand side. Otherwise, an error message "The matrix appears singular" is printed, and execution of the computer program is terminated. The program has been set up with the consideration that an out-of-core equation solver can replace the present in-core one without changing the data structure significantly.

Primary

OVERLAY (VORTEX,4,0)

Program

OUTPUT

Purpose

To print the program results, including: circulation along terminated edge of the fed sheet network; circulation along the wing trailing edge; X, Y and Z coordinates of panel center, velocity on upper and lower surfaces, and Δc_p for each panel in the wing and free vortex networks; upper and lower c_p and area for each panel in the wing network; normal force coefficient; pitching moment coefficient; pitch axis x value; root chord length; and total wing area.

Input

Common Block /BDYCS/-ZC

/CM03/-NPIF, NAIC3 /FSVEL/-FSV,XPITCH /INDEX/-NM,NPA,NZA

/MSPNTS/-ZM

/NFAJ/-NEQ,NF,NG /PANDQ/-AR,ART,C

/SOLN/-S

Output

See Purpose

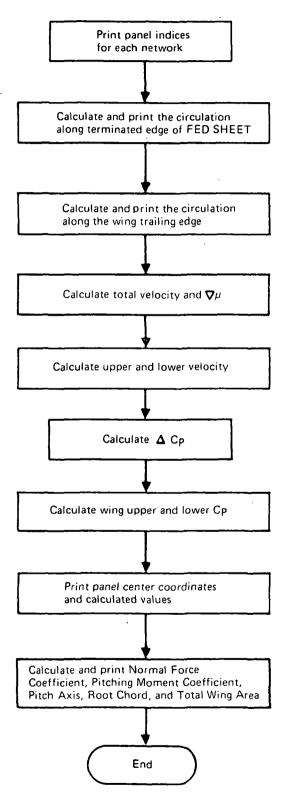
Subroutines Called MMULT, PTRNS, SNGCAL, UVECT, VIP

Discussion

The Fed Sheet terminated edge points are calculated as the midpoints between each pair of outboard Fed Sheet panel corner points. SNGCAL is called to calculate the circulation at each edge point.

The wing trailing-edge points are calculated as the midpoints between each pair of forward wake panel corner points. SNGCAL is again called to calculate the circulation at each point.

Flowchart of Program OUTPUT



The total velocity is calculated by multiplying the AIC matrix (DVDFS) by the vector, consisting of values S of doublet parameters and adding the components of the freestream velocity vector.

SNGCAL is called to calculate the value and 1st, 2nd derivatives of doublet strength at the panel center points of the wing and free sheet networks. The components of sheet vorticity (first derivatives of doublet strength) are transformed into the global panel system to define $\nabla \mu(\text{VELFS})$.

Upper and lower velocity is calculated by adding to and subtracting from the total velocity components, one-half of the $\nabla \mu$ components.

 $\Delta c_{\mathbf{p}}$ is calculated by multiplying two times the vector inner product of $\nabla \mu$ and the total velocity vector.

cp upper and lower for the wing network are calculated by the equation:

$$(VSQ \pm HDCP + 0.25*GMUSQ)$$

(1)

where VSQ is the velocity vector inner product, GMUSQ is the $\nabla \mu$ vector inner product, and HDCP is one-half of Δc_p .

The final calculations performed are for a summation table for the wing network consisting of normal force coefficient (c_N) , pitching moment coefficient (c_m) , pitch axis X value (XPITCH), root chord length (RCHORD) and total wing area (SW). The product (CNF) of the normal vector, Δ c_p , and wing panel area is used to calculate c_N and c_m .

 c_N is defined as two times the sum of CNF at each wing panel divided by the total wing area.

c_m is defined as two times the sum of CNF at each wing panel times the X of the panel center minus XPITCH, divided by RCHORD times total wing area.

XPITCH is the X value of the pitch axis input by the user.

RCHORD is defined as the X value where the trailing edge breaks away from the planform centerline minus the X value of the first transverse cut.

Total wing area is simply the sum of the individual wing panel areas contained in array C in common block PANDQ.

FILE USAGE

There are eight disk files used in the computer program. The files are passed through common block /CM03/. Their disk numbers are assigned in program TEA378 (Main Overlay). Files NTSIN and NTSOUT are the standard input and output files. The following illustration gives where and how the other six files are used.

File	Where	Usage
NTGD	TEA378	Writing on components of freestream velocity at control points; reading out initial values of doublet parameters
	ITFLOW	Writing on residuals; reading out corrections
	DFGMU	Writing on $\partial G/\partial \mu_e$ and $\partial G/\partial \mu_r$
	DFGDT	Writing on $\partial G/\partial \theta$
	AICGEN	Transferring panel information
NPIF	FGCAL	Reading out panel information
	DFGMU	Reading out panel information
	DFGDT	Reading out panel information
	AICGEN	Storing panel information
	VINFCC	Reading out panel information
	OUTPUT	Reading out panel information
NAIC3	FGCAL	Reading out components of influence coefficient
	DFGMU	Reading out components of influence coefficient
	AICGEN	Storing components of influence coefficient
	OUTPUT	Reading out components of influence coefficient
NAIC	FGCAL	Reading out rows of AIC matrix
	AICGEN	Storing rows of AIC matrix
NJAC	ITFLOW	Reading out rows of Jacobian
	DFGMU	Writing on $\partial F/\partial \mu_{P}$ and $\partial F/\partial \mu_{r}$
	DFGDT	Storing rows of Jacobian
NSCR	ITFLOW	Writing on rows of updated Jacobian
	DFGMU	Writing on partial derivatives with respect to doublet parameters
	DFGDT	Reading out partial derivatives with respect to doublet parameters

COMMON BLOCK DEFINITION

Variables of the more essential common blocks shared by main and primary overlays and some subroutines are defined below.

Common			
Block	Variables	Description	Where Set
ADR	RTD	Number of degrees in 1 rad	TEA378
	DTR	Number of radians in 1 deg	
BDYCS	ZC	Array of X,Y,Z coordinates of control points	TCNTRL
	ZCC	Array of normal vectors at control points on the panel surface	
	ZCR	Array of components of freestream velocity normal to the panel surface at control points	
	ZDC	Array of perturbation distances for control points at edges of networks	
	IPC	Array of panel indices for control points	
	ITC	Array of codes (= 1 for control points at edges of networks; =0 otherwise)	
CM03		See file usage	TEA378
DAT3	AR	Aspect ratio	INPUT
	NTR	Number of transverse cuts	
	XTR	Array of transverse cut x values	
	MSP	Number of spanwise wing percent values	
	YSP	Array of spanwise wing percent values	
	NTC	Number of transverse cuts intersecting root chord	
	NLE	Number of points defining wing leading edge	
	YLE	Array of Y coordinates of leading-edge points	

Common Block	Variables	Description	Where Set
	NTE	Number of wing trailing-edge, transverse-cut intersections	
	YTE	Array of Y coordinates of points defined by NTE	
	MFS	Number of spanwise cuts in the free vortex network	
EEQS	EMUE	Array of $\partial E/\partial \mu_e$	FGCAL
	EMU	Array of $\partial E/\partial \mu_r$ Array of $(\partial E/\partial \mu_e)^{-1}$ $(\partial E/\partial \mu_r)$	DFGMU
	IPR	Array of indices of row pivoting for equation solver	FGCAL
FLATP	NFLTP	=1 for flat panel; =0 otherwise	INPUT
FSVEL	FSV	Freestream velocity vector	INPUT
	FSVM	Freestream velocity magnitude	
	ALPHA	Wing angle of attack in radians	
	XPITCH	X value of pitch axis	
	RCHORD	Length of root chord	
ICONST	PI	π	AICGEN
	PI2	2π	
	PI4I	$1/4\pi$	
INDEX	NT	Array containing network type indices 2,4,6,5,7	INPUT
	NM	Array containing the number of spanwise panel points in each network	
	NN	Array containing the number of transverse cuts in each network	
	NP	Array containing the number of panels in each network	
	NS	Array containing the number of singularity parameters in each network	SING
	NC	Array containing the number of control points in each network	CONTRL
	NZ	Array containing the number of panel points in each network	

Common Block	Variables	Description	Where Set
	NPA	Array containing cumulative sum of array NP	
	NSA	Array containing cumulative sum of array NS	TSING
	NCA	Array containing cumulative sum of array NC	TCNTRL
	NZA	Array containing cumulative sum of array NZ	
	NNETT	Number of networks	
	NPANT	Number of total panels	
•	NSNGT	Number of total singularity parameters	TSING
	NCTRT	Number of total control points	TCNTRL
	NZMPT	Number of total panel corner points in all networks	
INTQ	Н	Array of H integrals	INTCAL
•	HZ	Z distance of field point above panel	
	IH .	Indicates necessity of using special expansion when field point is near panel surface	·
	MXQ	Maximum value of m+n for H integrals required to compute influence coefficients	DPIV
	MXK	Maximum value of k for H integrals required to compute influence coefficients	
IPRINT	IPNPUT	Controls printout of intermediate results from program INPUT in overlay (1,0)	TEA378
	IPGEOM	Controls printout of intermediate results from subroutines GEOMC and SURFIT in overlay (2,0)	
	IPSING	Controls printout of intermediate results from subroutine SING in overlay (2,0)	
	IPCNTR	Controls printout of intermediate results from subroutine CONTRL in overlay (2,0)	

Common Block	Variables	Description	Where Set
	IPEIVC	Controls printout of intermediate results from subroutine EIVC in overlay (2,0)	
	IPOUTP .	Controls printout of intermediate results from program OUTPUT in overlay (4,0)	
LSQSFC	ZK	X,Y,Z coordinates of corner points used in least squares fit	SURFIT,SING
	WTK	Weights used in least squares fit	
	AK	Generalized inverse from least squares fit	LSQSF
	NO	=2 for quadratic fit (6 terms) <2 for linear fit (3 terms)	SURFIT,SING
	NPK	Number of data points used in least squares fit	
MSPNTS	ZM	Array containing panel corner point X,Y,Z coordinates	INPUT
	ZL	Array containing panel lengths along transverse cuts	
NEQS	NE	Number of equations to be solved	TEA378,ITFLOW
	NR	Number of right-hand sides	
	NMAT	Name of file storing the coefficient matrix	
	NRHS	Name of file storing right-hand side or solution vector	
NFAJ	NEQ	Number of equations corresponding to control points at edges of networks	AICGEN
	NF	Number of equations corresponding to all other control points (excluding those at edges)	
	NG	Number of equations corresponding to number of panels of the free sheet network	
NINDX	NEQ	Number of equations corresponding to control points at edges of networks	EDGEIN
	NJC	NJC(j) gives new index for control point j	

Common Block	Variables	Description	Where Set
	IJC	IJC(k) gives the control point which has new index k	
NITF	NFUN	Number of functions called at every KIT iteration	ITFLOW
	JT	Iteration number	
	ITMX	Maximum number of iterations	INPUT
	KIT	Number of iterations to generate new AIC	ITFLOW
	ITPRIN	Printing output occurs at every ITPRIN iteration	INPUT
PANDQ	СР	X,Y,Z coordinates of panel corner points	GEOMC
	PC	Average X,Y,Z coordinates of four corner points	SURFIT
	RO	X,Y,Z coordinates of origin of local panel coordinate system	
	AR	Rotation matrix for transforming from global X,Y,Z coordinates to local panel ξ , η , ζ coordinates	
	ART	Transposition of AR	GEOMC
	P	ξ , η coordinates of panel corner points	SURFIT
	A	Panel principal curvature in \xi direction	
	В	Panel principal curvature in η direction	
	DIAM	Length of longest diagonal of panel	GEOMC
	C	Array of (ξ,η) moments	CCAL
	AST	Matrix defining dependence of coefficients of quadratic doublet distribution on free parameters	SING
	IIS	Array containing indices of free parameters on which panel doublet coefficients depend	
	INS	Number of free singularity parameters determining coefficients of panel quadratic doublet distribution	

Common			
Block	Variables	Description	Where Set
	ITS	Panel singularity type	
	NPDQ	Total number of panel-defining quantities in PANDQ common block, not used in this program	Not set
PINDX	KP	Index for keeping track of the position of record (panel information) on disk to be written	Wherever routines PTRNS and IPTRNS are called
	KQ	Index for keeping track of the position of record (panel information) on disk to be read	
	NPWR	Disk file on which panel information is to be written	
	NPRD	Disk file from which panel information is to be read	
PIVINT	XX	Local panel coordinates of control point	PIVC
	PP	Local coordinates of panel corner points	
	AA	Coefficients of the quadratic surface	
	ВВ	fit of the panel	
	DDIAM	Maximum diagonal of the panel	
	cc	Moments for the panel	
	DVDV	Integrals from routine DPIV	
	NTST	Number of coefficients in panel doublet distribution	
	NCF	Not used in this program	Not set
SIDEQ	QSIDE	Collection of geometric quantities describing relationship of field point to panel side	SIDECL
SKAIC1	AKS1	Coordinate of field point relative to panel corner point expressed in local system	INTCAL
	AET1	Coordinate of field point relative to panel corner point expressed in local system	
	AKS2	Coordinate of field point relative to panel corner point expressed in local system	

Common Block	Variables	Description	Where Set
	AET2	Coordinate of field point relative to panel corner point expressed in local system	
	DRM	Length of panel edge	
	EL1	Distance from panel corner point to projection of field point on panel edge line	
	EL2	Distance from panel corner point to projection of field point on panel edge line	
	ELM	Minimum value of distance from panel edge to projection of field point on panel edge line	
	ANK	Component of unit normal to panel edge	
	ANE	Component of unit normal to panel edge	
	A	Distance from projection of field point on panel plane to panel edge line	
	AA	Square of A	
	GG	Square of distance from field point to panel edge line	·
	S1	Distance from field point to end point of a panel side	
	S2	Distance from field point to end point of a panel side	
	S1I	Inverse of S1	
	S2I	Inverse of S2	
	HM	Magnitude of HZ	,
	НН	Square of HZ	
SKAIC2	GAK	Accumulates A times FK over four panel sides	FKCAL
	GKNK	Accumulates ANK times FNK over four panel sides	FNKCAL
	GENK	Accumulates ANE times FNK over four panel sides	
	GKMN	Accumulates ANK times FMN over four panel sides	FMNCAL

Common Block	Variables	Description	Where Set
	GEMN	Accumulates ANE times FMN over four panel sides	
	GAMN	Accumulates A times FMN over four panel sides	
	H111	Accumulates H(1,1,1) over four panel sides	FKCAL
	FK	F integrals for M=1 and N=1	
	FNK	F integrals for M=1	FNKCAL
	FMN	F integrals for K=1	FMNCAL
	E	E functions used for computation of F integrals	ECAL
SKAICI	MXFK	Maximum value of K for F integrals	INTCAL
	MXFKN	Maximum value of K for F integrals when field point is near panel edge and special expansion is required	FKCAL
	MXFNK	Not used in this program	Not set
	MXKM2	Used as upper limit for certain K loops	INTCAL
	MXKM4	Used as upper limit for certain K loops	
	MXQM1	Used as upper limit for certain M or N loops	
SKAICL	LMXQ2	Logical variable used to circumvent unnecessary calculations	INTCAL
	LMXQ3	Logical variable used to circumvent unnecessary calculations	
	LMXQ4	Logical variable used to circumvent unnecessary calculations	
	LMXK3	Logical variable used to circumvent unnecessary calculations	
	LMXK5	Logical variable used to circumvent unnecessary calculations	
	LMKEX	Logical variable determining necessity of using special expansion for field point near panel surface	

Common Block	Variables	Description	Where Set
SKRCH1	ZA	Array of network points serving as control points or locations of free singularity parameters	GCPCAL
	IA ·	Index array which counts nonidentical points in ZA	GRDIND
SOLN	S	Array of values of doublet parameters	TEA378,ITFLOW
	ZA	Array containing panel inclination angles	INPUT
SYMM	NSYMM	=1 for axisymmetric =0 otherwise	INPUT

DESCRIPTION OF SUBROUTINES

The subroutines are arranged in alphabetical order.

Subroutine AJGEN(X,N)

Purpose To obtain the analytic Jacobian for perturbation variables

(doublet parameters excluding those at edges and angles) assuming

D(AIC)/D(THETA)=0

Input Calling sequence

X-Array of values for the variables

N-Number of variables

Common block

/INDEX/—NM, NN, NZ

/MSPNTS/—ZM /ADR/—DTR

Output Common block

/SOLN/—S, ZA

Subroutines Called DFGMU, DFGDT

Discussion

The routine stores values of doublet parameters (excluding those at edges) and angles in array S and ZA, respectively. Routines are called to generate the partial derivatives of functions F and G with respect to doublet parameters MU, excluding those at edges (DFGMU) and angles

THETA (DFGDT).

Subroutine AWNET

Purpose To calculate the coordinates of all panel corner points in an arrow

wing planform configuration

Input Common block

/DAT3/-AR, NTR, XTR, MSP, YSP, NTC

Output Common block

/DAT3/—YLE, NTE

/MSPNTS/--ZM

Subroutines

Called

SWEPTE

Discussion The Y coordinates of the panel corner points at the intersection of the leading edge and transverse cuts are computed by multiplying the X

value of the transverse cut by one-fourth the aspect ratio.

The Y coordinates of the panel corner points between the leading edge and root chord on the transverse cuts are computed by multiplying the Y coordinate at the leading edge by the array of percent values YSP.

Subroutine SWEPTE is called to calculate the Y coordinates of all panel points aft of the root chord.

The X coordinates of the panel corner points are the X values of the transverse cuts input by the user. All Z coordinates are set to zero.

Subroutine

BSUBSM(A,NR,N,IPR,B,M)

Purpose

To perform back substitutions using the factorization obtained from a decomposition routine and find the solution for a system of equations

Input

Calling sequence

A —The lower triangle of the array consists of a lower triangular matrix L and the upper triangle consists of an upper triangular matrix U. They are obtained from a decomposition routine such as TDECOM

NR -Maximum row dimension of arrays A and B

N —Order of the coefficient matrix

IPR—Array consists of numbers of pivotal row, as derived from the subroutine TDECOM

B —Array consists of M right-hand sides of the linear system

M -Number of right-hand sides

Output

Calling sequence

B -Solution vectors

Subroutines

Called

VIPS

Discussion

The routine first uses pivotal information given in the array IPR to exchange elements of right-hand sides. It then performs forward substitution by solving the lower triangular system of equations LY=B and backward substitution by solving the upper triangular system of equations UX=Y. X is the desired solution of the given system of equations.

The routine is a modified version of a routine in the subroutine library of the Boeing Computer Services company.

Subroutine

CCAL(P,C)

Purpose

To calculate for each panel the quadrilateral moment integrals used in the computation of the source and doublet far-field velocity influence coefficients. (See sec. B.4, app. B, of the Engineering Document.)

Input

Calling sequence

P-Coordinates of four corner points of quadrilateral

Output

Calling sequence

C—Array of moment integrals

Subroutines

ECAL, ZERO

Called

Discussion

The routine computes the quadrilateral moment integrals C(M,N)=I(SIGMA, KSE**(M-1)*ETA**(N-1), DKSE*DETA) for M=1, MXQ and N=1, MXQ-M+1. A description of the calculations performed is contained in section B.4 of appendix B of the Engineering Document. The relevant equations are (B-93) through (B-102). The relevant procedure is procedure 6. The code closely follows the development and notation of this portion of appendix B.

Subroutine CMAB(A,B,R,NRA,NCA,NCB)

Purpose To multiply two matrices whose elements are stored compactly by row

(compass)

Input Calling sequence

A—Location of first matrix
B—Location of second matrix
R—Location of resultant matrix

NRC—Number of rows in first matrix NCA—Number of columns in first matrix NCB—Number of columns in second matrix

Output Calling sequence

R-Resultant matrix

Subroutines

Called

None

Discussion Performs the matrix operation (R)=(B)(A).

Subroutine CONTRL(NT,NM,NN,NC,NPA,ZM,ZC,ZCC,ZCR,ZDC,IPC,ITC)

Purpose To compute control point defining quantities for each network

Input Calling sequence NT—Network type

NM-Number of spanwise cuts in the network

NN—Number of transverse cuts in the network NPA—Total number of panels in all previous networks

TVPA—Total number of panels in all previous networks

ZM-Coordinates of corner points in the network

Common block /IPRINT/—IPCNTR /FSVEL/—FSV /PANDQ/—PC

Output Calling sequence

NC—Number of control points on the network
ZC—Coordinates of control points on the network
ZCC—Surface normal vector at control points

ZCR-Normal components of freestream velocity

ZDC—Relocation distance of control point

IPC—Sequence number of panel to which control point belongs

ITC-Network edge control point indicator

Subroutines Called GCPCAL, GRDIND, PTRNS, SURPRO, MMULT

Discussion

The routine calculates quantities associated with the control points and boundary conditions of the problem. Separate computations are performed for each network type. First, the control points (points at which the boundary conditions are applied) are located. This is done by averaging certain combinations of corner points and then projecting the resultant points onto the panel surfaces. Those control points located on a network edge are withdrawn slightly from the edge and not projected onto their panel surfaces to avoid numerical difficulty later. The control points are ordered and indexed along with auxiliary quantities which are computed as well. Such quantities include the panel normal at the control point, the component of freestream velocity in this direction (for use in applying the boundary conditions), and the distances the edge control points are withdrawn.

Subroutine

CROSS(A,B,C)

Purpose

To calculate the cross product of two vectors

Input

Calling sequence
A—First vector

B-Second vector

Output

Calling sequence

C-Resultant vector

Subroutines Called None

Discussion

CROSS performs the following calculations:

C(1)=(A(2)*B(3))-(A(3)*B(2)) C(2)=(A(3)*B(1))-(A(1)*B(3))C(3)=(A(1)*B(2))-(A(2)*B(1))

Subroutine

DFGDT(ZM,NM,NN)

Purpose

To calculate partial derivatives of functions F and G with respect to panel inclination angles of free sheet, assuming D(AIC)/D(THETA)=0

Input

Calling sequence

ZM-Coordinates of corner points of free sheet network

NM—Number of spanwise cuts of network NN—Number of transverse cuts of network

Common block /CM03/—NSCR /BDYCS/—ZC /FSVEL/—FSV

/NFAJ/—NEQ, NF, NG

/ADR/—DTR

Output

Common block /CM03/—NJAC

Subroutines Called PTRNS, CROSS, UVECT, VIP, UNIPAN, MMULT

Discussion

A detail discussion of the formula used in the computation is given in the Engineering Document (see app. C, geometry update coefficients). The routine first finds a normal vector N for the panel. It then computes partial derivatives of N with respect to angle THETA and forms partial derivatives of N·V and of pressure jump with respect to THETA. Finally, it stores all partial derivatives in proper position of the Jacobian.

Subroutine

DFGMU

Purpose

To calculate partial derivatives of functions F and G with respect to doublet parameters (excluding those at edges)

Input

Common block

/CM03/--NPIF, NAIC3

/BDYCS/—ZC /INDEX/—NSNGT /FSVEL/—FSV

/NFAJ/—NEQ, NF, NG

/SOLN/-S

/EEQS/--EMUE, EMU, IPR

Output

Common block /CM03/—NSCR

Subroutines Called BSUBSM, PTRNS, MMULT, UNIPAN, VIPS

Discussion

The formula and notation used here are discussed in detail in the Engineering Document (see app. D, doublet strength update coefficients). The routine reads in DE/DMUE and DE/DMU and calculates (DE/DMUE)(-1)*(DE/DMU), where E is the function consisting of only those equations corresponding to control points at edges. Then, it obtains partial derivatives of N·V on wing and on free sheet with respect to doublet parameters. Partial derivatives of pressure jump V·GRAD(MU) with respect to doublet parameter are also calculated. Finally, partial derivatives with respect to doublet parameters excluding those at edges are formed.

Subroutine

DPIV

Purpose

To calculate the velocity influence coefficients induced at a field point

by a doublet panel

Input

Common block

/ICONST/--PI2, PI4I

/PIVINT/—X, P, A, B, DIAM, C, NTST

Output

Common block

/PIVINT/—DV

Subroutines

INTCAL, ZERO

Called

Discussion

The routine computes the doublet panel velocity influence coefficients at a specified field point. A description of the method and calculations performed is contained in appendix B of the Engineering Document. If the field point is sufficiently distant from the panel, a far-field approximation is employed. The approximation and computational method is presented in section B.4 of appendix B and the related code comprises the part of DPIV between statement 120 and statement 500. The loop 450 contains the bulk of the calculations, and its purpose is to compute the J vectors of equation (B-91). For this calculation the terms on the right side of equation (B-91) have been expanded; hence, the code does not directly correlate with this formula. Another evaluation procedure is employed when the field point is near the panel. A description of this procedure is presented in sections B.2 and B.3 of appendix B. The related code comprises the part of DPIV between statements 500 and 900. The loop 750 calculates the vector J, defined by equation (B-34), with the H integrals computed by the routine INTCAL. The loop 800 transforms the influence coefficients relative to the expansion of doublet strength about the projection of the field point to coefficients relative to the expansion of doublet strength about the origin.

Subroutine DWNET

Purpose

To calculate the coordinates of all panel corner points in a delta wing

planform configuration

Input Common block

/DAT3/—AR, NTR, XTR, MSP

Output

Common block /DAT3/—YLE /MSPNTS/—ZM Subroutines

None

Called

Discussion

The Y coordinates of panel corner points at the intersection of the leading edge and the transverse cuts are computed by multiplying the X value of the transverse cut by one-fourth the aspect ratio.

The Y coordinates of the panel corner points between the leading edge and root chord on the transverse cuts are computed by multiplying the Y coordinate at the leading edge by the array of percent values YSP.

The X coordinates of the panel corner points are the X values of the transverse cuts input by the user. All Z coordinates are set to zero.

Subroutine E0

ECAL(X1,X2,A1,A2,E,N)

Purpose

To evaluate $E(I) = A2 \cdot X2 \cdot \cdot \cdot (I-1) \cdot A1 \cdot X1 \cdot \cdot \cdot (I-1)$; I = 1, N. (See eq.

(B-59), app. B, of the Engineering Document.)

Input

Calling sequence X1—(see Purpose) X2—(see Purpose) A1—(see Purpose) A2—(see Purpose) N—(see Purpose)

Output

Calling sequence E—(see Purpose)

Subroutines

None

Called

Discussion The routine calculates the quantities:

 $E(I)=A2*X2**(I-1)-A1*X1**(I-1) \ for \ I=1,N \ using the recursion formula \\ E(I)=(X1+X2)*E(I-1)-X1*X2*E(I-2) \ and \ the \ initial \ conditions$

E(1)=A2-A1 and E(2)=A2*X2-A1*X1.

Subroutine

EDGEIN

Purpose

To provide new indices for the control points and doublets so that the corresponding equations (downwash condition) and doublets at edges of network will precede all the others

Input

Common block /BDYCS/—ITC /INDEX/—NCTRT

Output

Common block

/NINDX/--NEQ, NJC, IJC

Subroutines

None

Called

Discussion

The routine obtains the number of equations corresponding to control points at edges. Then it assigns indices according to whether control points are at edge or interior.

32.

<u>Subroutine</u> <u>EIVC(ZC,ZNC,ZDC,IPINF)</u>

Purpose To calculate the velocity induced by a doublet panel on a network edge

control point

Input Calling sequence

ZC-Coordinates of control point

ZNC—Unit normal to surface at control point ZDC—Distance from control point to panel edge

Common Block /IPRINT/—IPEIVC /ZIP/—IPZ, IP, JCZ

/PANDQ/---CP, PC, RO, AR, P, DIAM

/SYMM/—NSYMM

Output Calling sequence

IPINF-Indicates whether panel is close enough to control point to

induce a substantial downwash

Common block /PIVM/—DVDS

Subroutines Called ZERO, CROSS, UNIPAN

Discussion The routine calculates the velocity induced by a doublet panel (and its

image if configuration is symmetrical) on a network edge control point. The influence is computed by accumulating the influence of each panel edge. The influence of a panel edge is ignored unless a point on the edge is within a small sphere around the control point. In this case, the influence, resulting from both the doublet strength and its derivative perpendicular to the edge (evaluated at that edge point), is computed. The resultant velocity is then distributed among the

coefficients of the doublet distribution on the panel.

Subroutine FGCAL(FVZ,GVZ)

Purpose To solve for doublet parameters at edges and to calculate functions F

and G

Input Common Block

/CM03/—NPIF, NAIC3, NAIC

/BDYCS/—ZC, ZCR /FSVEL/—FSV

/NFAJ/—NEQ, NF, NG

/SOLN/—S

Output Calling sequence

FVZ—Values of F GVZ—Values of G

Common block

/EEQS/—EMUE, EMU, IPR

Subroutines Called VIPS, LINEQS, PTRNS, MMULT, VIP, UNIPAN

Discussion

The routine reads rows of AIC matrix to form coefficients of function E. The solution for doublet parameters (MUE) at edges are found by using function E and given values of all other doublet parameters (MU). Since E is a function of doublet parameters only, DE/DMUE and DE/DMU are simply the coefficients of E. If the matrix DE/DMUE is singular, an error message will be printed and the execution of the computer program will be terminated. Components of influence coefficients are read in and multiplied by values of doublet parameters to form perturbation velocity. The latter is added to freestream velocity to become the average velocity vector V. The DOT product N·V is then calculated for every interior control point on wing (forming part of function F) and on free sheet (forming function G).

The jump in pressure coefficients $V \cdot GRAD(MU)$ (see Engineering Document) on free sheet is also calculated (forming the other part of function F).

Subroutine

FKCAL

Purpose

To calculate certain F integrals used to compute the H integrals involved in the formulas for the source and doublet panel induced velocity influence coefficients. (See sec. B.3 of app. B of the Engineering Document.)

Input

Common block

/SKAICL/—LMKEX

/SKAIC1/—EL1, EL2, ELM, A, AA, GG, S1, S2, S1I, S2I, HM

/SKAICI/--MXFK

Output

Common block /SKAICI/—MXFKN SKAIC2/—GAK,H111

Subroutines Called **ECAL**

Discussion

The routine computes the integrals F (1,1,K) for K=1,MXFK where F(1,1,K)=I(L,1./RHO**K,DL). A description of the calculations performed is contained in section B.3 of appendix B of the Engineering Document. The relevant equations are (B-60), (B-61), (B-68), and (B-69). The relevant procedures are 4 and 5. The routine also computes the arctangent terms of step 1 (eq. (B-41) of procedure 1. The code closely follows the development and notation of section B.3. Note that FNK(N,K)=F(1,N,K).

Subroutine FMNCAL

Purpose To calculate certain F integrals used to compute the H integrals

involved in the formulas for the source and doublet panel induced velocity influence coefficients. (see sec. B.3 of app. B of the

Engineering Document.)

Input Common block

 $/INTQ/_MXQ$

/SKAICL/—LMXQ2, LMXQ3

/SKAIC1/—AKS1, AET1, AKS2, AET2, ANK, ANE, A, AA. S1, S2, HH

Output Common block

/SKAIC2/—GKMN, GEMN, GAMN

Subroutines Called **ECAL**

Discussion

The routine computes the integrals F(M,N,1) for N=1,MXQ and M=1,MXQ-N+1 where F(M,N,1)=I(L,KSE**(M-1)*ETA**(N-1)/RHO, DL). A description of the calculations performed is contained in section B.3 of appendix B of the Engineering Document. The relevant equations are (B-62), (B-63), (B-64), and (B-65). The relevant procedures are 4 and 5. The code closely follows the development and notation of section B.3. Note that FMN(M,N) = F(M,N,1).

Subroutine FNKCAL

Purpose To calculate certain F integrals used to compute the H integrals

involved in the formulas for the source and doublet panel induced velocity influence coefficients. (see sec. B.3 of app. B of the

Engineering Document.)

Input Common block

/SKAICL/—LMXQ3, LMXQ4, LMXK5 /SKAIC1/—ANK, ANE, AA, S1I, S2I, HH

/SKAICI/—MXKM2, MXQM1

Output Common block

/SKAIC2/—GKNK, GENK

Subroutines

Called

ECAL

Discussion The routine computes the integrals F(1,N,K) for N=2,MXQ and

K=3,MXK-2,2 where

F(1,N,K)=I(L,ETA**(N-1)/RHO**K,DL). A description of the calculations performed is contained in section B.3 of appendix B of the Engineering Document. The relevant equations are (B-66) and (B-67). The relevant procedures are procedures 4 and 5. The code closely follows the development and notation of section B.3. Note that

FNK(N,K)=F(1,N,K).

Subroutine FUNC(X,N,RX)

Purpose To evaluate function F (N·V on wing and V·GRAD(MU) on free sheet)

and G (N·V on free sheet)

Input Calling sequence

X-Array of values for the variables

N-Number of variables

Common block

/NFAJ/—NEG, NF, NG

/NITF/—NFUN /SOLN/—ZA /ADR/—DTR

Output

Calling sequence

RA-Array of values of functions

Subroutines Called UPDATE, AICGEN(OVERLAY-2,0), FGCAL

Discussion

The routine stores values of doublet parameters (excluding those at edge) and angles in arrays S and ZA, respectively. It uses new angles to update the corner points of free sheet, fed sheet, and part of the wake network. AICGEN(OVERLAY-2,0) is then called to designate locations of doublets and control points and to generate velocity components and AIC matrix using the updated corner points. If perturbation in angle is not significant, UPDATE and AICGEN are skipped. Finally, the routine calls FGCAL to calculate values of functions F and G.

Subroutine

GCPCAL(NM,NN,NM1,NN1,ZM,ZA)

Purpose

To construct an NM+1 by NN-1 grid of points from corner point data

Input

Calling sequence

NM—Number of corner points in a row
NN—Number of corner points in a column
NM1—Number of grid points in a row (NM+1)
NN1—Number of grid points in a column (NN+1)

ZM-Coordinates of corner points

Output

Calling sequence

ZA-Coordinates of grid points

Subroutines

Called

None

Discussion

The routine computes an NM+1 by NN+1 grid of points derived from corner point data. The points in the grid consist of the average of each set of four adjacent corner points, the average of each set of two adjacent edge corner points, and the four extreme corner points. These points are obtained by computing approximate averages of the corner

points.

Subroutine GEOMC(NT,NM,NN,NPA,ZM)

Purpose To calculate geometric defining quantities for each panel in a network

Input Calling sequence

NT-Network type

NM—Number of spanwise cuts in network NN—Number of transverse cuts in network

NPA—Total number of panels in all previous networks ZM—Coordinates of corner points in the network

Common block
/IPRINT/—IPGEOM

Output Common block

/PANDQ/—CP,PC,RO,AR,ART,P,A,B,DIAM,C

Subroutines Called SURFIT, CCAL, IPTRNS

Discussion The routine calculates and stores geometric defining quantities for

each panel of a network. First, the four grid points defining the panel corner points are found. Together with adjacent grid points, these corner points are fed into SURFIT, which defines the actual panel surface and the local panel coordinate system. Then CCAL is called to calculate panel moments. Finally, all the panel-defining quantities are

stored on a file.

Subroutine GRDIND(NM,NN,Z,I,IS)

Purpose To order nonidentical points of an NM by NN grid of points via an

index array

Input Calling sequence

NM—Number of grid points in a row NN—Number of grid points in a column

Z-Coordinates of grid points

Output Calling sequence

I-Index array containing sequence number of each grid point

IS-Total number of nonidentical points in a grid

Subroutines

PIDENT

Called

Discussion The routine sequences an NM by NN grid of points. The sequencing

proceeds in the order ((M=1,NM),N=1,NN), where (M,N) is the point in row M and column N. Any point identical with the point in the same row and previous column or with the point in the same column and previous row is assigned the same sequence number as that point. The sequence numbers of the grid points are stored in an NM x NN index array and returned as output along with the total number of

nonidentified points.

Subroutine GWNET

Purpose To calculate the coordinates of all panel corner points in a gothic wing

planform configuration

Input Common block

/DAT3/—NTR,XTR,MSP,YSP,NTC,YLE

Output Common block

/DAT3/—NTE /MSPNTS/—ZM

Subroutines

Called

SWEPTE

Discussion The Y coordinates of panel corner points at the intersection of the

leading edge and transverse cuts are input by the user.

The Y coordinates of panel corner points between the leading edge and root chord on the transverse cuts are computed by multiplying the Y coordinate at the leading edge by the array of percent values YSP.

Subroutine SWEPTE is called to calculate the Y coordinates of all

panel points aft of the root chord.

The X coordinates of the panel corner points are the X values of the transverse cuts input by the user. All Z coordinates are set to zero.

Subroutine INTCAL

Purpose To compute the H integrals involved in the formulas for the source and

doublet panel induced velocity influence coefficients. (See sec. B.3 of

app. B of the Engineering Document.)

Input Common block

/INTQ/--MXQ,MXK

/PIVINT/—X,P,AC,BC,DIAM

Output Common block

/INTQ/—H,HZ,IH

Subroutines

Called

SIDECL, ZERO, TRNSFR, FKCAL, FMNCAL, FNKCAL

Discussion The routine calculates the integrals H(M,N,K)=1(SIGMA,KSE**(M-1)

*ETA**(N-1)/RHO**K,DKSE*DETA) for M=1,MXQ and N=1,MXQ-M+1 and K=1,MXK,2. A description of the calculations performed is contained in section B.3 of appendix B of the Engineering Document. The routine can be divided into three parts. In the first part, preliminary quantities concerning the geometric relationship of the field point to the quadrilateral are calculated. In the second part, the F integrals are calculated for each side of the quadrilateral and

accumulated. In the third part, procedure 1, 2, or 3 is executed.

Subroutine

IPTRNS(IP)

Purpose

To write panel information on disk

Input

Calling sequence

IP-Panel number of information to be written

Common block

/PANDQ/—CP,PC,RO,AR,ART,P,A,B,DIAM,C,AST,IIS,INS,ITS

/PINDX/—KP,NPWR

Output

Common block /PINDX/—KP

Subroutines

Discussion

None

Called

Writes 197 words of panel information from common block PANDQ

onto disk file specified by NPWR.

Subroutine

ITFLOW(X,N,RX,DX,Y,RY)

Purpose

To perform iterative scheme using quasi-Newton algorithm for the

solution of a set of nonlinear equations

Input

Calling sequence

X—Array of initial values for the variables

N-Number of variables DX,Y,RY—Scratch arrays

Common block /NFAJ/—NEQ,NF /NITF/—ITMX,ITPRIN

Output

Calling sequence

X-Array of solution vector RX—Array of residual vector

Subroutines

VIP. FUNC,

Called

(OVERLAY-3,0)

Discussion

The routine calls FUNC to evaluate residuals RX and calls AJGEN to set up the Jacobian AJ. The system of equations AJ+DX=-RX is solved and a new approximate solution is found using corrections DX. Residuals and Jacobian are evaluated at the new solution. The procedure is repeated until the sum of squares of residuals satisfies a predetermined tolerance TOL or the given maximum number of iterations ITMX is reached. The routine includes a procedure of generating new AIC after every kit iteration. The Jacobian will be calculated by calling AJGEN only when new AIC is generated. Otherwise, it will be updated by using a formula of quasi-Newton scheme (see Engineering Document). Number of iteration, sum of squares of residuals, and step size are printed for every ITPRIN iteration. For iteration study and checkout purpose, some other intermediate print statements are included (see listing).

OUTPUT(OVERLAY-4,0),

AJGEN.

SOLVER

Subroutine **KSORT**

Purpose To sort the column of a two-dimensional array using the given key

index array

Calling sequence Input

A-Array of which the column is to be sorted

M-Number of rows of A N-Number of columns of A

KEY-Array consists of given key indices W-Working array of same dimension as A

Output Calling sequence

A—The sorted array

Subroutines

None

Called Discussion

The contents of array A are stored in a working array using the indices given in key array. Working array is then transferred back to

array A.

Subroutine

LINEQS(A,NR,N,IPR,B,M,D1)

Purpose

To solve a system of linear equations $A \cdot X = b$

Input

Calling sequence

A-Array consists of elements of the coefficient matrix

NR-Maximum row dimension of arrays A and B

N—Order of the coefficient matrix

B-Array consists of M right-hand sides of the linear system

M—Number of right-hand sides

Output

Calling sequence

A—The lower triangle of the array consists of a lower triangular matrix L, and the upper triangle consists of an upper triangular matrix U. (Since U is unit upper triangular, its diagonal elements

are not stored.)

IPR—Array gives numbers of pivotal row (a record of interchanges)

B—Solution vectors

D1-=+1 or -1 according to the number of interchanges being even or odd. It also indicates successful return; = 0 indicates that the coefficient matrix appears singular.

Subroutines Called

TDECOM, BSUBSM

Discussion

Routine TDECOM is first called by LINEQS to perform the decomposition of the coefficient matrix A into a lower triangular matrix L and an upper triangular matrix U. The result is then used in BSUBSM for carrying out back substitutions and obtaining the

solution to the system of equations.

This routine is a modified version of a routine in the subroutine library of the Boeing Computer Services company.

Subroutine

LSQSF

Purpose

To find the generalized inverse from a least squares fit

Input

Common block

/LSQSFC/—ZK,WTK,NO,NPK

Output

Called

Common block /LSQSFC/-AK

Subroutines

TRANS, MMULT, PDSEQS

Discussion

The routine first forms the weighted normal equations. It then calls routine using the Cholesky scheme to solve the system of equations and finds the generalized inverse. If the system of equations is not positive definite, an error message will be printed and execution of the

computer program will be terminated.

Subroutine

MMULT(A,B,C,L,M,N)

Purpose

To multiply two matrices

Input

Calling sequence

A-Array containing elements of matrix A B-Array containing elements of matrix B

L-Number of rows in A and C

M-Number of columns in A and rows in B

N-Number of columns in B and C

Output

Calling sequence C-Resultant matrix

Subroutines

CMAB

Called

Discussion

MMULT calls CMAB to calculate (C) (A)(B).

Subroutine

PANUNI(ART,RO,Y,X)

Purpose

To transform point coordinates from the local panel system to the universal system

Input

Calling sequence

ART-Local to global panel system transformation matrix

RO-X,Y,Z coordinates of panel center (universal) Y-X,Y,Z coordinates of point to be transformed (local)

Output -

Calling sequence

X—X,Y,Z coordinates of transformed point (universal)

Subroutines

MMULT

Called

Discussion

The local panel coordinates are multiplied by the matrix ART using subroutine MMULT to produce the global panel coordinates which, when added to the universal panel center, produce the universal

coordinates.

Subroutine

PDSEQS(A,NR,N,DN,B,M,D1)

Purpose

To solve a system of equations A*X=B, where A is a positive definite symmetric matrix, using Cholesky decomposition

Input

Calling sequence

A-Array of which the upper triangle is the upper triangle of a given

positive definite symmetric matrix $NR\mbox{--}Maximum\ row\ dimension\ of\ arrays\ A\ and\ B$

N—Order of the positive definite coefficient matrix B—Array consists of M right-hand sides of the linear system

M-Number of right-hand sides

Output

Calling sequence

B—Solution vectors

A-Array of which the upper triangle is same as input, the lower triangle contains the lower triangular matrix L from Cholesky

decomposition with diagonal elements excluded DN—The reciprocals of diagonal elements of L

D1—=1 for successful return

=0 indicates that the given coefficient matrix appears not positive definite

Subroutines Called None

Discussion

The routine first performs the Cholesky decomposition of the given matrix A into a lower triangular matrix L and its transpose. It then solves the given system of equations by back substitutions.

Subroutine

PIDENT(P,Q,IDENT)

Purpose

To determine whether the points P and Q are to be considered numerically identical

Input

Calling sequence

P—Coordinates of first point Q—Coordinates of second point

Output

Calling sequence

IDENT—Logical variable equal to true if P and Q are considered identical, and false otherwise

Subroutines Called None

Discussion

The routine determines whether the points P and Q are considered numerically identical. The criterion for identity is that the distance from P to Q must be smaller than or equal to 1.E-12 times the sum of the lengths of P and Q.

Subroutine PIVC

Purpose To obtain doublet panel influence coefficients for a given control point

Input Calling sequence

Z-X,Y,Z coordinates of a given control point

Common block

/PANDQ/—RO,AR,ART,P,A,B,DIAM,C

/SYMM/—NSYMM /ZIP/—IPZ,IP

Output Common block

/PIVM/—DVDS

Subroutines

UNIPAN, DIPV, MMULT

Discussion

Called

The routine first transfers some of the panel information to be used by the integration routine. It then calls the integration routine to provide influence coefficients for a given control point induced by doublet distribution of the specified panel and its image (when NSYMM is set to 1). The influence coefficients are modified to account for the case when the given control point is located on the influencing panel itself (see Engineering Document—Aerodynamic Influence Coefficients).

Subroutine PTRNS(IP)

Purpose To read panel information from disk

Input Calling sequence

IP-Panel number of information to be read

Common block

/PINDX/---KQ,NPRD

Output Common block

/PANDQ/—CP,PC,RO,AR,ART,P,A,B,DIAM,C,AST,IIS,INS,ITS

/PINDX/—KQ

Subroutines

Called

None

Discussion Reads 197 words of panel information from disk file specified by NPRD

into common block PANDQ.

Subroutine SHEGEN(ALPHA,X,S,N,Y,Z)

Purpose To provide an initial guess of the free and fed sheet geometry at a

particular transverse cut

Input

Calling sequence

ALPHA—Angle of attack of the wing (in radians)
X—X coordinate of transverse cut (APEX is X=0.0)
S—Y coordinate of leading edge on transverse cut

N-Desired number of free sheet panels in transverse cut

Calling sequence

Output

Y-Y coordinate of corner points defining shape of free and fed sheets on given transverse cut

Z—Z coordinates of corner points defining shape of free and fed sheets on given transverse cut

Subroutines Called None

Discussion

The routine computes an initial guess of the free and fed sheet geometry at a particular transverse cut. (See starting solution section of Engineering Document for method. Points describing the curves of figure 17 are stored in the array YZVAL.) Each curve represents the free and fed sheet geometry for one of eight values of A. Points describing the free and fed sheet geometry for an arbitrary value of A are obtained by linear interpolation (or extrapolation). Linear interpolation is then employed on this new set of points to construct a representation of the free sheet by the number of points specified in the input data.

Subroutine SIDECL(W,DSMIN,D)

Purpose

To compute geometric quantities associated with the relationship of the field point to the quadrilateral Σ for use in computing the H integrals. (See fig. 30 and sec. B.3 of app. B of the Engineering Document.)

Input

Common block
/PIVINT/—X,P

Output

Calling sequence

W—Point on quadrilateral closest to projection of field point onto quadrilateral plane

DSMIN—Minimum distance of projection of field point onto quadrilateral plane to perimeter of quadrilateral

D—Distance from W to projection of field point onto quadrilateral plane

Common block /SIDEQ/—QSIDE

/SKAIC1/—AKS1,AET1,AKS2,AET2,DRM,EL1,EL2,ELM,ANK,ANE,A,AA

Subroutines Called TRNSFR

Discussion

The routine computes geometric quantities associated with the relationship of the quadrilateral Σ to the projection of the field point onto the quadrilateral plane. In particular, the routine determines whether the projection lies inside or outside of the quadrilateral as well as calculates the minimum distance from the projection to the perimeter of the quadrilateral. Other quantities computed include those quantities displayed in figure 31 and discussed in section B.3 of appendix B of the Engineering Document. The quantities associated with the quadrilateral in general are returned via the call list, whereas the quantities associated with each side of the quadrilateral are stored in a common block array, a side at a time.

Subroutine

SINFCC(Z)

Purpose

Given the X,Y,Z coordinates of a point SINFCC defines a matrix (DSDFS), which when multiplied by a vector consisting of values of all doublet parameters, gives the value and 1st,2nd derivatives of doublet strength at the given point

Input

Calling sequence

Z-X,Y,Z coordinates of the given point

Common block /INDEX/—NSNGT

/PANDQ/—RO,AR,AST,IIS,INS

Output

Common block /SNGC/--DSDFS

Subroutines Called UNIPAN

Discussion

Subroutine UNIPAN converts the input point from the universal to local panel coordinate system.

A six-by-six matrix is formed by the general equation representing the doublet strength distribution at the given point on a panel and its derivatives.

A six-by-sixteen matrix (AST) for coefficients of quadratic doublet distribution on the panel also exists. The matrix is computed in subroutine SING.

The matrix DSDFS is formed by multiplying these two matrices.

Subroutine SING(NT.NM.NN,NS.NSA,NPA.ZM)

Purpose To calculate the singularity distribution defining quantities for a given

network

Input Calling sequence

NT-Network type

NM—Number of spanwise cuts in the network NN—Number of transverse cuts in the network

NSA-Total number of singularity parameters in all previous

networks

NPA-Total number of panels in all previous networks

ZM-Coordinates of corner points in the network

Common block /IPRINT/—IPSING /PANDQ/—RO,AR

Output Calling sequence

NS-Number of singularity parameters in the network

Common block

/PANDQ/—AST,IIS,INS,ITS

Subroutines Called GCPCAL, GRDIND, PTRNS, UNIPAN, LSQSF, IPTRNS

Discussion

The routine calculates the dependence of each panel singularity strength distribution on the free singularity parameters of the network. Separate computations are performed for each network type. First, the locations of the free singularity parameters on the network are computed and indexed. For each panel, the singularity parameters affecting the distribution of singularity strength on that panel are isolated. Each such parameter is assigned a weight (large if the parameter actually lies on the panel). The panel singularity distribution is then obtained by fitting a quadratic form (if the singularity is of doublet type) to the parameters by the method of least squares. The matrix that relates the coefficients of the distribution to the singularity parameters is then stored on a file along with indices identifying the parameters.

Subroutine SNGCAL(Z,TSC)

Purpose To calculate the value and 1st,2nd derivatives of doublet strength at

the specified point

Input Calling sequence

Z-X.Y,Z coordinates of the given point

Common block /SOLN/--S

Output Calling sequence

TSC-Array consists of the value and 1st.2nd derivatives of doublet

strength

Subroutines

SINFCC, MMULT

Called

Discussion

SNGCAL calls subroutine SINFCC to produce the matrix DSDFS. MMULT multiplies this matrix by the vector consisting of values of all doublet parameters previously obtained to produce the value and 1st,2nd derivatives of doublet strength at the given point.

Subroutine

SURFIT

Purpose

To define panel surface and local panel coordinate system

Input

Common block /FLATP/—NFLTP

/LSQSFC/—ZK,WTK,NO,NPK

/PANDQ/--CP

/IPRINT/—IPGEOM

Output

Common block

/PANDQ/—PC,RO,AR,P,A,B

Subroutines

Called

CROSS, UVECT, TRANS, UNIPAN, LSQSF, MMULT

Discussion

The routine defines a panel surface and local panel coordinate system. As a first approximation to the panel surface, the routine takes the quadrilateral formed by projecting the panel corner points onto the plane through the midpoints of the line segments joining these corner points. A local coordinate system is constructed with the origin at the average of the quadrilateral corner points and with one axis normal to the quadrilateral. To obtain a second order approximation to the panel surface, the routine calculates a paraboloid passing through the corner points with curvature obtained by least squaring the paraboloid to adjacent corner points. The local coordinate system is then rotated and translated in such a manner that the paraboloid can be represented in canonical form. An iterative process is required to eliminate linear terms without translating the origin.

Subroutine

SURPRO(Z,ZP,UN)

Purpose

To find the location of the projection of a point onto a panel surface as well as the surface normal at this location

Input

Calling sequence

Z-Global coordinates of point to be projected

Common block

/PANDQ/—RO,AR,ART

Output

Calling sequence

ZD Clab land

ZP—Global coordinates of location of projection

UN-Global coordinates of unit normal to panel surface at this

location

Subroutines

Called

UNIPAN, UVECT, PANUNI, MMULT

Discussion

The routine calculates the projection of a point onto a panel surface as well as the surface normal vector at the projected point. All input and output vectors are assumed to be given in global coordinates. The routine converts to local coordinates, projects and converts back to global coordinates. In the event that the given point does not lie above or below the panel, the projection is made onto the paraboloid of which the panel is a part.

Subroutine

SWEPTE(X,S,N,Y,M,YP)

Purpose

To calculate the Y coordinates of the panel corner points aft of the root chord for swept trailing-edge designs

Input

Calling sequence

- X —Array of transverse cut X values starting with the last cut that intersects the root chord
- S —Array of Y coordinates of the leading edge on the transverse cuts specified by X
- N —Number of transverse cuts aft of the last transverse cut to intersect the root chord plus one
- Y —Array of Y coordinates of panel corner points lying on the last transverse cut that intersects the root chord
- M -Number of spanwise percent values input by the user

Output

Calling sequence

YP-Array of Y coordinates of panel corner points aft of the root chord

Subroutines Called

None

Discussion

Given the coordinates of two points defining a line and one coordinate of a third point on the line, the unknown coordinate of the third point can be calculated by triangulation.

One of the points defining the line is the leading-edge/trailing-edge intersection point. The other point is the panel corner point lying on the last transverse cut that intersects the root chord.

The X value of the third point is the value of the transverse cut.

Subroutine

TCNTRL

Purpose

To designate the location of control points for all network panels and to compute the unit normal vector and the normal component of freestream velocity vector at every control point

Input

Common block

/INDEX/--NT,NM,NN,NPA,NZA,NNETT

/MSPNTS/—ZM

Output

Common block

/BDYCS/—ZC,ZCC,ZCR,ZDC,IPC,ITC

/INDEX/—NCA,NCTRT

Subroutines

CONTRL

Called

Discussion

The routine calls CONTRL to calculate the location of control points for all panels and to compute the unit normal vector and the normal component of freestream velocity vector at every control point on all panels for each network. It also finds the cumulative number of control points and the total number of control points.

Subroutine

TDECOM(A,NR,N,V,IPR,D1)

Purpose

To decompose a square matrix into lower and upper triangular matrices with partial pivoting and row equilibration

Input

Calling sequence

A —Array consists of elements of a given matrix

NR -Maximum row dimension of array A

N -Order of the given matrix

V -Scratch array, may be same array as IPR to save storage

Output

Calling sequence

A —The lower triangle of the array consists of a lower triangular matrix L, and the upper triangle consists of an upper triangular matrix U (since U is unit upper triangular, its diagonal elements are not stored)

are not stored)

IPR—Array gives numbers of pivotal row (a record of interchanges)

D1 —=+1 or -1 according to the number of interchanges being even or odd. It also indicates successful decomposition

=0 indicates that the given matrix appears singular

Subroutines Called VIP, VIPS

Discussion .

The routine performs the crout factorization of a given matrix with partial pivoting and row equilibration. The upper and lower triangular matrices resulting from the decomposition are stored in the array A which originally consisted of elements of the given matrix. If one of the pivots appears to be too small, D1 is set to zero and an error exit is

This routine is a modified version of a routine in the subroutine library of the Boeing Computer Services company.

Subroutine

TGEOMC

Purpose

To generate essential geometry information for each panel of all the networks

Input

Common block

/INDEX/—NT,NM,NN,NPA,NZA,NNETT

/MSPNTS/—ZM

Output

See output of subroutine GEOMC

Subroutines

GEOMC

Called

Discussion

The routine calls GEOMC to calculate essential geometry for all

panels of each network.

Subroutine

TRANS(A,AT,M,N)

Purpose

To form the transpose of a matrix A and store the result in a matrix B

Input

Calling sequence

A-Array containing matrix elements to be transposed

M-Number of rows in A and columns in B N-Number of columns in A and rows in B

Output

Calling sequence

AT-Array containing elements of the transpose of the given matrix

Subroutines

None

Called

Discussion

AT(J,I) is set to A(I,J) as I varies from 1 to M and J varies from 1 to N.

Subroutine

TRNSFR(X,Y,N)

Purpose

To move a number of elements from one array to another

Input

Calling sequence

X-Location of the first array element to be moved

N-Number of elements to be moved

Output

Calling sequence

Y-Array of elements identical to the first N elements in array X

Subroutines

Called

None

Discussion

Y(I) is set to X(I) as I varies from 1 to N.

Subroutine

TSING

Purpose

To designate the location of doublets on all network panels and to

compute the matrix for coefficients of quadratic doublets distribution

for each panel

Input

Common block

/INDEX/—NT,NM,NN,NPA,NZA,NNETT

/MSPNTS/—ZM

Output

Common block

/INDEX/—NS,NSA,NSNGT

Subroutines

SING

Called

Discussion

The routine calls SING to calculate the location of doublets on panels and to compute the matrix for coefficients of quadratic doublet distribution for every panel of each network. It also finds the cumulative number of doublets. Finally, the total number of doublets is obtained.

Subroutine

UNIPAN(AR,RO,X,Y,)

Purpose

To transform point coordinates from the universal system to the local

panel system

Input

Calling sequence

AR-Global to local panel system transformation matrix

RO-X,Y,Z coordinates of panel center (universal)

X—X,Y,Z coordinates of point to be transformed (universal)

Output

Calling sequence

Y—X,Y,Z coordinates of transformed point (local)

Subroutines

Called

MMULT

Discussion

The coordinates of the panel center are subtracted from the coordinates of the point to be transformed. This global array is then multiplied by the matrix AR using subroutine MMULT to produce the local panel coordinates.

Subroutine

UPDATE

Purpose

To update corner points of free sheet, fed sheet, and the part of wake

attached to those sheets

Input

Common block

/INDEX/—NM,NN,NP,NZ

/MSPNTS/—ZM,ZL

/SOLN/—ZA

Output

Common block /MSPNTS/-ZM

Subroutines

None

Called

Discussion

Corner points are updated using given values of angle and fixed chord length of panels in transverse cut obtained previously in INPUT(OVERLAY-1,0). It is assumed that panel corner points move only in transverse cuts. The routine assumes that NM(3)=2, NN(4)=2,

and NM(5)=NN(5)=2.

Subroutine UVECT(A)

Purpose To calculate the direction cosines of a vector

Input Calling sequence

A-Direction numbers of a vector

Output Calling sequence

A-Direction cosines of a vector

Subroutines

None

Called

Discussion UVECT performs the following calculations—A(I)/SQRT(A(1)*A(1)+

A(2)*A(2)+A(3)*A(3), where I varies from 1 to 3.

Subroutine VINFCC

Purpose To generate the three components of aerodynamic influence coefficients

for a given control point induced by all panels doublet distribution

Input Calling sequence

Z-X,Y,Z coordinates of a given control point

ZN—Normal vector at the control point on panel surface ZD—Perturbation distance for control point at edges

JPC-Index of panel of which components of AIC are to be transformed

to its local coordinates

Common block /CMO3/--NPIF

/INDEX/-NPANT,NSNGT

Output Common block

/PINC/—DVDFS

Subroutines

Called

PTRNS, EIVC, PIVC, MMULT

Discussion For every panel, the routine calls PTRNS to transfer panel.

information. Depending on the given control point being at the edge or interior of the panel, the routine calls EIVC or PIVC to evaluate the integrals. The latter is then multiplied by the generalized inverse from least squares fit of quadratic doublet distribution obtained in subroutine SING to form the three components of aerodynamic influence coefficients. If JPC is specified, the components of AIC will

be transformed to local coordinates of that particular panel.

Subroutine VIP(A,INCA,B,INCB,N,C)

VIPA(A,INCA,B,INCB,N,C) VIPS(A,INCA,B,INCB,N,C)

Purpose To perform vector inner product calculation (VIP) and to add (VIPA) to

or subtract (VIPS) from an incoming value (COMPASS)

Input Calling sequence

A-Vector A

INCA-Increment between successive elements of A

B-Vector B

INCB-Increment between successive elements of B

N-Number of elements to be multiplied

C-An incoming value to be added to (VIPA) or to be

subtracted from (VIPS)

Output Calling sequence

C—Result: C=A·B(VIP), C=C+A·B(VIPA), and C=C-A·B(VIPS)

Subroutines

Called

None

Discussion The inner product of two vectors A and B is calculated and stored in

C(VIP). The result is added to (VIPA) or subtracted from (VIPS), an incoming value C, and the sum or the difference is stored back in C.

This routine is a modified version of a compass routine in the

subroutine library of the Boeing Computer Services company.

Subroutine ZERO(A,N)

Purpose To set the elements of an array to zero (COMPASS)

Input Calling sequence

A-Location of first element to be set to zero

N-Number of elements to be set to zero

Output Calling sequence

A-Array of zero elements

Subroutines

Called

None

Discussion A(I) is set to zero as I varies from 1 to N.

PROGRAM LISTING

Overlay programs and user library are listed in order as previously shown in the section "Names of Programs and Subroutines."

```
CVERLAY(VORTEX,0,0)
      PERSON TEABTR(INDUT=502, GUTPUT, TAPE1, TAPE2, TAPE3, TAPE4,
                      TAPES = INPUT, TAPE 6=OUTPUT, TAPE7, TAPE8)
     1
f ** * * * * *
      PERGRAM
                TEA378
      PUPPCSE
                TO CALL VARIOUS OVERLAYS TO PERFORM THE FOLLOWING TASKS
                (1) FEADING THE INPUT DATA AND SETTING UP SECMETRY DEFINE
                -TION.
                (2) GENERATING AIC MATRIX BY AN ADVANCED PANEL-TYPE METHO
                (3) SOLVING SYSTEM OF FOUNTIONS WITH THE GENERATED ALC TO
                OBTAIN INITIAL DOUBLET DISTRIBUTIONS,
                AND TO USE THE POUTING ITELOW TO FIND AN ITERATIVE SOLU-
                TION OF THE FLOW PROBLEM WITH NONLINEAR BOUNDARY CONDI-
                TITNS.
      SUBFICUTINES
                TNPUT(JVERLAY-1,C),AICSEM(QVERLAY-2,O),SOLVERLOVERLAY-3,C
      CALLED
                1. OUTPUT (OVEFLAY-4.0), ITELOW
Ç.
C
      DISCUSSION SEE PROGRAM DOCUMENT 1.3 DESCRIPTION AND FLOW CHART OF
                OVERLAY PROGRAMS.
C *** * ** *
              /CMO3/NTSIN, MTSOUT, NTGD, NPIF, NAIC3, NAIC, NJAC, NSCF
      COMMON
      COMMON/BDYCS/D7C(6,125),7CF(125),7DC(125),IZC(125,2)
      COMMON/INDEX/DN(3,7), DN4(10,4), NNETT, NPANT, NSNGT, NCTRT, NZMPT
      COMMON /MSPNTS/ZM(3,175),ZL(75)
      COMMON/FLATP/NFLTP
      COMMON/FSVEL/FSV(3), FSVM, ALPHA, XPITCH, FCHORD
      CCMMON/SYMM/NSYMM
      COMMON /NEOS/NE, NR, NMAT, NPHS
      COMMON INFAUINED, NE, NO
      COMMON /NITE/NEUN, JT, ITMX, KIT, ITPRIN
      COMMON /SOLN/S(125), ZA(75)
      COMMON /ADR/RTD.DTP
      COMMON /IPFINT/IPMPUT.IPGEOM.IPSING.IPCNTF.IPEIVC.IPOUTE
      DIMENSION X(130), RX(130), DX(130), Y(130), PY(130)
                              CONSTANTS FOR CONVERTING RADIAN TO DEGREE
C.
                               AND VICE VERSA
C.
      PTD = 57.29577951
                             DTR = .0174532925
                               SETS DISK FILE NUMBERS
С
      NTSIN = 5
                     NTSOUT = 6
                  $
      NTGD = 1
                 $NPIF = 2
      NAIC3 = 3
                 $ NAIC = 4
                 $ NSCR = 8
      NJAC = 7
                               SETS PRINTING CODES FOR INTERMEDIATED
C
                               PESULTS, = 1 FOR PRINTOUT $ = 0 OTHERWISE
C
      tPNPUT = 0 	 s 	 IPDUTP = 0
      IPGECM = IPSING = IPCNTH = IPEIVC = 0
                              CALLS OVERLAY(1.0) TO SET UP NETWORK
\mathbf{c}
C
                               INDICES AND CORNER POINTS
      CALL OVERLAY(6HVORTEX,1,0)
```

```
CALLS OVERLAY(2,0) TO GENERATE
(
ſ
                              VELOCITY COMPONENTS AND AIC MATRIX
      MEUN = 0
      CALL OVERLAY(6HVORTEX.2.0)
                              OBTAINS INITIAL VALUES FOR DOUBLET
C
C
                              PARAMETERS BY SOLVING SYSTEM OF EQUATIONS
C
                              WITH AIC MATRIX
      FEWIND NTGD
      NE = NCTRT S NR = 1
      DO 10 JC=1.NCTRT
   10 WRITE(NTGD) ZCR(JC)
      NMAT = NAIC & NRHS = NTGD
      CALL OVEPLAY(6HVORTEX, 3, 0)
      FEWIND NEHS
      READ(NRHS) (S(I).I=1,NSNGT)
      IF(ITMX.NE.0) GO TO 15
                              DISPLAYS INITIAL DOUBLET DISTRIBUTION,
C
C
                              POSITION OF FREE SHEET, VELOCITY COMPONENT
\mathbf{C}
                              AND DELTA OF WHEN NO ITERATION IS REQUESTED
      NEUN = 100 	 $ IPOUTP = 1
      CALL OVERLAY(6HVORTEX,4,0)
      GO TO 40
                          ITERATIVE SOLUTION
(
   15 CONTINUE
      IPNPUT = 0 $
                      IPCUTP = 0
      IPGEEM = IPSING = IPCNTR = IPEIVC = 0
                              STORES INITIAL GUESSES (DOUBLET PAGAMETERS
C.
                              FXCLUDING THOSE AT EDGES AND ANGLES)
C
      00 20 I=1.NF
   20 Y(I) = S(NEQ+I)
      DO 30 1=1,NG
   30 X(NF+T) = ZA(I) *PTD
      M = NF + NG
     - CALL ITELOW(X, N, PX, DX, Y, PY)
   40 CONTINUE
      END
```

```
SUBFOUTINE AJGEN(X,N)
C *****
Ċ
      SUPPOUTINE AUGEN
C
C
      PHEPESE
                TO OBTAIN THE ANALYTIC JACOBIAN FOR PERTURBATION VARIABLE
C
                -S (DOUBLET PAPAMETERS EXCLUDING THOSE AT EDGES AND ANGLE
C
                -S) ASSUMING D(AIC)/D(THETA) = 0
C
ŗ
      INPUT
                CALLING SEQUENCE
                X - ARRAY OF VALUES FOR THE VARIABLES
C
C
                N - NUMBER OF VARIABLES
C
                COMMON BLOCK
C
                /INDEX/ - NM,NN,N7
r
                /MSPNTS/ - ZM
C
                /ADR/ - DTR
C
C
      CUTPUT
                COMMON BLOCK
Ç
                /SOLN/ - S.ZA
C
C
      SUBPCUTINES
Ċ
      CALLED
               DEGMU, DEGDT
0
C
      DISCUSSION THE ROUTINE STORES VALUES OF DOUBLET PARAMETERS(EXCLUD
                -ING THOSE AT EDGES! AND ANGLES IN ARRAY S AND ZA PESPEC-
C
                TIVELY. ROUTINES ARE CALLED TO GENERATE THE PARTIAL DERI-
                VATIVES OF FUNCTIONS F AND G WITH RESPECT TO DOUBLET
                PAPAMETERS MU EXCLUDING THOSE AT EDGES (DEGMU) AND ANGLES
                THETA (DEGDT)
C *****
      DIMENSION X(1)
      COMMON/INDEX/NT(9),NM(9),NN(9),NP(9),NS(9),NC(9),NZ(9),
     CMPA(10), NSA(10), NCA(10), NZA(10), NNETT, NPANT, NSNGT, NCTPT, NZMPT
      COMMCN /MSPNTS/ZM(3,175),ZL(75)
      COMMON /NEAJ/NEQ.NE.NG
      COMMON /SOLN/S(125).ZA(75)
      COMMON /ADF/FTD.DTF
      DO 10 I=1.NF
   IC S(NEQ+I) = X(I)
      DO 20 1=1,NG
   20 \text{ ZA(I)} = \text{X(NF+I)*DTF}
                          DETAINS PARTIAL DEPIVATIVES WORLD. MU
C
      CALL DEGMU
                          DRIAINS PARTIAL DERIVATIVES W.P.T. THETA
Ç
      NZMP = NZ(1) + 1
      CALL DEGDT(ZM(1,NZMP),NM(2),NN(2))
      PETURN
      END
```

```
SUBPOUTINE DEGDT (ZM, NM, NN)
( ** * * * *
\mathbf{C}
      SUBROUTINE DEGDT
C
\boldsymbol{\Gamma}
      PUFPCSF
                TO CALCULATE PARTIAL DERIVATIVES OF FUNCTIONS F AND G
                WITH RESPECT TO PANEL INCLINATION ANGLES OF FREE SHEET
^
                \DeltaSSUMING D(AIC)/D(THETA) = 0
C
                CALLING SEQUENCE
      INPUT
C
                ZM - COORDINATES OF CURNER POINTS OF FREE SHEET NETWORK
                NM - NUMBER OF SPANWISE CUTS OF NETWORK
C
                NN - NUMBER OF TRANSVERSE CUTS OF NETWORK
                COMMON BEOCK
C
                /CM03/ - NSCP
                /BDYCS/ - ZC
                /FSVEL/ - FSV
                /NEAJ/ - NEQ.NE.NG
                /ADF/ - DTR
C
C
      CUTPUT
                COMMON BLOCK
                JOHOS/ - NUAC
r
      SUBSCUTINES
      CALLED
                PTRNS, CROSS, UVECT, VIP, UNIPAN, MMULT
      DISCUSSION A DETAIL DISCUSSION OF THE FORMULA USED IN THE COMPUTA
                -TICM IS GIVEN IN ENGINEERING DOCUMENT (SEE APPENDIX -
                GEOMETRY UPDATE COEFFICIENTS). THE ROUTINE FIRST FINDS A
C
                NORMAL VECTOR N FOR THE PANEL. IT THEN COMPUTES PARTIAL
                DEPIVATIVES OF N WITH RESPECT TO ANGLE THETA. AND FORMS
C
                PARTIAL DERIVATIVES OF N.V AND OF PRESSURE JUMP WITH RES-
                PECT TO THETA. FINALLY IT STORES ALL PARTIAL DEPIVATIVES.
                IN PROPER POSITION OF THE JACOBIAN.
C *****
              /CMO3/NTSIN,NTSDUT,NTGD,NPIF,NAIC3,NAIC,NJAC,NSCR
      COMMON/BDYCS/ZC(3,125),ZCC(3,125),ZCR(125),ZDC(125),IZC(125,2)
      COMMON/PANDQ/CP(3,4),PC(3),PC(3),AR(3,3),ART(3,3),P(2,4),DUM(3),
     CC(6,6),AST(6,16),TIS(16),INS,ITS,NPDQ
      COMMON/FSVEL/FSV(3), FSVM
      COMMON /PINOX/KO.KO.NPWR.NPRD
      COMMON /NEAJ/NEO.NE.MG
      COMMON /SOLN/S(125),ZA(75)
      COMMON /EEOS/EMUE(2500), EMU(3750), IPR(50)
      COMMON / ADR/PTD, DTP
      DIMENSION ZM(3.NM.NN)
      DIMENSION 4(3),9(3),0ADT(3),0BDT(3),0N1(3),9N2(3)
      DIMENSION CN(3), W(3), GMU(3), DNDTH(3)
      DIMENSION DNVDTH(50), DCPDTH(50), AJ(130)
      FOUTVALENCE (DNVDTH.EMUE), (CCPDTH.EMUE(101)), (AJ.EMU)
      FOUTVALENCE (X, M(1)), (Y, W(2))
      FEWIND NSCR
      REWIND NJAC
```

```
PEWIND NTGD
       NFG = NF + NG
       NEW = NF - NG
C
                            PROVIDES ZERO FOR D(AIC)/D(THETA)
(
      DO 310 J=1.NG
C 310 AJ(NF+J) = 0.
      CALL ZERO(AJ(NF+1),NG)
      DO 320 I=1, NEW
       READ(NSCR) (AJ(J),J=1,NF)
      WRITE(NJAC) (AJ(J), J=1.NFG)
  320 CONTINUE
       KQ = 0
      FEWIND NPIF
                     $ NPRD = NPIF
       IPL = NFW
      DADT(1) = DBDT(1) = 0.
       NMM1=NM-1
       NNM1 = NN - 1
      DO 200 MP=1.NNM1
       DO 200 TP=1.NMM1
       ITH=C
       IPL = IPL + 1
      CALL PTRNS(IPL)
ŗ
                            CALCULATES CROSS PRODUCT OF VECTORS A AND E
                            TO FORM AN UNIT NORMAL VECTOR
      09 65 I=1.3
       ABE=ZM(I,IP,MP)-ZM(I,IP+1,MP+1)
       \Delta BM = ZM(I, IP+1, MP) - ZM(I, IP, MP+1)
       \Delta(I) = \Delta BE + \Delta BM
   65 B([]=ABE-ABM
       CALL CROSS(A,B,CN)
       SN=SCPT(CN(1) **2+CN(2) **2+CN(3) **2)
      CALL UVECT(CN)
      CALL VIP(CN.1, FSV.1.3, VL3)
      TVL3 = 2.*VL3
Ç
                            CALCUALTES GRAD(MU)
      TSC2 = 0. $ TSC3 = 0.
      CALL UNIPAN(AP, RC, ZC(1, NEQ+IPL), W)
      DO 90 IC=1. INS
      IS = IIS(IC)
      DX = \Delta ST(4, IC) *X + \Delta ST(5, IC) *Y
      DY = AST(5, IC) *X + AST(6, IC) *Y
      DSDES2 = AST(2,IC) + DX
      DSDFS3 = AST(3,IC) + CY
      TSC2 = TSC2 + OSDFS2*S(IS)
      TSC3 = TSC3 + DSDFS3 * S(IS)
   90 CONTINUE
      W(1) = TSC2 + W(2) = TSC3
                                            W(3) = 0.
      CALL MMULT(ART, W, GMU, 3, 3, 1)
C
                           STARTS TO CALCUALTE D(N.V)/DTHETA AND
C .
                           D(V.GRAD(MU) 1/DTHETA
      00 100 NP=1.NNM1
      DO 100 JP=1.NMM1
```

```
ITH=ITH+1
      IF(JP-IP)10,10,30
C
                           THETA INBOARD OF PANEL OUTBOARD EDGE
   10 IF(NP-MP+1)30,40,20
C
                           THETA AFT OF PANEL L.E.
   20 IF(NP-MP)30.50.30
C.
                           SETS D(N_{\bullet}V)/DTHETA = 0 AND
C
                           D(V \cdot GPAD(MU))/DTHETA = 0
   30 DNVDTH(ITH)=0.
      DCPDTH(ITH) = J.
      GO TC 100
                           THETA AT PANEL L.E.
Ç
   40 DADT(2)=ZM(3,JP,MP)-ZM(3,JP+1,MP)
      DADT(3)=ZM(2,JP+1,MP)-ZM(2,JP,MP)
      IF(JP-IP)44,45,44
   44 DBDT(2)=DBDT(3)=0.
      DADT(2) = DADT(2) + DADT(2)
      DADT(3) = DADT(3) + DADT(3)
      GO TE 60
   45 DBDT(2) = ZM(3,JP+1,MP) - ZM(3,JP,MP)
      DRDT(3) = ZM(2,JP,MP) - ZM(2,JP+1,MP)
      GO TO 60
                           THETA AT PANEL T.E.
   50 PART(2) = ZM(3, JP+1, MP+1) - ZM(3, JP, MP+1)
      DADT(3)=ZM(2,JP,MP+1)-ZM(2,JP+1,MP+1)
      IF(JP-IP)54,55,54
   54 DBDT(2)=DBDT(3)=0.
      DADT(2)=DADT(2)+DADT(2)
      DADT(3) = DADT(3) + DADT(3)
      GD TC 60
   55 DBDT(2)=ZM(3,JP+1,MP+1)-ZM(3,JP,MP+1)
      DBDT(3) = ZM(2,JP,MP+1) - ZM(2,JP+1,MP+1)
   60 CALL CROSS(DADT, B, DN1)
      CALL CROSS(A,DBDT,DN2)
      DO 70 I=1.3
   70 DNDTH(I)=DN1(I)+DN2(I)
      CALL VIP(CN.1, DNDTH.1,3, DNTHL3)
      DO 80 I=1.3
   80 DMDTH(I) = (DNDTH(I) - DNTHL3*CN(I))/SN
                              FORMS D(N.V)/DTHETA
C
      CALL VIP(DNDTH,1,FSV,1,3,DNVDTH(ITH))
      DNVDTH(ITH) = DNVDTH(ITH)*DTR
                              CALCULATES DIDELTA CPI/DIHETA
      CALL VIP (GMU, 1, DNDTH, 1, 3, GMUDN)
      DCPDTH(ITH) = -TVL3*GMUDN
      DCPDTH(ITH) = DCPDTH(ITH) * DTR
  100 CONTINUE
      PEAD (NSCR)
                   (AJ(J),J=1,MFI
      WRITE(NJAC) \{AJ(J),J=1,NF\},\{DCPDTH(J),J=1,ITH\}
      WRITE(MTGD) (DNVDTH(J),J=1,ITH)
  200 CONTINUE
                           STORES ALL PARTIAL DERIVATIVES IN PROPER
C
```

```
POSITION OF THE JACOBIAN
```

```
REWIND NTGD
DD 4CO I=1,NG
READ(NSCR) (AJ(J),J=1,NF)
FAD(NTGD) (DNVDTH(J),J=1,NG)
WPITE(NJAC) (AJ(J),J=1,NF),(DNVDTH(J),J=1,NG)
400 CONTINUE
FETURN
END
```

C

```
SUBRCUTINE DEGMU
( * * * * * *
C
      SUBROUTINE DEGMU
C
                TO CALCULATE PARTIAL DERIVATIVES OF FUNCTIONS F AND G
C
      PURPESE
                WITH RESPECT TO DOUBLET PARAMETERS (EXCLUDING THOSE AT
C
ŗ
                EDGES )
C
C
      INPUT
                COMMON BLOCK
C
                /CMO3/ - NPIF, NAIC3
                /BDYCS/ - 70
C
C
                /INDEX/ - NSNGT
                /FSVEL/ - FSV
C
                /NFAJ/ - NEO,NF,NG
C
                /SOLN/ - S
ŗ
C
                /EEQS/ - EMUE, EMU, TPR
C
                COMMON BLOCK
C
      DUTPUT
C
                /CMC3/ - NSCR
C
C
      SUBRCUTINES
C
      CALLED
                BSUBSM, PTRNS, MMULT, UNIPAN, VIPS
Ç
      DISCUSSION. THE FORMULA AND NOTATION USED HERE ARE DISCUSSED IN DE
C
                -TAIL IN ENGINNERING DOCUMENT (SEE APPENDIX - DOUBLET ST-
                RENGTH UPDATE COEFFICIENTS). THE ROUTINE READS IN DEFEMUE
                AND DE/DMU AND CALCULATES (DF/DMUE)(-1)*(DE/DMU) WHERE E
C
                IS THE FUNCTION CONSISTING OF ONLY THOSE EQUATIONS CORRES
                -PONDING TO CONTROL POINTS AT EDGES. THEN IT OBTAINS PAR-
€
                TIAL DERIVATIVES OF N.V ON WING AND ON FREE SHEET WITH
C
                PESPECT TO DOUBLET PARAMETERS. PARTIAL DERIVATIVES OF PRE
C
                -SSURE JUMP V.GPAD(MU) WITH RESPECT TO DOUBLET PARAMETER
C
                ARE ALSO CALCULATED. FINALLY, PARTIAL DERIVATIVES WITH RE
C
C
                -SPECT TO DOUBLET PARAMETERS EXCLUDING THOSE AT EDGES APE
                FORMED.
C
U ****
      COMMEN /CMO3/NTSIN,NTSOUT,NTGD,NPIF,NAIC3,NAIC,NJAC,NSCP
      COMMON/BDYCS/ZC(3,125),ZCC(3,125),ZCR(125),ZDC(125),IZC(125,2)
      COMMON/INDEX/DN(9,7), DNA(1C,4), NNETT, NPANT, NSNGT, NCTPT, NZMPT
      COMMON/PANDQ/CP(3,4),PC(3),PC(3),AR(3,3),ART(3,3),P(2,4),A,B,DIAM,
     CC(6,6), AST(6,16), IIS(16), INS, ITS, NPDQ
      COMMON/FSVEL/FSV(3), FSVM
      COMMON /PINC/DVDFS(3,125)
      COMMON /PINDX/KP.KQ.NPWR.NPRD
      COMMON /NEAJ/NEQ.NE.NG
      COMMON /SOLN/S(125).ZA(75)
      COMMON /EEQS/5MUE(2500), EMU(3750), IPR(50)
      DIMENSION VL(3), FSVL(3), W(3), DSDFS2(16), DSDFS3(16)
      DIMENSION FGMUE(50), AJ(100)
      FQUIVALENCE (X,W(1)),(Y,W(2)),(FGMUF,IPR),(AJ,EMUE)
                          CALCULATES DE = (DE/DMUE)(-1)*(DE/DMU)
\mathbf{C}
                          USING EMUE AND EMU FROM SUBROUTINE FGCAL
```

 \mathbf{C}

```
CALL RSUBSM(EMUE.NEQ.NEQ.IPR.EMU.NF)
      DALM CHIWSA
      REWIND NITGO
      KQ = 0
      PEWIND NPIF & NPPD = NPIF
      FEWIND NAIC3
C
                          SKIPS FIRST NEO RECORDS CORRESPONDING TO
                          CONTROL POINTS AT EDGES
      DO 10 I=1,NEQ
   10 FEAD(NATC3) DVDFS(1)
      MFW = MF - NG
      DO 100 IJ=1.NF
      IP = IJ
      CALL PTENS(IP)
      PEAD(NAIC3) DVDFS
      DO 30 J=1.NSNGT
      CALL MMULT(AR, DVDFS(1,J),W,3,3,1)
      nn 20 I=1,3
   20 DVDFS(I \cdot J) = W(I)
   3G CONTINUE
      IF([J.GT.NFW]
                      GO TO 40
C
                          STORES D(N.V) ON WING
      WRITE(NJAC) (DVDFS(3,J),J=1,NSNGT)
      GO TO 100
                          STORES D(N.V) ON FREE SHEET
C
   40 CONTINUE
      WPITE(NTGD) (DVDFS(3.J).J=1.NSNGT)
ſ
                          CALCULATES D(V.GRAD(MU)) ON FREE SHEET
      CALL MMULT(DVDFS,S,VL,3,NSNGT,1)
      CALL MMULT(AP, FSV, FSVL, 3, 3, 1)
      DO 50 I=1,3
   50 VL(I) = VL(I) + FSVL(I)
      TSC2 = 0. $ TSC3 = 0.
      CALL UNIPAN(AR, RO, ZC(1, NEQ+IJ), W)
      DC 60 IC=1.INS
      IS = IIS(IC)
      DX = AST(4,IC)*X + AST(5,IC)*Y
      DY = \Delta ST(5, [C) + X + \Delta ST(6, [C) + Y
      DSDFS2(IC) = AST(2,IC) + DX
      DSDFS3(IC) = AST(3,IC) + DY
      TSC2 = TSC2 + DSDFS2(IC)*S(IS)
      TSC3 = TSC3 - DSDFS3(IC)*S(IS)
   60 CONTINUE
      DO 70 IS=1,NSNGT
   70 DVDFS(1, IS) = 2.*(TSC2*DVDFS(1, IS) - TSC3*DVDFS(2, IS))
      DP 80 IC=1. INS
      IS = IIS(IC)
   80 DVDFS(1, IS) = DVDFS(1, IS)
                    + 2.*(VL(1)*DSDFS2(IC) + VL(2)*DSDFS3(IC))
      WRITE(NJAC) (DVDFS(1,J),J=1,NSNGT)
  100 CONTINUE
C
                          FORMS (DF/DMU) - (DF/DMUE)*DE
```

```
PEWIND NJAC
      REWIND NSCP
      00 130 I=1.NF
      READ(NUAC) (FGMUE(J), J=1, NEQ), (AJ(J), J=1, NE)
      00 120 J=1.NF
      JN1 = (J-1)*NEQ+1
  12C CALL VIPS(FGMUE.1.EMU(JN1),1.NEQ.AJ(J))
      WRITE(NSCR) (AJ(J), J=1, NF)
  130 CONTINUE
                            FORMS (DG/DMU) - (DG/DMUE) *DE
C
      FEWIND NTGD
      00 150 I=1.NG
      FEAD(NTGD) (FGMUE(J), J=1, NFQ), (AJ(J), J=1, NF)
      00 140 J=1,NF
      J^{\dagger \dagger 1} = (J-1) * M = Q + 1
  140 CALL VIPS(FGMUE, 1, EMU(JN1), 1, NEQ, AJ(J))
      WRITE(NSCR) (AJ(J),J=1,NF)
  150 CONTINUE
      FETUPN
      END
```

SUBPOUTINE EGCAL (EVZ.GVZ) · ***** C SUBPCUTINE FSCAL C ŗ PURPOSE TO SOLVE FOR DOUBLET PARAMETERS AT EDGES AND TO CALCULATE C FUNCTIONS F AND G (INPUT COMMON BLOCK C /CMO3/ - NPIF.NAIC3.NAIC /BDYCS/ - ZC.ZCF /FSVEL/ - FSV /NFAJ/ - NEQ.NF.NG C /SOLN/ - S C OUTPUT CALLING SEQUENCE FVZ - VALUES OF F GVZ - VALUES OF G -C COMMON BLOCK /EEOS/ - EMUE, EMU, IPR SUBPCUTINES CALLED VIPS.LINECS.PTRNS, MMULT. VIP. UNIPAN DISCUSSION. THE POUTINE READS FOWS OF AIC MATRIX TO FORM COEFFI-CTENTS OF FUNCTION E. THE SOLUTION FOR DOUBLET PARAMETERS C (MUE) AT EDGES ARE FOUND BY USING FUNCTION E AND GIVEN C VALUES OF ALL OTHER DOUBLET PARAMETERS (MU). SINCE E IS A FUNCTION OF COUBLET PARAMETERS ONLY, DE/DMUE C AND DEIDMU ARE SIMPLY THE COFFFICIENTS OF E. IF THE MATRIX DEFOMUS C IS SINGULAR, AN ERROP MESSAGE WILL BE PRINTED AND THE EX-ECUTION OF THE COMPUTER SPAGRAM WILL BE TERMINATED. C COMPONENTS OF INFLUENCE COFFFICIENTS ARE READ IN AND MUL-TIPLIED BY VALUES OF DOUBLET PARAMETERS TO FORM PERTURBA-TION VELOCITY. THE LATTER IS ADDED TO FREE STREAM VELC-CITY TO BECOME THE AVERAGE VELOCITY VECTOR V. THE DOT PPO -DUCT N.V IS THEN CALCULATED FOR EVERY INTERIOR CONTROL POINT ON WING (FORMING PART OF FUNCTION F) AND ON FREE SHEET (FORMING FUNCTION G). THE JUMP IN PRESSURE COEFFICIENTS V.GRAD(MU) (SEE ENGIN-C FERING DOCUMENT) ON FREE SHEET IS ALSO CALCULATED (FORM-ING THE OTHER PART OF FUNCTION F). (*** ** DIMENSION FVZ(1), GVZ(1) COMMON /CMO3/NTSIN,NTSOUT,NTGD,NPIF,NAIC3,NAIC,NUAC,NSCF : S COMMON/BDYCS/ZC(3,125),ZCC(3,125),ZCR(125),ZDC(125),IZC(125,2) COMMON/INDEX/DN(9,71,DNA(IC,41,NNETT,NPANT,NSNGT,NCTRT,NZMPT COMMON/PANDQ/CP(3.4).PC(3).PO(3).AP(3.3).ART(3.3).P(2.4).A.B.DTAM. CC(6.6), AST(6.16), HIS(16), INS, HTS, NPDQ COMMON/FSVEL/FSV(3),FSVM

COMMON /PINC/DVDES(3,125)
COMMON /PINDX/KP.KC.NPWP.NPPD

COMMON /NEAJ/NEQ.NE.NG

```
COMMON /SQLN/S(125),7A(75)
      COMMON /EEQS/EMUE(2500), FMU(3750), IPR(50)
      DIMENSION VG(3), VL(3), W(3)
      EQUIVALENCE (X,W(1)),(Y,W(2))
\Gamma
                               SOLVES FOR EDGE DOUBLETS BY USING
C
                               FUNCTION E AND GIVEN VALUES OF ALL
C
                               OTHER DOUBLETS
      PEWIND NAIC
      00 30 I=1.NEQ
      IM = I - NEQ
   30 FEAD(NAIC) (EMUE(J*NEO+IN), J=1, NEQ), (EMU(J*NEO+IN), J=1, NF)
      ME01 = NEO + I
      09 40 I=1,NEQ
      S(I) = ZCR(I)
   40 CALL VIPS(EMU(I), NEQ, S(NEQ1), 1, NF, S(I))
      CALL LINEGS (EMUE, NEQ, NEQ, IPR, S, 1, D1)
      1F(D1.NE.C.) GD TD 50
      PPINT 10C1
 1001 FORMAT(/* (DE/DMUE) APPEARS SINGULAR*)
      STOP
   50 CONTINUE
C
                               STARTS TO CALCULATE FUNCTIONS F AND G
      KQ = 0
      REWIND NPIF $ NPPD = NPIF
      REWIND NAICS
C
                               SKIPS FIRST NEO RECORDS CORRESPONDING TO
                               CONTROL POINTS AT EDGES
      DO 60 I=1.NEQ
   60 READ(NAIC3) DVDFS(1)
      NFW = NF - NG
      DO ICC [J=1.NF
      IP = IJ
      CALL PTPNS(IP)
      FEAD(NAIC3) DVDES
      CALL MMULT(DVDFS.S.VG.3, NSNGT.1)
      DO 70 I=1.3
   7C VG(I) = VG(I) + FSV(I)
      IF(IJ.GT.NFW) GO TO 80
                               CALCULATES N.V DN WING
\mathbf{C}
      CALL VIP(AR(3),3,VG,1,3,FV7(IJ))
      OF TO 100
                               CALCULATES N.V ON FREE SHEET
C
   8C TG = TJ - NFW
      CALL MMULT(AP, VG, VL, 3, 3, 1)
      GVZ(TG) = VL(3)
                              CALCULATES V.GRAD(MU) ON FREE SHEET
C
      TSC2 = 0. $ TSC3 = 0.
      CALL UNIPAN(AR, PO, ZC(1, MEQ+IJ), W)
      00 90 IC=1, INS
      IS = IIS(IC)
      DX = AST(4,IC)*X + AST(5,IC)*Y
      DY = AST(5, IC) *X + AST(6, IC) *Y
```

```
DSDFS2 = AST(2,IC) + DX

DSDFS3 = AST(3,IC) + DY

TSC2 = TSC2 + DSDFS2*S(IS)

TSC3 = TSC3 - DSDFS3*S(IS)

90 CONTINUE

FV7(IJ) = 2.*(TSC2*VL(1) - TSC3*VL(2))

100 CONTINUE

PFTUPN

FND
```

```
SUBPOUTINE FUNC(X,N,RX)
C****
       SUBPOUTINE FUNC
C
C
                TO EVALUATE FUNCTION F (N.V ON WING AND V.GRAD(MU) ON
       PUPPESE
Ç
                FREE SHEET) AND G (N.V ON FREE SHEET)
C
                CALLING SEQUENCE
       IMPUT
C
                X - ARRAY OF VALUES FOR THE VARIABLES
                N - NUMBER OF VARIABLES
                COMMON BLOCK
                /NFAJ/ - NEG.NF.NG
                /NITF/ - NFUN
                /SOLN/ - ZA
                /ADF/ - DTF
Ç
       OUTPUT
                CALLING SEQUENCE
                RX - ARRAY OF VALUES OF FUNCTIONS
C
0
C
       SUBFCUTINES
C
                UPDATE, AICGEN(DVERLAY-2,0), FGCAL
      CALLED
\Gamma
       DISCUSSION THE ROUTINE STORES VALUES OF DOUBLET PARAMETERS, (EX-
                CLUDING THOSE AT EDGE! AND ANGLES IN ARRAYS S AND ZA
C
                RESPECTIVLEY. IT USES NEW ANGLES TO UPDATE THE CORNER
C
                POINTS OF FREE SHEET, FED SHEET AND PART OF THE WAKE NET-
                WORK. AICGEN(OVERLAY-2,0) IS THEN CALLED TO DESIGNATE LO-
C
                CATIONS OF DOURLETS AND CONTECT POINTS AND TO GENERATE
C
                VELOCITY COMPONENTS AND AIC MATRIX USING THE UPDATED CORN
                -ER POINTS. IF PRETURBATION IN ANGLE IS NOT SIGNIFICANT
                UPDATE AND AIGGEN ARE SKIPPED. FINALLY, THE FOUTINE CALLS
                FGCAL TO CALCULATE VALUES OF FUNCTIONS F AND G.
C *****
       DIMENSION X(1) +RX(1)
       COMMON /NEAJ/NEQ.NE.NG
       COMMON /NITE/NEUN.JT.ITMX.KIT.ITPRIN
       COMMON /SOLN/S(125),ZA(75)
       COMMEN /ADR/PTD.DTP
      DO 10 I=1.NF
   10 S(NEC+I) = X(I)
       SUM = 0.
       DO 20 I=1.NG
       XDTR = X(NE+I)*DTF
      DZ\Delta = ZA(I) - XDTR
      SUM = SUM + DZA#DZA
   20.74(T) = XDTR
       IF(NFUN.EQ.0) GO TO 30
       IF(SUM.LE.1.0E-30) GO TO 40
       PRINT ICCI. SUM
C1001 FORMAT(/* SUM OF SOUARES OF CHANGES IM ANGLES (RAD.) =*.F14.6)
C
                              UPDATES COPNER POINTS
Ċ
```

CALL UPDATE

OBTAINS VELOCITY COMPONENTS AND AIC MATRIX

30 CONTINUE
CALL GVERLAY(6HVORTEX,2.0)

C GETS VALUES OF FUNCTIONS F AND G

40 CONTINUE
CALL FGCAL(FX.RX(NF+1))
PETURN

END

SUBFOUTINE ITFLOW(X,N,RX,DX,Y,RY) (***** SUBPOUTINE ITELOW C Ç C PHPOCSE TO PERFORM ITERATIVE SCHEME USING QUASI-NEWTON ALGORITHM ۲, FOR THE SOLUTION OF A SET OF NONLINEAR EQUATIONS INPUT CALLING SECUENCE X - ARRAY OF INITIAL VALUES FOR THE VARIABLES C N - NUMBER OF VARIABLES C DX.Y.RY - SCRATCH AFRAYS COMMON BLOCK C /NFAJ/ - NEQ.NF C /NITE/ - ITMX, ITPRIN Ç (C OUTPUT CALLING SEQUENCE X - ARRAY OF SOLUTION VECTOR PX - ARRAY OF PESIDUAL VECTOR Ç SUBFRUTTNES C VIP-FUNC-CUTPUT(OVERLAY-4.0).AJGEN.SOLVER(OVERLAY-3.0) CALLED DISCUSSION. THE ROUTINE CALLS FUNC TO EVALUATE RESIDUALS EX AND CALLS AUGEN TO SET UP THE JACOBIAN AU. THE SYSTEM OF BOUA -TIONS AJ \pm DX = -PX IS SOLVED AND A NEW APPROXIMATE SOLU-TION IS FOUND USING COFFECTIONS DX. RESIDUALS AND JACOBI-C AN ARE EVALUATED AT THE NEW SOLUTION. THE PROCEDURE IS RE -PEATED UNTIL THE SUM OF SQUARES OF PESIDUALS SATISFIES A C PREDETERMINED TOLERANCE TOL OR THE GIVEN MAXIMUM NUMBER C OF ITERATIONS ITMX IS REACHED. THE ROUTINE INCLUDES & PRO C -CEDURE OF GENERATING NEW ALC AFTER EVERY KIT ITERATIONS. C THE JACOBIAN WILL BE CALCULATED BY CALLING AJOFN ONLY WHEN NEW AIC IS GENERATED. OTHERWISE. IT WILL BE UPDATED C BY USING A FORMULA OF QUASI-NEWTON SCHEME (SEE FNGINEER-Ç. ING DOCUMENT). NUMBER OF ITERATION, SUM OF SQUAFES OF RE-SIDUALS AND STEP SIZE ARE PRINTED FOR EVERY ITPRIN ITERA-C TIONS. FOR ITERATION STUDY AND CHECK OUT PURPOSE. SOME C OTHER INTERMEDIATE PRINT STATEMENTS ARE INCLUDED (SEE C C LISTINGI. · ***** DIMENSION X(1), RX(1), DX(1), Y(1), RY(1) /CMC3/NTSIN,NTSOUT,NTGD,NPIF,NAIC3,NAIC,NJAC,NSCF COMMON /NEQS/NE, NP, NMAT, NPHS COMMON /NFAJ/NEQ.NE.NG COMMEN /SOLN/S(125).ZA(75) COMMON /NITE/NEUN.JT.ITMX.KIT.ITPGIN DIMENSION AU(130) SETS PRINTING GODE (FOR ITERATION STUDY) C IP = 0

Ç

C

KIT = 5

SETS NO. OF ITERATIONS TO GENERATE NEW AIC

SETS TOLEPANCE FOR CONVERGENCE. AND

```
PERCENTAGE FOR NEWTON STEP
C
      TOL = 1.0E-4
      CAMA = C.1
                              INITIALIZES ITERATION
r
      TSRX = 1.0E50
      IT = 0
   10 \text{ NFUN} = 0
      CALL VIP(X, 1, X, 1, N, SX)
                              CALLS FUNC TO EVALUATE RESIDUALS
C
      CALL FUNC(X,N,SX)
      NFUN = NFUN + 1
      CALL VIP(RX,1,RX,1,N,SRX)
                              CHECKS IF STEP SIZE REDUCTION IS NECESSARY
C
                              AND SETS THE APPROPRIATE CODE
C
      10 = 0
      IF(SFX.LT.TSFX)
                      IC = 1
      TSEX = SEX
                              PRINTS RESULTS FOR EVERY ITPFIN ITFFLTIONS
C
      [F(MCD(IT, ITPRIN).NE.C) GO TO 15
      WEITE(NTSOUT, 5010) IT, SRX
 5010 FORMAT(IH1, * ITERATION NO.*, I4, 9X, *SUM OF SQUARES OF RESTOUALS =*,
     $518.10)
      IF(IT.NE.O) WRITE(NTSOUT,5020)
                                       SADS
      DO 13 I=1,NF
   13 S(NEC+I) = X(I)
      CALL OVERLAY(6HVORTEX, 4, 0)
   15 [F([P.EQ.0] GO TO 18
      PPINT 105
  105 FORMAT(1H1)
      PRINT 101, IT, SRX, NEUN
  101 FORMAT(//# ITERATION NO.*,13,5X,*SUM OF SQUARES OF RESIDUALS =*,F1
     18.10/* NO. OF FUNCTION CALLED =*, 14)
      PRINT 102. (X(I), I=1,N)
  102 FORMAT(/* VALUES OF VARIABLES*/(5E14.6))
      PRINT 103, (RX(I), I=1,N)
  103 FORMAT(/* PESIDUALS*/(5E14.6))
   18 [F(IT.EO.O) GO TO 20
      ITO = IT + I
      IF(ITO.GE.ITMX) GO TO 110
      IF(SEX.LT.TOL) GO TO 110
C
                          TO OBTAIN THE JACOBIAN
   20 CALL AJGEN(X.N)
      00 100 K=1.KIT
€.
C
                          TO SOLVE AJ \neq DX = -PX
      PEWIND NTGD
      00 3C I=1.N
      PXN = -PX(I)
   30 WRITE(NTGD) RXN
                   $ NRHS = NTGD
      NMAT = NJAC
```

```
CALL OVERLAY (6HVOFTEX, 3, 0)
      FEWIND MRHS
      PEAD (NRHS)
                   \{DX\{I\}, I=I, N\}
      IF(K.EQ.1)
                   PRINT 107, (DX(I), I=1, N)
 107 FORMAT(/* CORRECTIONS*/(5814.6))
      CALL VIP(DX.1.DX.1.N.SDX)
C
^
                           DETERMINES THE STEP SIZE
      PXO = SORT(SX/SDX)
      CALFA = AMINICGAMA*RXD.1.1
      FALFA = CALFA
      IH = 0
   40 00 50 I=1.N
      DX(I) = CALFA*DX(I)
   50 Y(T) = X(T) + DY(T)
      PRINT 108, FALFA
C
 108 FORMAT(/* (FRACTION OF NEWTON STEP TAKEN =*.E14.6,*)*)
C
Ç
      PFINT 107, (DX(I), I=1, N)
Ċ
      PRINT 102. (Y(1), I=1, N)
C
                               EVALUATES NEW RESIDUALS
      CALL FUNC(Y,N,RY)
      NFUN = NFUN + 1
      CALL VIP(RY, 1, RY, 1, N, SEY)
      IF(SPY.LT.SRX) GO TO 60
      IF(IC.EQ.1. AND.K. FQ.1) GD TO 60
      IH = IH + 1
      PRINT 106, IH, SRY
C
C 106 FORMATI/15, * CYCLE OF STEP SIZE FEDUCTION*/* SUM OF SQUAPES OF FES
     11DUALS =*,F14.6)
      IE(IE-GE-3) GO TO 60
      CALFA = 0.5
      FALEA = 0.5*FALEA
      GD TO 40
ŗ
C
                               UPDATES THE JACOBIAN
   60 ADS = SDX#FALFA##2
      PADS = 1./ADS
      REWIND NUAC
      PEWIND NSCP
      DO 75 1=1.N
      FEAD(NJAC)
                   (AJ(J),J=1,N)
      CALL VIP(AJ. 1, DX. 1, N, TJD)
      PJD = (RY(I) - RX(I) - TJD) + RADS
      00 70 J=1,N
      \Delta J(J) = \Delta J(J) + RJD*DX(J)
   70 CONTINUE
   75 WRITE(NSCF)
                    (N, l=L, \{L\}, LA)
      MTH=NSCF
      NSCP = NJAC
      NJAC=NTH
```

C

```
C
                          RESETS VALUE OF THE VARIABLES AND THE RESIDUALS
      DO 80 I=1.N
      X(I) = Y(I)
   80 \text{ PX(I)} = \text{RY(I)}
      SFX = SRY
      JT = IT + K
                              PRINTS RESULTS FOR EVERY ITPRIN ITERATIONS
C.
      SADS = SQRT(ADS)
      IF(K.FO.KIT) GO TO 100
     IF(MOD(JT, ITPRIN).NE.O) GO TO 90
      WRITE(NTSOUT,5010) JT,SFX
      WPITE(NTSOUT.5020) SADS
 5020 FORMAT(/* STEP SIZE (LENGTH OF CORRECTION VECTOR) =*.F14.6)
      DO 85 (=1.NE
   85 S(NEC+I) = X(I)
      CALL OVEPLAY(6HVORTEX,4,0)
   90 [F([P.EO.O] GO TO 100
      PRINT 101, JT, SRX, NEUN
      PRINT 104, RXD, FALFA
  104 FORMAT(/* PATIO OF LENGTH OF INITIAL VECTOR TO LENGTH OF FULL NEWT
     ION STEP =*/514.6/* FRACTION OF NEWTON STEP TAKEN =*,514.6)
      PRINT 102, (X(I), T=1,N)
      PRINT 103, (PX(I),I=1,N)
  100 CONTINUE
      IT = IT + KIT
      IF(IT.LE.ITMX) GD TO 10
  110 CONTINUE
      PETUPN
      END
```

```
SUBROUTINE UPDATE
(****
      SUPPCUTINE UPDATE
€
               TO UPDATE CORNER POINTS OF FREE SHEET, FED SHEFT AND THE
      PURPOSE
ŗ
               PART OF WAKE ATTACHED TO THOSE SHEETS
C
      INPUT
               COMMON BLOCK
C
               /INDEX/ - NM.NN.NP.NZ
               /MSPNTS/ - ZM.ZL
C
               /SOLN/ - ZA
      CUTPUT
               COMMON BLOCK
               /MSPNTS/ - 7M
      SUPRCUTINES
C
      CALLED
               NONE
C
C
      DISCUSSION COPMER POINTS ARE UPDATED USING GIVEN VALUES OF ANGLE
C
               AND FIXED CHOPD LENGTH OF PANELS IN TRANSVERSE OUT OBTAIN
C
                -FD PREVIOUSLY IN INPUT(OVERLAY-1.0). IT IS ASSUMED THAT ..
               PANEL CORNER POINTS MOVE ONLY IN TRANSVERSE CUTS.
               THE ROUTINE ASSUMES THAT NM(31=2, NN(41=2, AND NM(5)=
C
               NN(5) = 2.
C
C ****
      CCMMCN/INDEX/NT(9),NM(9).NN(9),NP(9),NS(9),NC(9),NZ(9),
     CMPA(10), NSA(10), NCA(10), NZA(10), NMETT, NPAMT, NSNGT, NCTRT, NZMPT
      COMMON /MSPNTS/ZM(3,175),ZL(75)
      COMMON /SOLN/S(125).ZA(75)
                          UPDATES CORNER POINTS OF FREE SHEET
C
      NZM = NZ(1) + NM2
      DO 100 J=2,NN2
      J2 = J-2
      JA = J2 \pm (NM2 - 1)
      JM = NZM + J2*NM2
      00 \ 100 \ I=2,NM2
      [1] = [-1]
      IA = JA + I1
      IM = JM + II
      ZLP = ZL(IA)
                    5 ZAP = ZA(IA)
      7M(2,TM+1) = ZM(2,TM) + ZLP*COS(ZAP)
      ZM(3,IM+1) = ZM(3,IM) + ZLP*SIN(ZAP)
  100 CONTINUE
                          UPDATES CORNER POINTS OF FED SHEFT
C
                      NZ2 = NZ1 + NZ(2)
      NZ1 = NZ(1)
                   $
      NP2 = NP(2) $
                     NP3 = NP(3)
      DO 200 I=1,NP3
      IM = NZM + I * NM2
      IMN = NZ2 + (2*I+1)
      ZM(2,IMN) = ZM(2,IM)
      ZM(3,IMN) = ZM(3,IM)
```

```
IA = NP2 + I
      ZLP = 7L(IA) $ ZAP = ZA(IA)
      ZM(2.IMN+1) = ZM(2.IMN) + ZLP*COS(ZAP)
      ZM(3.JMN+1) = ZM(3.JMN) + ZLP*SIN(ZAP)
 200 CONTINUE
                         UPDATES FORZEN WAKE ATTACHED TO FREE SHEET
      NM3 = NM(3)    S = NM4 = NM(4)
      NZ3 = NZ2 + NZ(3) $ NZ4 = NZ3 + NZ(4)
      NZMA = NZ2 - NM2
      NZMR = NZ3 + NM4 - NM2
      DO 300 I=2.NM2
      IM = NZMA + I
      IMN = NZMB + I
      ZM(2,IMN+NM4) = ZM(2,IMN) = ZM(2,IM)
      ZM(3,IMN+NM4) = ZM(3,IMN) = ZM(3,IM)
  300 CONTINUE
                         UPDATES FROZEN WAKE ATTACHED TO FED SHEET
•
      NM5 = NM(5)
      NZMC = NZ3 - NM3
      DD 400 I=1,NM5
      IM = NZMC + I
      IMN = NZ4 + I
      ZM(2,IMN+2) = ZM(2,IMN) = ZM(2,IM)
      ZM(3,IMN+2) = ZM(3,IMN) = ZM(3,IM)
 400 CONTINUE
      RETUEN
      END
```

```
PROGRAM INPUT
( * * * * *
      PROGRAM INPUT
C
      PURPOSE
                READ AND ECHO USER INPUT DATA
C
                CALCULATE FREE STREAM VELOCITY
C
                CALCULATE COORDINATES OF ALL PANEL CORNER POINTS
(
                CALCULATE INITIAL LENGTH AND ANGLE OF PANELS ON
C
                  THE FREE VORTEX AND FED SHEET
      INPUT
                DATA CARDS (SEE ENGINEERING DOCUMENT - USER GUIDE)
      CUTPUT
                COMMON BLOCK
                /DAT3/ - AR.NTF,XTF,MSP,YSP,NTC,NLE,YLE,NTE,YTE,MSF
Ç
                /FSVEL/ - FSV.FSVM.ALPHA.XPITCH.FCHORD
                /INDEX/ - NT.NM.NN.NP.NZ.NPA.NZA.NNETT.NPANT.NZMPT
C
                /MSPNTS/ - ZM,ZL
                /SOLN/ - Z4
C
C
C
      SUBPCUTINES
C
      CALLED
                SHEGEN, DWNET, AWNET, GWNET
C
      DISCUSSION SEE PROGRAM DOCUMENT 1.3 DESCRIPTION AND FLOW CHART OF
C
                OVERLAY PROGRAMS.
C *****
               /CMO3/NTSIN,NTSOUT,NTGD,NPIF,MAIC3,NAIC,NJAC,NSCF
      COMMON
      COMMON/INDEX/NT(9).NM(9).NM(9).NP(9).NS(9).NC(9).NZ(9).
     CNPA(10).NSA(10).NCA(10).NZA(10).NNETT.NPANT.NSNGT.NCTRT.NZMPT
      COMMON/MSPNTS/ZM(3,175),ZL(75)
      COMMON /SOLN/S(125).ZA(75)
      COMMON/FLATP/NFLTP:
      COMMON/FSVEL/FSV(3), FSVM, ALPHA, XPITCH, PCHORD
      COMMON/SYMM/NSYMM
      COMMEN / ADR /PTD. DTR
      COMMON /NITE/NEUN.JT.ITMX.KIT.ITPFIN
      COMMON /DAT3/AR, NTP, XTF(10), MSP, YSP(10), NTC, NLE, YLE(10),
                    NTE, YTE(10), MES
      COMMON /IPRINT/IPNPUT.IPGEOM.IPSING.IPCNTP.IPEIVC.IPOUTP
                 ILE(10), ITE(10), YF(15), ZF(15)
      DIMENSION
                  IDICT(14), ICARD(20)
      DIMENSION
      DATA
            NDICT/14/
             IDICT/4H$ALP,4H$ASP,4H$TRA,4H$SPA,4H$CEN,4H$DEL,4H$APF,
      DATA
     1
                   4H$GOT.4H$INP.4H$FRE.4H$PIT.4H$ITE.4H$PRI.4H$END/
                          SETS NSYMM = 1 FOR AXISYMMETRIC
C
                               NSYMM = 0 OTHERWISE
C
      NSYMM = 1
                              SETS NELTP = 1 FOR FLAT PANEL
Ç
C
                                    NELTP = 0 FOR CURVED PANEL
      MFLTF = 1
C
                          PRINTS TITLE AND DATA CARDS
```

OVERLAY(VORTEX,1,0)

C

```
WRITE(NTSOUT, 5010)
 5010 FORMAT(1H1//57X, *A COMPUTER PROGRAM*/65X, *FOR*/42X, *A THREE DIMENS
      IONAL SOLUTION OF FLOWS OVER WINGS*/48X,*WITH LEADING EDGE VOPTEX
     2SEPARATION*////53X.*- LIST OF INPUT DATA CARDS -*)
      NC\Delta FD = 0 $ 1CPP = 42
      IDEND = IDICT(14)
   10 WRITE(NTSOUT,5020)
 5070 FOFMAT(//34x, +NO. +, 4X, +CAPD IMAGES+//).
   20 FEAD(MISIN, 5030) ICARD
 5030 FORMAT(20A4)
      !F(ECF.NTSIN) - 40.30
   30 NCARD = NCARD + 1
      MEITEINTSOUT.50401
                          NCARD. ICARD
 5040 FOPMAT(30X, 16, 5X, 20A4)
      IF(ICARD.EQ.IDEND) GO TO 40
      IF(MCD(NCARD.LCPR).NE.O) GO TO 20
      WRITE(NTSOUT.5050)
 5050 FORMAT(1H1)
      GG TT 10
   40 NBSP = NCARD-3
      DO 50 I=1.NBSP
      PACKSPACE NTSIN
   50 CONTINUE
                          READS INPUT VARIABLES
C
   60 READ (NTSIN, 5030)
                         TCAFD
      IF(EOF.NTSIN) 65.70
   65 WRITE(NTSIN, 5055)
 5055 FORMAT(//* - END OF FILE ENCOUNTERED - */* - END CARD ASSUMED PROC
     IESSING WILL CONTINUE*1
      GO TO 220
   70 00 80 160=1.NDICT
      IF(ICAPD.EQ.IDICT(IGD))
                                GO TO 90
   SC CONTINUE
      WRITE(NTSDUT, 5060) ICAPD
 5060 FORMATI///# - THE FOLLOWING INPUT DATA CAPD DDES NOT MATCH ANY DES
     ITGNATED KEYWORD -*//2X.20A4)
      STOP
   9C GOTO (100,110,120,130,140,150,160,170,180,190,195,200,210,220),IGD
                          PEADS ANGLE OF ATTACK IN DEGREES
  100 FEAD (MISIN. 5070)
                         ALPHAD
 5070 FORMAT(6E10.0)
      ALPHA = ALPHAD*DTR
      GO TC 60
                          READS ASPECT RATIO
  LIC PEAD(MTSIN, 5070)
                         ΔP
      GO TO 60
                          READS NO. AND X COMPD. OF TRANSVERSE CUTS
  12C PEAD (MTSIN, 5070)
                         TEAN
      NTR = TRAN
                         (XTR(I), I=1,NTR)
      PEAD (NTSIN, 5070)
      GO TO 60
                          PEADS NO. AND PERCENT VALUES OF SPANWISE CUTS
C
```

```
130 READ(NTSIN, 5070)
                          SPAN
      MSP = SPAN
      PEAD (NTSIN, 5070)
                          (YSP(I), I=1, MSP)
      GO TO 60
C
                           READS NO. OF TRANSVERSE CUTS ALONG CENTERLINE
  140 FEAD(NTSIN.5070)
                          CTFA
      NTC = CTRA
      GD TC 60
C
                           SETS CODE FOR DELTA WING PREPROCESSOR
  150 READ (NTSIN, 5070)
                          DUMMY
      KWPP = 1
      GO TO 60
                           SETS CODE FOR ARROW WING PREPROCESSOR
  160 PEAD (NTSIN, 5070)
                          DUMMY
      KWPR = 2
      GO TO 60
C
                           READS Y VALUES OF LEADING EDGE CORNER POINTS
C
                           AND SETS CODE FOR GOTHIC WING PREPROCESSOR
  170 PEAD(NTSIN, 5070)
                          (YLE(I), I=I,NTR)
      KWPR = 3
      GD TO 60
C
                           READS INPUT COPNER POINTS AND INDICES FOR
C
                           GENERAL TYPE OF WING NETWORK
  180 READ(NTSIN.5070)
                          FN7
      NZW = FNZ
      IF(NZW.EC.MSP*NTR) GO TO 182
      WRITE(NTSOUT, 5080)
 5080 FORMAT(//* NO. OF INPUT CORNER POINTS FOR WING NETWORK IS NOT EQUA
     IL TO*/* THE PRODUCT OF NO. OF TRANSVERSE CUTS AND NO. OF SPANWISE
     2CUTS*1
      STOP
  182 DO 184 J=1.NTR
      JN = (J-1)*MSP
      XJ = XTR(J)
      DO 183 T=1,MSP
  183 ZM(1,JN+I) = XJ
      READ(NTSIN, 5070)
                          \{ZM\{2,JN+I\},ZM\{3,JN+I\},I=I,MSP\}
  184 CONTINUE
      READ (NTSIN, 5070)
                          FNLE
      MLE = FNLE
                          (YLE(I). I=1.NLE)
      PEAD (NTSIN, 5070)
      DO 186 I=1, NLE
      ILF(I) = K = YLE(I)
      YLE(I) = ZM(2,K)
  186 CONTINUE
      FEAD (NTSIN, 5070)
                          FNTE
      NTE = FNTE
      PEAD(NTSIN.5070)
                          (YTE(I) \cdot I = 1 \cdot NTE)
      DO 188 I=1.NTE
  188 ITE(I) = YTE(I)
      KWPR = C
      GO TD 60
```

```
(
                          READS NO. OF SPANNISE CUTS FOR THE FREE SHEET
(
                          NETWORK
  190 READ(NTSIN, 5070)
                         SFS
      MES = SES
      OR TO 60
                              READS X VALUE OF PITCH AXIS
  195 READ(NTSIN, 5070)
                         XPITCH
      60 TO 60
                          PEADS MAX. NO. OF ITERATIONS ALLOWED FOR THE
ſ
                          NONLINEAR EQUATIONS SOLVER
C.
  200 READ(NTSIN, 5070)
                         TMX
      XMT = XMT
      GO TC 60
                          READS PRINTING OPTION
ζ
  210 FEAD(NTSIN, 5070)
                         PRINT
      ITPRIN = PRIMT
      IF(TTPRIN.FQ.O)
                       ITPPIN = 5
      00 TF 60
Ü
                          CALCULATES FREE STREAM VELOCITY AND FOOT CHORD
  220 CONTINUE
      FSV(1) = COS(ALPHA)
      ESV(2) = 0.
      FSV(3) = SIM(ALPHA)
      FSVM=SQFT(FSV(1) ##2+FSV(2) ##2+FSV(3) ##2)
      PCHOFD = XTR(NTC)
      IF(KWPR.EQ.O) GO TO 260
C
\mathbf{C}
                          USES PREPROCESSOR TO GENERATE CORNER POINTS FOR
C
                          WING NETWORK
      GO TO (230,240,250), KWPR
                              CALLS DELTA WING PREPROCESSOR
  230 CALL DWNET
      NLF = NTR & NTE = MSP
      NMZ = (NTR-1)*MSP
      DO 235 I=1.NTE
      TTE(I) = NMZ + I
  235 CONTINUE
      GO TO 260
                              CALLS ARROW WING PREPROCESSOR
C
  240 CALL AWNET
      MIF = MTF
                 5 NTE = NTP-NTC+1
      NMZ = (NTC-1) \pm MSP + 1
      00:245 I=1,NTE
      ITE(I) = MMZ + (I-1)*MSP
  245 CONTINUE
      GO TO 260
                              CALLS GOTHIC WING PREPROCESSOR
  250 CALL GWNET
      NLE = NTR 5 NTE = MTR-NTC+1
      NMZ = (NTC-1) * MSP + 1
      DO 255 I=1,NTE
```

```
ITF(I) = NMZ + (I-1)*MSP
  255 CONTINUE
C
Ç
                          SETS UP NETWORKS INDICES
  260 \text{ NM}(1) = \text{MSP}
                   $
                       NN(1) = MAXO(NTC.NLE)
      NM(S) = WES
                   $
                       NY(2) = NLE
      NM(3) = 2
                    $
                       'IN(3) = NLE
      NM(4) = NTE + NM(2) - 1  NN(4) = 2
      NM(5) = 2
                    $NN(5) = 2
C
C
                          DESIGNATES NETWORK TYPE
      NMETT = 5
                    NT(2) = 4 + NT(3) = 6
      VT(1) = 2
                  3
      NT(4) = 5
                 $ NY(5) = 7
C
C
                          CALCULATES OTHER NETWORK DATA
      NPA(1) = 0 $ MZA(1) = 0
      DO 270 K=1, NNETT
      NP(K) = (NM(K)-1) * (NN(K)-1)
      NZ(K) = NM(K) \neq NN(K)
      NPA(K+1) = NPA(K) + NP(K)
      NZA(K+1) = NZA(K) + NZ(K)
  270 CONTINUE
      NZ(NNETT+1) = 0
      NPANT = NPA(NNETT+1)
      NZMPT = NZA(NNETT+1)
      MZ1 = NZA(2) + NZ2 = MZA(3) + MZ3 = MZA(4)
      NZ4 = NZA(5) $ NZ5 = NZA(6)
      M1 = NM(1) $ M2 = NM(2) $ M3 = NM(3)
      M4 = NM(4)    M5 = NM(5)
(,
                          CALCULATES COPNER POINTS FOR FREE SHFFT, FED
C
0
                          SHEET AND THE ATTACHED FROZEN WAKE
      NNI = NN(1)
      XWAKE = 50. \pm XTR(NN1)
      IF(XWAKE.LE.100.0) XWAKE = 100.
                              FOR NETWORK NO. 2
C
      X1 = ZM(1,M1)
                         Y1 = ZM(2,M1) $ Z1 = ZM(3,M1)
      DO 280 T=1.M2
      ZM(1,NZ1+I) = XI
      ZM(2,NZ1+I) = Y1
      ZM(3*NZ1+I) = ZI
  280 CONTINUE
                              FOR NETWORK NO. 3
٢
                          $Y1 = ZM(2,N71+M2) $Z1 = ZM(3,NZ1+M2)
      XI = ZM(1,NZ1+M2)
      DO 290 I=1,M3
      ZM(1,NZ2+I) = XI
      ZM(2,NZ2+I) = YI
      ZM(3,NZ2+I) = ZI
  290 CONTINUE
                              FOR NETWORK NO. 2
C
      NMS = M2 - 1
```

```
00 310 K=2,NLE
      K1 = K-1
      NMK = NZ1 + K1*M2
      CALL SHEGEN (ALPHA, XTR (K), YLE(K), NMS, YE, ZE)
      XK = XTP(K)
      7LEK = ZM(3.K*M1)
      00 300 J=1,M2
      JM = NMK + J
      ZM(1,JM) = XK
      ZM(2*JM) = YF(J) + ZM(3*JM) = ZF(J) + ZLEK
  300 CONTINUE
1
                             FOR NETWORK NO. 3
      MMZ = MZZ + KI * M3
      ZM(1,NMZ+1) = ZM(1,NMZ+2) = XK
      7M(2,NMZ+1) = YF(MZ) $ 2M(3,NMZ+1) = ZF(MZ) + ZLEK
      Z^{M}(2,NMZ+2) = YF(M2+1) + ZM(3,NMZ+2) = ZF(M2+1) + ZUFK
  310 CONTINUE
                             FOR NETWORK NO. 4
      6200 = 072 - 02 + 0708 = 023 + 076 - 1
      DO 320 I = 2.M2
      IM = NZMA + I S IMN = NZMB + I
      7M(1,IMN) = 2M(1,IM) $ 2M(1,IMN+M4) = XWAKE
      ZM(2,IMN+M4) = ZM(2,IMN) = ZM(2,IM)
      ZM(3,IMN+M4) = ZM(3,IMN) = ZM(3,IM)
  320 CONTINUE
                             FOR NETWORK NO. 5
      NZMC = NZ3 - M3
      DO 330 [=1,M5
      IM = N7MC + I + I = N74 + I
      ZM(1,IMN) = ZM(1,IM) + ZM(1,IMN+2) = XWAKE
      7M(2,1MM+2) = 2M(2,1MM) = 2M(2,1M)
      ZM(3.IMN+2) = ZM(3.IMN) = ZM(3.IM)
  330 CONTINUE
C
                         MATCHES LEADING EDGE CORNER POINTS
      NMZ = N71 + 1
      DO 340 T=2.NLF
      TM = T*M1 $ TMM = NMZ + (T-1)*M2
      ZM(2,IM) = ZM(2,IMN)
      ZM(3,IM) = ZM(3,IMN)
  340 CONTINUE
C
                         SETS UP CORNER POINTS FOR THE PART OF
Ţ
                         THE WAKE NETWORK ATTACHED TO WING
      DO 350 T=1, MTE
      IM = ITE(I) $ IMN = NZ3 + I
      ZM(1,IMN) = ZM(1,IM) + ZM(1,IMN+M4) = XWAKE
      ZM(2,IMN+M4) = ZM(2,IMN) = ZM(2,IM)
      ZM(3.1MN+M4) = ZM(3.1MN) = 7M(3.1M)
  350 CONTINUE:
C
                         PRINTS OUT CORNER POINTS
5
```

```
IF(IPNPUT.EQ.O) GD TO 1040
      PPINT 1000
 1000 FORMAT (*1CHECK TEST PROBLEM DATA*)
      OB 1030 I=1, NMETT
      JI = NZA(I) + I + I + JZ = NZA(I+I)
      PPINT 1010. T
 1010 FORMAT(//# NETWORK NO. #. 13)
      PFINT 1020, (ZM(1,J),ZM(2,J),ZM(3,J),J=J1,J2)
 1020 FORMAT(12F10.5)
 1030 CONTINUE
 1040 CONTINUE
C
                           CALCULATES INITIAL LENGTH AND ANGLE OF SPAN-
Ç
                           WISE SECTION OF PANELS FOR FREE AND FED SHEETS
                           ASSUMING NM(3) = 2
      IF(IPNPUT.NE.C)
                        PRINT 1050
 1050 FOFMAT( #1 ANGLE AND LENGTH#/)
      NM2 = NM(2)    NN2 = NN(2)
      NZM = NZ(1) + NM(2)
      DC 360 J=2,NN2
      J2 = J-2
      JA = J2*(NM2 - 1)
      JM = NZM + J2 \neq NM2
      DO 360 1=2.NM2
      I1 = I-1
      IA = JA + II
      IM = JM + II
      Y! = ZM(2.IM)
                      5 Y2 = 7M(2, IM+1)
      71 = 7M(3.IM) $ 72 = 7M(3.IM+1)
      0Y = Y2 - Y1
                      5 DZ = Z2 - Z1
      ZLP = SQRT(DY**2 + DZ**2)
      ZAP = ATAN2(DZ,DY)
      ZL(I\Delta) = ZLP
      7A(IA) = 7AF
      IF(IPNPUT.NE.O) PRINT 1060, IA, IM, ZAP, ZLP, Y1, Z1, Y2, Z2, DY, PZ
 1060 FORMAT(215,2812.4,6F8.3)
  360 CONTINUE
      NP2 = NP(2) \qquad S \qquad NP3 = NP(3)
      DO 370 I=1,NP3
      IA = MP2 + I
      IM = NZZ + (2*I+1)
      Y1 = ZM(2,IM) $ Y2 = ZM(2,IM+1)
      Z1 = ZM(3,IM)
                      $ 22 = ZM(3.IM+1)
      0Y = Y2 - Y1   5   07 = 72 - 21
      ZLP = SQRT(DY**2 + D7**2)
      ZAP = ATAN2(DZ,DY)
      7L(IA) = 7LP
      Z\Delta(T\Delta) = Z\Delta P
      IF(IPNPUT.NE.D) PRINT 1060, IA,IM,ZAP,ZLP,Y1,Z1,Y2,Z2,PY,FZ
  370 CONTINUE
      FETUPN
      END
```

```
SUBRICUTINE AWNET
( * * * * * *
      SUBROUTINE AWNET
C
\mathbf{c}
                TO CALCULATE THE COORDINATES OF ALL PANEL CORMER FOINTS
C
      PUPPOSE
                IN AN ARROW WING PLANFORM CONFIGURATION
C
C
C
      INPUT
                COMMON BLOCK
                /DAT3/ - AR, NTR, XTR, MSP, YSP, NTC
(
C
      OUTPUT
                COMMON BLOCK
                /DAT3/ - YLE,NTE
C
                /MSPNTS/ - ZM
C
Ċ
      SUBFICUTINES
                SWEPTE
      CALLED
ŗ
C
      DISCUSSION. THE Y COOFDINATES OF THE PANEL CURNER POINTS AT THE
                INTERSECTION OF THE LEADING EDGE AND TRANSVERSE CUTS ARE
(
                COMPUTES BY MULTIPLYING THE X VALUE OF THE TRANSVERSE CUT
                BY ONE-FOURTH THE ASPECT RATIO.
                   THE Y COOPDINATES OF THE PANEL CORNER POINTS BETWEEN
C
C
                THE LEADING EDGE AND ROOT CHOPD ON THE TRANSVERSE CUTS
Ç
                APE COMPUTED BY MULTIPLYING THE Y COMPDINATE AT THE
C
                LEADING EDGE BY THE ARRAY OF PERCENT VALUES YSP.
ŗ
                   SUBFOUTINE SWEPTE IS CALLED TO CALCULATE THE Y
C
                COORDINATES OF ALL PANEL POINTS AFT OF THE POOT CHORD.
C
                   THE X COMPDINATES OF THE PANEL CORNER POINTS ARE THE
C
                X VALUES OF THE TRANSVERSE CUTS INPUT BY THE USER. ALL Z
                COOPDINATES ARE SET TO ZERO.
•
C ******
      COMMON/MSPNTS/ZM(3,175), ZL(75)
      COMMON /DAT3/AR, NTR, XTF(10), MSP, YSP(10), NTC, NLE, YLF(10),
                    NTE, YTE(10), MFS
      DIMENSION
                  YW(10), XY(10,10)
                           FINDS D (= S/X)
      D = \Delta R/4
                           OBTAINS CORNEN POINTS COORD. FOR THE UPPER PART
(
      X1 = XT^{c}(1)
      YLE(1) = 0*X1
      DO 10 1=1,MSP
      7M(1,1) = X1
      ZM(2.11 = ZM(3.11 = 0.
   10 CONTINUE
      DC 3C J=2.NTR
      J!! = (J-1) *MSP
      (L) \cap TX = LX
      SEMI = D*XJ
      YLF(J) = SEM[
      DO 20 I=1,MSP
      7M(1,JN+I) = XJ
      IM(2,JN+I) = SEMI*YSP(I)
```

```
20 \text{ ZM}(3*JN+1) = 0.
   30 CONTINUE
0
                           OBTAINS CORNER POINTS COORD. FOR THE LOWER PART
                           WITH SWEPT TRAILING EDGE
      KT1 = NTC-1
      NTF = NTR - KT1
      DO 40 T=1.NTE
      YLE(KTI+I) = D*XTE(KTI+I)
   40 CONTINUE
      NM7 = KT1 #MSP
      00 50 J=1,MSP
      YW(J) = ZM(2,NMZ+J)
   50 CONTINUE
      CALL SWEPTE (XTR(NTC), YLE(NTC), NTE, YW, MSP, XY)
      MITEL = MITE-1 .
      nn 60 J=1.NTE1
      JM = NMZ + J*MSP
      XJ = XTP(NTC+J)
      DO 60 I=1.MSP
      IM = JM + I
      ZM(1,IM) = XJ
      ZM(2,IM) = XY(I,J)
      ZM(3,IM) = 0.
   60 CONTINUE
      FETURN
       FND
```

```
SUBFOUTINE DWNFT
(****
ŗ
      SUPPOUTINE OWNER
C
ŗ
                TO CALCULATE THE COORDINATES OF ALL PANEL CORNER POINTS
      PUPPCSE
C
                IN A DELTA WING PLANFORM CONFIGURATION
C
C
      INPUT
                COMMON BLOCK
C
                /DATS/ - AF, NTF, XTP, MSP
C
C
      CUTPUT
                COMMON BLOCK
C
                /DAT3/ - YLE
C
                /MSPNTS/ - ZM
r
C
      SUBROUTINES
C
      CALLED
                NONE
C
C
      DISCUSSION. THE Y COORDINATES OF PANEL CORNER POINTS AT THE
C
                INTERSECTION OF THE LEADING EDGE AND THE TRANSVERSE CUTS
                ARE COMPUTED BY MULTIPLYING THE X VALUE OF THE TRANSVERSE
C
Ċ
                CUT BY ONE FOURTH THE ASPECT PATIO.
C
                   THE Y COORDINATES OF THE PANEL CORNER POINTS RETWEEN
Ċ
                THE LEADING FOGE AND ROOT CHOPD ON THE TRANSVERSE CUTS
                ARE COMPUTED BY MULTIPLYING THE Y COORDINATE AT THE
                LEADING EDGE BY THE ARRAY OF PEPCENT VALUES YSP.
                   THE X COORDINATES OF THE PANEL CORNER POINTS ARE THE
Ċ
                X VALUES OF THE TRANSVERSE CUTS INPUT BY THE USER. ALL
C
                Z COORDINATES ARE SET TO ZERO.
€.
C *****
      COMMON/MSPNTS/ZM(3,175),ZL(75)
      COMMON /DAT3/AP, NTP, XTR(10), MSP, YSP(10), MTC, NLF, YLE(10),
                   INTE, YTE(10), MES
C
                          FINDS D (= S/XI)
      D = \Delta R/4
C
                          OBTAINS CORNEN POINTS COORD.
      X1 = XTP(1)
      YLE(1) = D*X1
      DO 10 I=1,MSP
      ZM(1,I) = XI
      ZM(2,I) = ZM(3,I) = C.
   IO CONTINUE
      00 30 J=2.NTP
      92M*(1+L) = 11L
      XJ = XTF(J)
      SEMI = D*XJ
      YLE(J) = SEMI
      00 20 [=1,MSP
      ZM(1,JN+T) = XJ
      ZM(2,JM+I) = SEMI*YSP(I)
   20 \text{ ZM}(3.JN+I) = 0.
   30 CONTINUE
      RETUPN
      END
```

```
SUBROUTINE GWNET
( * * * * *
      SUBROUTINE GWNET
C
      PHERICSE
                TO CALCULATE THE COORDINATES OF ALL PANEL CORNER POINTS
\mathbf{C}
                IN A GOTHIC WING PLANFORM CONFIGURATION
      INPUT
                COMMON BLOCK
                /DAT3/ - NTR,XTR,MSP,YSP,NTC,YLE
      CUTPUT
                COMMON BLOCK
C
                /DAT3/ - NTE
                /MSPNTS/ - ZM
      SUBFCUTINES
                SWEPTE
      CALLED
      DISCUSSION THE Y COORDINATES OF PANEL COPNER POINTS AT THE
                INTERSECTION OF THE LEADING EDGE AND TRANSVERSE CUTS ARE:
                INPUT BY THE USER.
                   THE Y COOPDINATES OF PANEL COPNER POINTS BETWEEN THE
                LEADING EDGE AND FOOT CHOPD ON THE TRANSVERSE CUTS ARE
                COMPUTED BY MULTIPLYING THE Y COORDINATE AT THE LEADING
                EDGE BY THE APRAY OF PERCENT VALUES YSP.
                   SUBPOUTINE SWEPTE IS CALLED TO CALCULATE THE Y
                COORDINATES OF ALL PANEL POINTS AFT OF THE ROOT CHORD.
                   THE X COORDINATES OF THE PANEL CORNER POINTS ARE THE
C
                X VALUES OF THE TRANSVERSE CUTS INPUT BY THE USER. ALL
C
                Z COORDINATES ARE SET TO ZERO.
C*****
      COMMON/MSPNTS/ZM(3,175), ZL(75)
      COMMON /DAT3/AR.NTR.XTP(10), MSP.YSP(10), NTC.NLE, YLE(10).
     1
                    NTE, YTE (10), MFS
      DIMENSION
                  YW(10), XY(10,10)
                          DETAINS CORNEN POINTS COOPD. FOR THE UPPER PART
      X1 = XTF(1)
      DO 10 I=1.MSP
      ZM(1,I) = XI
      ZM(2,I) = ZM(3,I) = 0.
   10 CONTINUE
      DC 30 J=2,NTR
      JN = (J-1) \neq MSP
      XJ = XTR(J)
      SEMI = YLE(J)
      DO 20 I=1.MSP
      ZM(1,JN+I) = XJ
      ZM(2,JN+I) = SEMI*YSP(I)
   20 \text{ ZM}(3.JN+I) = 0.
   30 CONTINUE
                          OBTAINS CORNER POINTS COURD. FOR THE LOWER PART
C
                          WITH SWEPT TRAILING EDGE
C
      KT! = NTC-1
```

```
NTF = NTR - KT1
   MM7 = KT1 * MSP
   PO 50 J=1,MSP
   YW(J) = ZM(2,NMZ+J)
50 CONTINUE
   CALL SWEPTE (XTR (NTC), YEE (NTC), NTE, YW, MSP, XY)
   NTFI = NTE-I
   00 60 J=1,NTE1
   JM = NMZ + J#MSP
   (L+)TN)atx = LX
   DO 60 I=1,MSP
   IM = JM + I
   ZM(1,TM) = XJ
   ZM(2,IM) = XY(I,J)
   ZM(3.IM) = 0.
60 CONTINUE
   PETURN
   END
```

```
SUBROUTINE SHEGEN(ALPHA, X, S, N, Y, Z)
C****
      SUBFRUTINE SHEGEN (ALPHA, X, S, N, Y, Z)
C
C
      PURPOSE
                TO PROVIDE AN INITIAL GUESS OF THE FREE AND FED SHEET
C
                GEOMETRY AT A PARTICULAR TRANSVERSE OUT
C
C
      INPUT
                CALLING SEQUENCE
C
                ALPHA - ANGLE OF ATTACK OF THE WING (IN RADIANS)
C
                X - X COOPDINATE OF TRANSVERSE OUT (APEX IS X=0.6)
                S - Y COOPDINATE OF LEADING EDGE ON TRANSVERSE CUT
C
C
                N - DESIRED NUMBER OF FREE SHEET PANELS IN TRANSVERSE OUT
C
      DUTPUT
                CALLING SEQUENCE
                Y - Y COORDINATE OF CORNER POINTS DEFINING SHAPE OF
C
                    FREE AND FED SHEFTS ON GIVEN TRANSVERSE OUT
C
                Z - Z COORDINATES OF CORNER POINTS DEFINING SHAPE OF
C
                    FREE AND FED SHEETS ON GIVEN TRANSVERSE CUT
C
      SUBFCUTINES
C
      CALLED
               NONE
C
C
                   THE POUTINE COMPUTES AN INITIAL GUESS OF THE FREE AND
С
                FED SHEET GEOMETRY AT A PARTICULAR TRANSVERSE CUT. (SEE
                STAPTING SOLUTION SECTION OF ENGINEERING DOCUMENT FOR
C
                METHOD) POINTS DESCRIBING THE CURVES OF FIGURE 17 ARE
C
                STORED IN THE ARRAY YZVAL. EACH CURVE REPRESENTS THE
C
                FREE AND FED SHEET GEOMETRY FOR ONE DE EIGHT VALUES DE A.
C
                POINTS DESCRIBING THE FREE AND FED SHEET GEOMETRY FOR AN
                ARBITRARY VALUE OF A ARE OBTAINED BY LINEAR INTERPOLATION
C
                (OR EXTRAPOLATION). LINEAR INTERPOLATION IS THEN EMPLOYED
C
                ON THIS NEW SET OF POINTS TO CONSTRUCT A REPRESENTATION
C
                OF THE FREE SHEET BY THE NUMBER OF POINTS SPECIFIED IN
C
C
                THE INPUT DATA.
C *** **
      DIMENSION Y(N),Z(N)
      DIMENSION AVAL(8), YZVAL(2,9,8), YZ(2,9), D(8)
         SET NUMBER OF Y-Z CURVES AND NUMBER OF POINTS
C
С
         REPRESENTING EACH CURVE
      DATA NA. NP /8.9/
         VALUES OF A FOR EACH CURVE
C.
      DATA AVAL /.2,.6,1.,1.4,1.8,2.2,2.6,3.0/
         VALUES OF Y AND Z FOR POINTS ON CURVES
      DATA YZVAL /
     £1.,0.,.993,:02,.98,.C45,.963,.07,.94,.088,.92,.097,.897,.C97,
     C.878,.09,.892,.05,
     C1., O., 1.C12, .033, .998, .098, .973, .154, .92, .224, .853, .268, .79,
     C. 277, . 74, . 269, . 789, . 146,
     c1., 0., 1.03, .047, 1.028, .134, 1., .232, .958, .314, .87, .403, .764, .445,
     C.687,.44,.708,.246,
     01.0.1.046.046.06.1.06.1.06.1.039.29.99.408.89.53.785.58
     C.68, .587, .666, .33,
```

```
(1.,0.,1.,061,.07,1.087,.188,1.076,.339,1.019,.502,.924,.624,.812,
     C.689,.704,.703,.65,.398,
     (1.,0.,1.075,.08,1.112,.222,1.11,.392,1.055,.565,.96,.7,.844,.770,
     C. 735, . 8, . 644, . 454,
     C1., 0., 1.09, .09, 1.14, .252, 1.142, .435, 1.095, .617, 1.008, .756, .877,
     C.858,.77,.882,.645,.5,
     C1., C., 1.102, .099, 1.162, .277, 1.172, .468, 1.132, .647, 1.05, .8, .908,
     0.922,.805,.95,.648,.541
     (1
ſ
          CEMPUTE VALUE OF A FROM INPUT DATA
      A=ALPHA+X/S
C
          SELECT THE DATA CURVES FOR USE IN INTERPOLATING
C
          (OR EXTRAPOLATING) NEW CURVE FOR COMPUTED VALUE OF A
      DO 10 K=2.NA
      L=K-1
      TE(A.LT.AVAL(K)) GO TO 12
      CONTINUE
 19
 12
      DELTA=(A-AVAL(L))/(AVAL(L+1)-AVAL(L))
         CALCULATE POINTS DESCRIBING CURVE FOR COMPUTED
C
C
         VALUE OF A
      DO 20 T=1,2
      DO 20 J=1.NP
      YZ(I,J)=YZVAL(I,J,L)+DELTA*(YZVAL(I,J,L+1)-YZVAL(I,J,L))
 20
\mathbf{C}
         SET INITIAL POINT ON FREE SHEET
      Y(1) = YZ(1,1)
      Z(1) = YZ(2,1)
C
         GET LAST POINT ON FREE SHEET
         (AND INITIAL POINT ON FED SHEET)
      Y(N+1)=YZ(1,NP-1)
      Z(N+1)=YZ(2,NP-1)
C
         SET LAST POINT ON FED SHEET
      Y(N+2)=YZ(1,NP)
      Z(N+2)=YZ(2.NP)
      D(1) = 0.
      MPMI=NP-1
         CALCULATE DISTANCES BETWEEN POINTS ON MEW CURVE
(
      DO 30 I=2.NPMI
      D(I) = D(I-1) + SQRT((YZ(1,I)-YZ(1,I-1)) + 2 + (YZ(2,I)-YZ(2,I-1)) + 2)
 30
      CONTINUE
      DIST=D(NPM1)/FLOAT(N)
         LINEARLY INTERPOLATE DESIRED NUMBER OF POINTS
C
         FOR FREE SHEET REPRESENTATION
ŗ
      ₽0 40 I=2.N
      DIS=FLOAT(I-1)*DIST
      DO 35 J=2.NPM1
      K = J - 1
      IF(DIS.LT.D(J)) GO TD 38
      CONTINUE
 35
      DELTA=(DIS-D(K))/(D(K+1)-D(K))
 38
      Y(I)=YZ(I,K)+DELTA+(YZ(I,K+I)-YZ(I,K))
      7(1) = YZ(2,K) + DELTA*(YZ(2,K+1) - YZ(2,K))
 40
      CONTINUE
```

N2 = N + 2

SCALE POINTS TO ACCOUNT FOR MAGNITUDE OF LOCAL SEMI-SPAN

DO 50 I=1,N2

Y(I) = Y(I)*S

Z(I) = Z(I)*S

CONTINUE

FETUEN

END

```
SUBRICUTINE SWEPTE(X,S,N,Y,M,YP)
C ****
C
      SUBROUTINE SWEPTE
C
                TO CALCULATE THE Y COORDINATES OF THE PAMEL CORNER POINTS
C
      PURPOSE
C
                AFT OF THE ROOT CHORD FOR SWEPT TRAILING EDGE DESIGNS
C
C
      INPUT
                CALLING SEQUENCE
C
                X - APPAY OF TRANSVERSE OUT X VALUES STARTING WITH THE
                    LAST OUT THAT INTERSECTS THE POOT CHORD
C
C
                S - APRAY OF Y COOPDINATES OF THE LEADING EDGE ON THE
C
                    TRANSVERSE CUTS SPECIFIED BY X
C
                N - NUMBER OF TEANSVERSE CUTS AFT OF THE LAST TEANSVERSE
C
                    CUT TO INTERSECT THE POOT CHORD PLUS ONE
Ċ
                Y - ARRAY OF Y COGRDINATES OF PANEL CORNER POINTS LYING
C
                    ON THE LAST TRANSVERSE OUT THAT INTERSECTS THE ROOT
C
                    CHORD.
r
                M - NUMBER OF SPANWISE PERCENT VALUES INPUT BY THE USER
C
C
      OUTPUT
               CALLING SEQUENCE
                YP - ARRAY OF Y COORDINATES OF PANEL CORNER POINTS AFT OF
                     THE FOOT CHOED.
C
C
      SUBPCUTINES
      CALLED
               NONE
      DISCUSSION GIVEN THE COORDINATES OF TWO POINTS DEFINING 4 LINE
C
                AND ONE COORDINATE OF A THIRD POINT ON THE LINE. THE
C.
C
               UNKNOWN COORDINATE OF THE THIRD POINT CAN BE CALCULATED
C
                BY TOTANGULATION.
                   ONE OF THE POINTS DEFINING THE LINE IS LEADING FDGE-
Ç
               TRAILING EDGE INTERSECTION POINT. THE OTHER POINT IS THE
C
               PANEL CORNER POINTS LYING ON THE LAST TRANSVERSE OUT THAT
C
                INTERSECTS THE POOT CHOPD.
                   THE X VALUE OF THE THIRD POINT IS THE VALUE OF THE
\mathbf{C}
               TRANSVERSE CUT.
C *** ***
      DIMENSION X(1), S(1), Y(1), YP(10,1)
      DX = X(N) - X(1)
      N1 = N - 1
      IF(N.EQ.2) SO TO 15
      DO 10 J=2.N1
      XX = X(J) - X(I)
      J1 = J - 1
      PO 10 1=1.M
      YS = Y(1)
      TM = (S(N) - YS)/DX
      YP(I,JI) = TM \times XX + YS
 10 CONTINUE
   15 CONTINUE
      DO 20 I=1.M
      YP(I,NI) = S(N)
  20
      FETUEN
      FND
```

```
PROGRAM ALCGEN.
C *****
C
      PROGRAM
                AICGEN
Ç
C
      PURPOSE
                TO CALCULATE ESSENTIAL GEOMETRY INFORMATION FOR FACH
C
                PAMEL AND THE LOCATIONS OF DOUBLETS AND CONTROL POINTS
C
                FOR EACH NETWORK AND TO GENERATE THE AFRODYNAMICS INFLUEN
                -CE COEFFICIENTS USING AN ADVANCED PANEL-TYPE METHOD
C
C
      IMPUT
                COMMON BLOCK
C
                /INDEX/ - NT.NM.NN.NP.NZ.NPA.NZA.NNETT.NPANT.NZMPT
C
                /NITE/ - NEUN
Ċ
                /IPRINT/ - IPGEOM, IPSING, IPCNTR, IPEIVC
C
C
      DUTPUT
                COMMON BLOCK
\boldsymbol{c}
                /CMO3/ - NPIF.NAIC3.NAIC
C
                /BDYCS/ - ZC.ZCC.ZCP.ZDC.IPC.ITC
C
                /INDEX/ - NS.NC.NSA.NCA.NSNGT.NCTRT
                /NINDX/ - NEO, NJC, IJC
C
C
                /ICONST/ - PI,PI2,PI4I
C
      SUBROUTINES
      CALL FD
                TG =OMC. TSING. TCNTFL, EDGEIN, KSOFT, PTRNS, IPTRNS, VINECC, VIP
C
      DISCUSSION SEE PROGRAM DUCUMENT 1.3 DESCRIPTION AND FLOW CHAPT OF
C
                OVERLAY PROGRAMS
C
CCMMCN /CMO3/NTSIN,NTSQUT,NTGD,NPIF,N4IC3,N4IC,NJ4C,NSCF
      COMMON/BOYCS/ZC(3,125),ZCC(3,125),ZCR(125),ZDC(125),IPC(125),
                    [TC(125)
     1
      COMMCN/INDEX/NT(9),NM(9),NN(9),NP(9),NS(9),NC(9),NZ(9),
    CMPA(10),NSA(10),NCA(10),NZA(10),NNETT,NPANT,NSNGT,NCTRT,NZMPT
      COMMON/PANDQ/CP(3,4),PC(3),FC(3),AP(3,3),ART(3,3),P(2,4),A,8,DIAM,
     CC(6,6),AST(5,16),IIS(16),INS,ITS,NPDO
      COMMON /NINDX/NFP.NJC(125).IJC(125)
      COMMON /PINC/DVDFS(3,125)
      COMMON /PINDX/KP.KQ.NPWP.NPPD
      COMMON /NEAJ/NEQ.NE.NG
      COMMON /NITE/NEUN.JT.ITMX.KIT.ITPPIN
      COMMON /ZIP/IPZ, IP, ITZ, JCZ
      COMMCN/ICONST/PI,PI2,PI4I
      COMMON /IPPINT/IPNPUT, IPGEOM, IPSING, IPCNTP, IPEIVG, IPOUTP
      DIMENSION ATC(125)
                              SETS CONSTANTS PI. ETC.
C
      PI = 3.1415926535897931
      DI2 = 2.*PI
      PI4I = 0.25/PI
C
                              CALLS POUTINE TO GENERATE ESSENTAIL GEOME-
                              TRY INFORMATION FOR EACH PANEL OF ALL
C
                              THE NETWORKS
C
      KP = 0
```

OVERLAY(VORTEX.2.0)

```
REWIND NPIF
                    5 MPW? = NPIF
      CALL TGERMO
                              CALLS ROUTINE TO DESIGNATE THE LOCATION OF
Ĉ
                              DOUBLETS ON ALL NETHORKS PANELS AND TO
                              COMPUTE THE MATRIX FOR COSPETCIENTS OF
(
                              DOUBLET DISTRIBUTION FOR EACH PANEL
      KQ = 0
      PEWIND MPIF
                       NPPD = NPIF
      KD = 0
      FEWIND NTGD
                    5
                       NPWR = NTGD
      CALL TSING
                              CALLS ROUTING TO DESIGNATE THE LOCATION OF
C
                              CONTROL POINTS FOR ALL NETWORK PANELS AND
r
                              TO COMPUTE THE UNIT NORMAL VECTOR AND THE
                              MORMAL COMPONENT OF FREE STREAM VELOCITY
C
                              VECTOR AT EVERY CONTROL POINT
C
      KC = 0
     PEWIND NTGD & NPPD = NTGD
      CALL TONTPL
                              TO PEARRANGE INDICES SO THAT THOSE CON-
C
                              TROL POINTS AND DOUBLETS AT EDGES OF NET-
C
                              WORKS PRECEDE ALL THE OTHERS
C
      CALL EDGEIN
      CALL KSCRT(ZC.3.NCTRT.NJC.DVDES)
      CALL KSORT (ZCC, 3, NCTRT, NJC, DVDFS)
      CALL KSCRT(ZCR, L, NCTRT, NJC, AIC)
      CALL KSCRT(7DC.1.NCTRT.MJC.AIC)
      CALL KSORT(IPC. I, NOTRIT, NUC. AIC)
      CALL KSCRT(ITC.1.NCTRT, MUC.AIC)
      KO = 0
      PEWIND NTGD & NPRD = NTGD
      KP = 0
      FEWIND NPIF $ NPWP = NPIF
      DO 100 IP=1.NPANT
      CALL PTENS(IP)
      00 50 I=1, INS
      IS = IIS(I)
  50
      IIS(II) = NJC(IS)
      CALL IPTRNS(IP)
  100 CONTINUE
      IE(NEUN.EQ.O) GO TO 500
                              TO SKIP AIC CALCULATION IF NEUN. ME.O.
C
      On 300 JC=I',NCTRT
      IF(ITC(JC).EO.1)
                       ZCP(JC) = C.
  300 CONTINUE
      GO TE 900
                          GENERATES AIC MATRIX
C
  500 CONTINUE
      PRINT 3001, JT
C3001 FOFMAT(//* ITERATION NO.*, 14,5X, *NEW AIC MATRIX GENERATED*)
      FEWIND NATCS
      REWIND NAIC
```

```
IF(IPEIVC.NE.O) PRINT 1003
 1003 FORMAT(#1FROM EIVC#/)
      JPC=C
      DO 700 JC=1.NCTRT
      IPZ = IPC(JC)
      ITZ = ITC(JC)
      JC7 = JC
      IF(ITZ.FQ.1) ZCR(JC) = 0.
      CALL VINECCIZC(1,JC),ZCC(1,JC),ZDC(JC),JPC)
      WRITE(NAIC3) DVDFS
      DO 650 TS=1, NSMGT
      CALL VIP(ZCC(1,JC),1,DVDFS(1,IS),1,3,AIC(IS))
  650 CONTINUE
      WRITE(NAIC)
                   AIC
  700 CONTINUE
                         CALCULATES NUMBER OF EQUATIONS FOR E, F AND G
C
      NEQ = NEP
      NF = NSNGT - NEQ
      NC = NP(2)
  900 RETURN
      END
```

```
SUBROUTINE CCAL(P.C)
( *****
C
      SURROUTINE CCAL (P.C.)
Ç
                TO CALCULATE FOR EACH PANEL THE QUADRILATERAL MOMENT
C
      PUPPCSE
                INTEGRALS USED IN THE COMPUTATION OF THE SOURCE AND
                DOUBLET FAR FIELD VELOCITY INFLUENCE COEFFICIENTS. (SEE
                SECTION B.4 . APPENDIX B OF THE ENNGINEERING DOCUMENT.)
C
C
      TUSNI
                CALLING SEQUENCE
                P - COORDINATES OF FOUR CORNER POINTS OF QUADRILATERAL
C
C
                CALLING SEQUENCE
      OUTPUT
C
                C - ARRAY OF MOMENT INTEGRALS
      SUBPCUTINES
C
      CALLED
                ECAL, ZERG
C
      DISCUSSION THE ROUTINE COMPUTES THE QUADFILATERAL MOMENT
C
                INTEGRALS C(M,N)=I(STGMA,KSE**(M-1)*ETA**(N-1),DKSE*DETA)
                FOR M=1,MXQ AND N=1,MXQ-M+1. A DESCRIPTION OF THE
C
                CALCULATIONS PERFORMED IS CONTAINED IN SECTION 8.4 OF
C
                APPENDIX B OF THE ENGINEERING DOCUMENT. THE RELEVANT
                EQUATIONS ARE (B.93) THROUGH (B.102). THE RELEVANT
                PROCEDURE IS PROCEDURE 6. THE CODE CLOSELY FOLLOWS THE
C
                DEVELOPMENT AND NOTATION OF THIS PORTION OF APPENDIX P.
( *** ***
      DIMENSION P(2,4),C(6,6)
      CCMMCN/SK4IC2/R1(2),F2(2),DP(2),E(7),GA(6,6),DUMS(241)
         EQUATIONS AND PROCEDURES REFERENCED IN THIS POUTINE
C
          ARE CONTAINED IN APPENDIX B OF ENGINEERING DOCUMENT
C
C
         SET ORDER OF MOMENTS DESIRED
      MXQ=6
      MYOP I=MXO+1
      CALL ZEFC(C, MXQ*MXQ)
Ç.
         CYCLE THEOUGH SIDES OF QUADRILATERAL
      DC 500 IS=1.4
         EXECUTE PROCEDURE 6
€.
      ISP1=MOD(IS.4)+1
         CALCULATE GEOMETRIC QUANTITIES ASSOCIATED WITH
C
C
         SIDE OF QUADFILATERAL
      DO 50 1=1.2
      P1(1)=P(1.15)
      P2([)=P([, [SP1)
 50
      DF(I) = F2(I) - P1(I)
      D^{c}MS = DR(1) * DR(1) + DR(2) * DR(2)
      IF(DRMS.EQ.O.) GO TO 500
      \Delta = P1(1) * P2(2) - R1(2) * P2(1)
         BEANCH TO PROCEDURE (6.4) OF (6.8)
(
      IF(ABS(DR(1))-ABS(DP(2))) 100,100,200
 100
      \Lambda 1 = DP(1)/DP(2)
```

```
\Delta 2 = \Delta / DP(2)
           PPOCEDUPE (6.4.1)
(
       CALL ECAL(P1(2), R2(2), 1., 1., E, MXCP1)
       DO 130 N=1.4XQ
       G\Delta(1,N) = \Delta2 \pm E(N+1)/FLOAT(N)
 130
       IF(MXQ.LT.2) GO TO 300
C
           PERCEDURE (6.A.TI)
       DC 170 M=2, MXQ
       MYN=MXC-M+1
       DO 170 N=1.MXN
       SA(M,N) = A1 + GA(M-1,N+1) + A2 + GA(M-1,N)
       GO TO 300
       \Delta 1 = DP(2)/DP(1)
 200
       \Delta 2 = \Delta / OP(1)
           PROCEDUFE (6.8.1)
Ç
       CALL ECAL(R1(1), R2(1), 1., 1., E, MXOP1)
       DO 230 M=1, MXO
       G\Delta(M+1)=A2*E(M+1)/FLOAT(M)
 230
       IF(MYQ.LT.2) GD TD 300
           PROCEDURE (6.8.II)
C
       DO 270 N=2, MXQ
       MYM=NXQ-N+1
       DO 270 M=1, MXM
       GA(M,N) = A1 + GA(M+1,N-1) - A2 + GA(M,N-1)
 270
       CONTINUE
 300
           PERFORM ACCUMULATION OF EQUATION (8.94)
       DO 400 M=1, MXQ
       M \times N = M \times Q - M + I
       DO 400 N=1. MXN
       C(M,N)=C(M,N)+GA(M,N)/FLDAT(M+N)
 400
       CONTINUE
 500
 900
       FETURN
       END
```

SUPPCUTINE CONTRL(NT, NM, NN, NC, NPA, ZM, ZC, ZCC, ZCR, ZDC, IPC, ITC) C***** C SUBFICUTINE CONTRE(NT.NM.NN.NC.NPA.ZM.ZC.ZCC.ZCR.ZDC.IPC.ITC) C PUPPCSE TO COMPUTE CONTROL POINT DEFINING QUANTITIES FOR EACH NETWORK C C INPUT CALLING SEQUENCE NY - NETWORK TYPE MM - NUMBER OF SPANWISE CUTS IN THE NETWORK NN - NUMBER OF TRANSVERSE CUTS IN THE NETWORK r, C NPA - TOTAL NUMBER OF PANELS IN ALL PREVIOUS NETWORKS C ZM - COORDINATES OF CORNER POINTS OF THE METWORK C. COMMON BLOCK C /IPRINT/ - IPCMTR /FSVEL/ - FSV C /PANDO/ - PC Ç CUTPUT CALLING SEQUENCE NC - NUMBER OF CONTROL POINTS ON THE NETWORK C C 7C - COORDINATES OF CONTROL POINTS ON NETWORK C ZCC - SURFACE NORMAL VECTOR AT CONTROL POINTS C ZCR - NORMAL COMPONENTS OF FREESTREAM VELOCITY C ZDC - RELOCATION DISTANCE OF CENTROL POINT C IPC - SEQUENCE NUMBER OF PANEL TO WHICH CONTROL POINT BELONGS C ITC - NETWORK EDGE CONTROL POINT INDICATOR C SUBREUTINES Ĺ CALLED GCPCAL, GRDIND, PTPNS, SUPPRO, MMULT (C DISCUSSION. THE POUTINE CALCULATES QUANTITIES ASSOCIATED WITH THE CONTROL POINTS AND BOUNDARY CONDITIONS OF THE PROBLEM. Ċ SEPARATE COMPUTATIONS ARE PERFORMED FOR EACH NETWORK C C TYPE. FIRST THE CONTROL POINTS (POINTS AT WHICH THE C BOUNDARY CONDITIONS ARE APPLIED) ARE LOCATED. THIS IS DONE BY AVERAGING CERTAIN COMBINATIONS OF CORNER POINTS AND THEN PROJECTING THE RESULTANT POINTS ONTO THE PANEL . C SUPFACES. THOSE CONTROL POINTS LOCATED ON A NETWORK FDG C ARE WITHDRAWN SLIGHTLY FROM THE EDGE AND NOT PROJECTED C ONTO THEIR PANEL SURFACES TO AVOID NUMERICAL DIFFICULTY C LATER. THE CONTROL POINTS ARE ORDERED AND INDEXED ALONG C WITH AUXILIARY QUANTITIES WHICH ARE COMPUTED AS WELL. C SUCH QUANTITIES INCLUDE THE PANEL NORMAL AT THE CONT. C POINT, THE COMPONENT OF FREESTREAM VELOCITY IN THIS C DIRECTION (FOR USE IN APPLYING THE BOUNDARY CONDITIONS) C AND THE DISTANCE THE EDGE CONTROL POINTS ARE WITHDRAWN. C * * * * * *

COMMCN/FSVEL/ESV(3),FSVM .COMMCN/PANDO/CP(3,4),PC(3),FO(3),AF(3,3),AFT(3,3),P(2,4),A,B,DTAM,

```
CC(6,6), AST(6,16), IIS(16), INS, ITS, NPDQ
      COMMON /SKFCH1/74(3,175), IA(175)
      COMMON /IPFINT/IPNPUT, IPGEOM, IPSING, IPCNTR, IPEIVC, IPOUTP
      DIMENSION ZC(3,100),ZCC(3,100),ZCR(100),ZCC(100),IPC(100),ITC(100)
      DIMENSION ZM(3,NM,NN)
      DATA DELTA /1.0E-5/
      IF(NT.EQ.5.0R.NT.EQ.7) DELTA = 1.0E-7
      IF(IPCNTR.NE.O) PRINT 1001
 1001 FORMAT(IHI)
      NNI=NN+1
      NM1=NM+1
         CALCULATE LOCATION OF CONTROL POINTS FROM CORNER POINT DATA
C
      CALL SCPCAL(NM, NN, NM1, NN1, ZM, ZA)
         OFDER NON-IDENTICAL CONTROL POINTS
C
      CALL GEDIND (NML.NNL.ZA.IA.NIA)
          TRANSFER TO CODE FOR APPROPRIATE NETWORK TYPE
€.
      GO TO(100,200,300,400,500,600,600)
 100
      CONTINUE
Ç
          SCURCE/ANALYSIS NETWORK CALCULATIONS
         (NOT AN OPTION IN PRESENT PROGRAM)
C
      JC =0
      DO 199 N=2.NN
      DO 198 M=2.NM
      JC = JC + I
      IP=M-1+(NM-1)*(N-2)+NPA
      IPC(JC)=IP
      CALL PTRNS(IP)
      CALL SUPPRO(PC, ZC(1, JC), ZCC(1, JC))
      CALL MMULT(ZCC(1,JC),FSV,ZCP(JC),1,3,1)
      ZCP(JC) = -ZCP(JC)
 193
      CONTINUE
      CONTINUE
 199
      NC = JC
      60 TC 800
 200
      CONTINUE
         DOUBLET/ANALYSIS (WING) NETWORK CALCULATIONS
C
      JC=0
         CYCLE THROUGH ALL CONTROL POINTS ON THE NETWORK
C
      00 299 N=1.NN1
      DC 298 M=1,NM1
      LMN = M + NM1 + (N-1)
         COMPUTE INDICES ASSOCIATED WITH CONTROL POINT
C
      TE(TA(LMN).LE.JC) GO TO 298
      JC = JC + 1
      IP=MINO(M4XO(M,2),NM)-1+(NM-1)*(MINO(MAXO(N,2),NN)-2)+NPA
      IPC(JC) = IP
      fTC(JC) = 0
      IF(M.EQ.1.OR.M.EQ.NM1.OR.N.EQ.1.OR.N.EQ.NM1)
                                                      ITC(JC) = 1
         RETRIEVE PANEL INFORMATION
C
      CALL PTENS(IP)
      SDC = 0.
         CALCULATE CONTPOL POINT COORDINATES
C
```

```
DO 220 L=1,3
      DPZ = DELTA*(PC(L)-ZA(L,LMN))
      ZC(L,JC) = ZA(L,LMN) + DPZ
      SDC = SDC + DPZ \pm 2
      CONTINUE
 220
      ZDC(JC) = SQRT(SDC)
      IF(ITC(JC).NE.1) ZDC(JC) = C.
\boldsymbol{\Gamma}
          PROJECT CONTROL POINT ONTO PANEL SUPFACE UNLESS
\epsilon
          CENTROL POINT IS ON NETWORK EDGE
          COMPUTE SURFACE NORMAL AT CONTROL POINT
      [F(ZDC(JC).EQ.O.)
                          CALL SUFPRO(ZC(1,JC),ZC(1,JC),ZCC(1,JC))
      IF(ZBC(JC).NE.D.) CALL SUPPRO(ZC(1,JC),ZCC(1,JC),ZCC(1,JC))
C
         COMPUTE MORMAL COMPONENT OF FREESTREAM
C
          VELUCITY AT CONTROL POINT
      CALL MMULT(ZCC(1, JC), FSV, ZCR(JC), 1, 3, 1)
      ZCP(JC) = -ZCP(JC)
      IF (IPCNTR.NE.O)
     $wF{TF(6,1000) JC,{P,ZC(1,JC),ZC(2,JC),ZC(3,JC),ZCF(JC),ZDC(JC)
 298
      CONTINUE
 299
      CONTINUE
      MC=JC
      GD TE 800
 300
      CONTINUE
          SCURCE/DESIGN NETWORK CALCULATIONS
C
ŗ
          (NOT AN OPTION IN PRESENT PROGRAM)
      GO TO 800
 400
      CONTINUE
          DOUBLET/DESIGN (FREE SHEET) NETWORK CALCULATIONS
C
      JC=0
      DO 429 N=1,NN
      DO 428 M=1.NM
C
         RE-OPDER CONTROL POINTS ELIMINATING CONTROL POINTS
\mathbf{C}
         ON TWO OF THE NETWORK FDGES
      LMN = M + NM*(N-1)
      LMNP=M+NP1*(N-1)
      DO 420 L=1,3
      7\Lambda(L,LMN)=Z\Lambda(L,LMNP)
 420
      CONTINUE
 428
      CONTINUE
 429
      CONTINUE
0
         OFDER MON-IDENTICAL CONTROL POINTS
      CALL GROIND (NM, NN, ZA, IA, NTA)
C
         CYCLE THROUGH ALL CONTPOL POINTS ON THE NETWORK
      DD 499 N=1.NN
      DC 498 M=1,NM
         COMPUTE INDICES ASSOCIATED WITH CONTROL POINTS
C
      LMN=M+NM*(N-1)
      IF(IA(LMN).LE.JC) GD TO 498
      JC = JC + 1
      IP=MING(MAXO(M,2),NM)-1+(NM-1)\neq(MING(MAXO(N,2),NN)-2)+NPA
      IPC(JC)=IP
      ITC(JC) = C
```

```
IF(M \cdot EQ \cdot 1 \cdot OP \cdot N \cdot EQ \cdot 1) ITC(JC) = 1
          RETRIEVE PANEL INFORMATION
C
      CALL PTFNS(IP)
      SDC = C.
          CALCULATE CONTROL POINT COOPDINATES
      DO 450 L=1.3
      DPZ = DELTA*(PC(L)-ZA(L.LMN))
      ZC(L,JC) = ZA(L,LMN) + DPZ
      SDC = SDC + DPZ **2
 450
      CONTINUE
      ZDC(JC) = SQRT(SDC).
      IF(ITC(JC).NE.1) ZDC(JC) = C.
          PROJECT CONTROL POINT ONTO PANEL SURFACE
C
          UNLESS CONTROL POINT IS ON NETWORK EDGE
          COMPUTE SURFACE NORMAL AT CONTROL POINT
C
      IF(7DC(JC).EQ.O.)
                           CALL SUPPRO(ZC(1,JC),ZC(1,JC),ZCC(1,JC))
                           CALL SURPRO(ZC(1,JC),ZCC(1,JC),ZCC(1,JC))
      TF(ZDC(JC).NE.D.)
          COMPUTE NORMAL COMPONENT OF FREESTREAM
C.
          VELOCITY AT CONTROL POINT
C
      CALL MMULT(ZCC(1,JC),FSV,ZCR(JC),1,3,1)
      7CR(JC) = -ZCR(JC)
      IF (IPCNTR.NE.O)
     $WPITF(6,1000) JC, TP, ZC(1, JC), ZC(2, JC), ZC(3, JC), ZCR(JC), ZDC(JC)
 498
      CONTINUE
 490
      CONTINUE
      NC = JC
      SD TC 800
 500
      CONTINUE
         DOUBLET/DESIGN (WAKE) NETWORK CALCULATIONS
ŗ
      JC=0
         CYCLE THROUGH ALL CONTROL POINTS ON THE NETWORK
C
      DO 599 N=1.1
      DO 598 M=1,NM1
         COMPUTE INDICES ASSOCIATED WITH NETWORK
C
      LMN=N+NM1*(N-1)
      IF(TA(LMN).LF.JC) GO TO 598
      JC=JC+1
      IP=MINO(MAXO(M,2),NM)-1+(NM-1)*(MINO(MAXO(N,2),NN)-2)+NPA
      IPC(JC)=IP
      ITC(JC) = 1
          RETRIEVE PANEL INFORMATION
C
      CALL PTRNS([P)
      SDC = 0.
         CALCULATE CONTROL POINT COORDINATES
C
      DO 520 L=1.3
      DPZ = DELTA + (PC(L) - 2A(L, LMN))
      ZC(L,JC) = ZA(L,LMN) + DPZ
      SDC = SDC + DPZ**2
 520
      CONTINUE
      ZDC(JC) = SQRT(SDC)
          PROJECT CONTROL POINT ONTO PANEL SUFFACE
C
         COMPUTE SURFACE NORMAL AT CONTROL POINT
C
```

```
IF(7DC(JC).EQ.O.) CALL SUPPRO(ZC(1,JC),ZC(1,JC),ZCC(1,JC))
      IF(ZDC(JC).NE.O.)
                        CALL SUPPRO(ZC(1,JC),ZCC(1,JC),ZCC(1,JC))
C
         COMPUTE NORMAL COMPONENT OF FREESTREAM
C.
         VELOCITY AT CONTROL POINT
      CALL MMULT(ZCC(1, JC), FSV, ZCR(JC), 1, 3, 1)
      ZCP(JC) = -ZCP(JC)
      IF (IPCNTR NE . 0)
     598
     CONTINUE
 599
      CONTINUE
      NC=JC
      GO TO 800
 600
      CONT INUE
         DOUBLET/DESIGN (FED SHEFT) CALCULATIONS
C
      ND = NNI
      IC(NT.EQ.7) ND = 1
         CYCLE THROUGH ALL CONTROL POINTS ON THE NETWORK
C
      DO 699 N=1.ND
      DD 698 M=1.1
         COMPUTE INDICES ASSOCIATED WITH THE NETWORK
C
      LMN=M+NM1*(N-1)
      JC = JC + 1
      IP=MINO(MAXO(M, 2), NM)-1+(NM-1)*(MINO(MAXO(N, 2), NN)-21+NPA
      100(JC)=10
      ITC(JC) = 1
Ç,
         RETRIEVE PANEL INFORMATION
      CALL PTRNS(IP)
      SDC = 0.
         CALCULATE CONTROL POINT COORDINATES
C
      PO 620 L=1.3
      DPZ = DELTA*(PC(L)-ZA(L,LMN))
      IC(L,JC) = 7A(L,LMN) + OPZ
      SDC = SDC + DPZ**2
      CONTINUE
 620
      ZDC(JC) = SQRT(SDC)
         PROJECT CONTROL POINT ONTO PANEL SURFACE
C
         COMPUTE SURFACE NORMAL AT CONTROL POINT
                         CALL SUPPROIZE(1, JC), ZC(1, JC), ZCC(1, JC))
      IF(ZDC(JC).EQ.Q.)
      TF(ZDC(JC).NE.J.) CALL SUPPRO(ZC(1,JC).ZCC(1,JC).ZCC(1,JC))
         COMPUTE NORMAL COMPONENT OF FREESTREAM
C
         VELOCITY AT CONTROL POINT
      CALL MMULT (7CC(1, JC), FSV, ZCR(JC), 1, 3, 1)
      7CP(JC) = -ZCP(JC)
      IF(IPCNTF.NF.O)
     *WRITE(6,1000) UC, IP, ZC(1, JC), ZC(2, JC), ZC(3, JC), ZCR(JC), ZDC(JC)
1000 FORMAT(215,5E15.6)
698
      CONTINUE
699
      CONTINUE
      MC = JC
800
      CONTINUE
      FETURN
      END
```

SUBRCUTINE OPIV

しゃななななな

Ç

SUBPOUTINE DPIV

C C

PURPLSE TO CALCULATE THE VELOCITY INFLUENCE COEFFICIENTS INDUCED AT A FIELD POINT BY A DOUBLET PANEL

INPUT

COMMON BLOCK

/ICONST/ - PI2.PI4I C.

/PIVINT/ - X,P,A,B,DIAM,C,NTST

Ç

COMMON BLOCK OUTPUT /PIVINT/ - DV

Ç

Ç

SUBPCUTINES

CALLED

INTCAL, ZERO

C

INFLUENCE COEFFICIENTS AT A SPECIFIED FIELD POINT. A DESCRIPTION OF THE METHOD AND CALCULATIONS PERFORMED IS CONTAINNED IN APPENDIX B OF THE ENGINEERING DOCUMENT. IF THE FIELD POINT IS SUFFICIENTLY DISTANT FROM THE PANEL A FAR FIELD APPROXIMATION IS EMPLOYED. THE APPROXIMATION AND COMPUTATIONAL METHOD IS PRESENTED IN SECTION 8.4 OF APPENDIX 8 AND THE RELATED CODE COMPRISES THE PART OF DRIV BETWEEN STATEMENT 120 AND STATEMENT 500. THE LOOP 450 CONTAINS THE BULK OF THE CALCULATIONS AND ITS PURPOSE IS TO COMPUTE THE J VECTORS OF EQUATION (8.91). FOR THIS CALCULATION THE TERMS ON THE RIGHT SIDE OF EQUATION (B.91) HAVE BEEN EXPANDED, HENCE THE CODE DOES NOT DIRECTLY CORRELATE WITH THIS FORMULA. ANDTHER EVALUATION PROCEDURE IS EMPLOYED WHEN THE FIELD POINT IS NEAR THE PANEL. A DESCRIPTION OF THIS PROCEDURE IS PRESENTED IN SECTIONS 8.2 AND 8.3 OF APPENDIX 8. THE RELATED CODE COMPRISES THE PART OF DRIV BETWEEN STATEMENTS 500 AND 900. THE LOOP 750 CALCULATES THE VECTOR J DEFINED BY EQUATION (B.34) WITH THE H INTEGRALS COMPUTED BY THE POUTINE INTCAL. THE LOOP 800 TRANSFORMS

THE INFLUENCE COFFFICIENTS PELATIVE TO THE EXPANSION OF

DOUBLET STRENGTH ABOUT THE PROJECTION OF THE FIELD

POINT TO COEFFICIENTS RELATIVE TO THE EXPANSION OF

DISCUSSION THE ROUTINE COMPUTES THE DOUBLET PANEL VELOCITY

C C

(*****

1

C

C

LOGICAL LOGAB COMMON/ICONST/PI,PI2,PI4I COMMON/INTG/H(6,6,7), HZ, IH, MXQ, MXK

COMMON/PIVINT/X(3),P(2,4),A,B,D[AM,C(6,6),DV(3,6),NTST,NCF DIMERSION Q(3), QEX(3,6), MJ(6), NJ(6)

DOUBLET STRENGTH ABOUT THE ORIGIN.

DATA MJ. NJ /1, 2, 1, 3, 2, 1, 1, 1, 2, 1, 2, 3/

DATA DELMO.DELMO /4.,2.45/

FQUATIONS AND QUANTITIES REFFRENCED IN THIS ROUTINE ARE CONTAINED IN APPENDIX B OF THE ENGINEERING DOCUMENT

```
42=2.*A
       B2=2.*B
C.
          TEST FOR POSSIBILITY OF EMPLOYING FAR FIELD APPROXIMATION
       XM = SCRT(X(1) + X(1) + X(2) + X(2) + X(3) + X(3))
       RATIC=XM/DIAM
٢
          BASIC TEST
       IF(RATIO.GT.DELMD) GO TO 120
          AUXILIARY TEST BASED ON MORE REFINED ESTIMATE
(
       PATTC=0.
       DO 100 IC=1,4
       OTP = ARS(P(1, IC) + (P(1, IC) - 2. *X(1)) + P(2, IC) + (P(2, IC) - 2. *X(2)))
       PATIC=AMAX1(RATIO,QIP)
       CITAP\MX + MY = OITAP
          BRANCH TO NEAR FIELD CALCULATION IF FIELD POINT TOO
C
          CLOSE TO PANEL
       IF(PATICALT DELMO) GO TO 500
       CONT INUE
 120
          FAR FIELD CALCULATIONS
C
       U=1./XM
       U2=U*U
       U3=U*U2
       X(1)=U*X(1)
       X(2)=U \pm X(2)
       X(3) = U * X(3)
       \Delta 2X = \Delta 2 \times X(1)
       B2Y=02*X(2)
       UD4PI=U3*PI4I
       UD8PI=.5*UD4PI
          CALCULATE VECTOR J OF EQUATION (8.91)
C.
       DO 450 J=1.NTST
       M=MJ(J)
       N=NJ(J)
       QDPI=UD4PI
       IF((J.EQ.4).OF.(J.EQ.61) QDPI=UD8PI
       EI=C(M,N)
       E1M=C(M+1.N)
       E1N=C(M,N+1)
       E7 = -\Delta 2X \neq E1M - 82Y \neq E1N + X(3) \neq E1
       XF=-3.*E7
       O(1) = XF + X(1) - \Delta 2 + FIM
       Q(2) = XF * X(2) - B2 * E15
       Q(3) = XF * X(3) + E1
          USE ONLY MONOPOLE APPROXIMATION IF FIELD POINT SUFFICIENTLY
          DISTANT
       IF(PATIO.GT.DELMD) GO TO 400
       EIMM=C(M+2,N)
       F1MN=C(M+1,N+1)
       EINN=C(M,N+2)
       E2=X(1) \pm E1M+X(2) \pm F1N
       E2M = X(1) * E1MM + X(2) * E1MN
       E2N=X(1) #E1MN+X(2) #E1NN
       F5=A #E1MM+B #E1NN
```

```
F7M=-A2X*E1MM-B2Y*E1MN+X(3)*E1M
      E7N=-A2X#E1MN-B2Y#E1NN+X(3)#E1N
      XF = -3.4E5 - 15.4(X(1) + E7M + X(2) + E7M + X(3) + X(3) + E5)
      Q(1)=Q(1)+U*(XF*X(1)+3.*(E7M-A2*E2M))
      Q(2) = Q(2) + U*(XF*X(2) + 3.*(E7N+P2*E2N))
      Q(3)=C(3)+U*(XF*X(3)+3*(E2+2*X(3)*E5))
 400
      CONTINUE
      00 425 1=1.3
      CI)Q*I9CQ=(I,T)VC
 425
      CONTINUE
 450
      CONTINUE
      00 TO 900
 500
      CONTINUE
          NEAR FIELD CALCULATIONS
C
          DETERMINE ORDER OF H INTEGRALS REQUIRED
      MX 0 = 6
      MXK = 7
          CHECK IF PANEL IS FLAT
C
      LOGAB= (A.EQ.O.).AND.(P.EQ.C.)
       IF(LOGAB) MXC=4
       IF(LOGAB) MXK=5
       IF(NTST.LT.6) MXO=MXQ-1
       IF(NTST.LT.3) MXQ=MXQ-1
Ū
          CALCULATE H INTEGRALS -
      CALL INTCAL
          CALCULATE QUANTITIES FREQUENTLY USED IN SUBSEQUENT
C
          COMPUTATIONS
      CAB = A \times X(1) \times X(1) + B \times X(2) \times X(2) - X(3) + H7
      PIF=PI4T
      X2 = 2. * X(1)
      Y2=2.*X(2)
      \Delta 2X = \Delta 2 \times X(1)
      92Y=82*X(2)
      H3=3.*HZ
      H6=6 . *HZ
      H9=9 .*HZ
      HH3=3.*HZ*HZ
      HH15=15. *HZ*HZ
      HHH15=HZ*HH15
      CALL ZEPO(QEX.3*NTST)
       IF(IH-EQ-0) GO TO 675
          CALCULATE AUXILIARY TERMS OF H INTEGRALS DEFINED BY
          EQUATION (8.51) IF PROCEDURE 3 HAS BEEN EMPLOYED
      SPI2=PI2
       IF(HZ.LT.(0.)) SPI2=-P12
      IF(NTST-LT-3) GO TO 675
      OEX(1,2) = SPI2*(1,+A2*HZ)
      OEY(3,2)=SPI2*(A2X)
      QEY(2,3)=SPI2*(1.+82*HZ)
      QEX(3,3)=SP[2*(B2Y)
      IF(NTST.LT.6) GO TO 675
      QEX(1,4)=SPI2*(4. *A2X*HZ)
```

```
QEX(2,4)=SPI2*(2,*82Y*H7)
      OFX(3,4)=SPI2*(2.*(-HZ*(1.+HZ*(3.*4+B))+CAB))
      QEY(1.5) = SPI2*(82Y*HZ)
      CEX(2,5)=SPI2*(42X*HZ)
      QFX(1,6)=SPT2*(2,*\Delta2X*HZ)
      Q5X(2,6)=SPT2*(4.*B2Y*H7)
      QEX(3,6)=SPIZ*(2.*(-HZ*(1.+HZ*(3.*B+A))+CAP))
 675
      CONTINUE
C
         CALCULATE VECTOR J DEFINED BY EQUATION (8.34)
      DO 750 J=1,NTST
      M≃MJ(J)
      N=NJ(J)
      Q(1) = QEX(1, J) + H3 + H(N+1, N, 5)
      G(2) = QEX.(2, J) + H3 + H(M, M+1, 5)
      O(3) = OEX(3,J) + H(M,N,3) - HH3 + H(M,N,5)
C
          IGNORE TERMS DEPENDING ON CURVATURE IF PANEL IS FLAT
      TECLOGABI GO TO 699
      Q(1) = Q(1)
     C+A+((3.+H(M+3,N,5)-2.+H(M+1,N,3)+HH15+H(M+3,N,7))
     C+Y2*(-H(M,N,3)+HH15*H(M+2,N,7)))
     C+P*((3.*H(M+1,N+2,5)+HH15*H(M+1,N+2,7))+Y2*(HH15*H(M+1,N+1,7)))
     C+CAB*(-3 *H(M+1,N,5)+PP15*H(M+1,N,7))
      Q(2) = Q(2)
     C+A+((3.+F(M+2,N+1,5)+HH15+H(M+2,N+1,7))+X2+(HH15+H(M+1,N+1,7)))
     C+B*((3.*H(M.N+3.5)-2.*H(M.N+1.3)+HH15*H(M.N+3.7))
     C+Y2*(-H(M,N,3)+HH15*H(M,N+2,7))
     C+CAB*(-3.*H(M,N+1.5)+HH15*H(M,N+1.7))
      Q(3) = Q(3)
     C+\Lambda+((H3+H(M+2,N,5)-HHH15+H(M+2,N,7))
     C+X2*(H6*H(M+1,N,5)-HHH15*H(N+1,N,7))
     C+8#((H3#H(M,N+2,5)-HHH15#H(M,N+2,7))
     C+Y2*(H6*H(M,N+1,5)-HHH15*H(M,N+1,7)))
     C+CAB+(H9+H(M,N,5)-HHH15+H(M,N,7))
     CONTINUE
      00 700 I=1.3
      PV(1,J)=PIF*O(I)
 700
      CONTINUE
 750
      CONTINUE
      IF(NTST.LT.3) GO TO 900
ŗ
         REARRANGE COEFFICIENTS AS REQUIRED BY EQUATION (B.31)
      DO 900 T=1.3
      DV(I,2)=DV(I,2)+X(1)+DV(I,1)
      DV(I,3)=DV(I,3)+X(2)*DV(I,1)
      IF(NTST.LT.6) GO TO 800
      DVX=BV([,2)-.5*x(1)*DV([,1)
      DVY = DV(I,3) - .5 * X(2) * DV(I,1)
      DV(I,4)=.5*DV(I,4)*X(1)*DVX
      DV(1,5)=DV(1,5)+X(1)*DVY+X(2)*DVX
      DV(1,6)=.5*DV(1,6)+X(2)*DVY
 800
      CONTINUE
      CONTINUE
 900
      RETUPN
      END
```

```
SUBFCUTINE ECAL(X1, X2, A1, A2, F, N)
(****
       SUBFCUTINE ECAL (X1, X2, A1, A2, F, N)
•
Ç.
C
       PUPPOSE
                  TO EVALUATE E([]=A2*X2**(]-1)-A1*X1**([-1])
                  (SEE EQUATION (8.59), APPENDIX B OF ENGINEERING DOCUMENT)
•
       INPUT
                  CALLING SEQUENCE
                  X1 - (SEE PUPPOSE)
                  X2 - (SEE PURPOSE)
                  A1 - (SEE RURPOSE)
                  A2 - (SEE PURPOSE)
                  N - (SEE PURPOSE)
                  CALLING SPOUFNCE
       CUTPUT
C
                  E - (SEE PURPOSE)
C
       SUBPCUTINES
C
       CALLEC
                 NONE
       DISCUSSION THE ROUTINE CALCULATES THE QUANTITIES
                  F(I)=\Delta 2 \times X \times (I-1)-\Delta 1 \times X \times (I-1) FOR I=1,N USING THE
                  PECURSION FORMULA E(I)=(X1+X2)*E(I-1)-X1*X2*E(I-2)
                  AND THE INITIAL CONDITIONS E(1)=A2-A1 AND
                  F(2)=\Delta 2 \times X2 - \Delta 1 \times X1.
~***
       DIMENSION E(NI
       E(1)=A2-A1
       IF(N.LT.2) GO TO 900
       E(2) = A2 \times X2 - A1 \times X1
       IF(N.LT.3) GO TO 900
       X2PX1=X2+X1
       \times 2T \times 1 = \times 2 \times 1
       DO 10 I=3,N
       E(I) = X2PX1 * E(I-1) - X2TX1 * E(I-2)
 10
 900
       FETUEN
       END
```

```
SUBPCUTINE EDGEIN
[.*****
      SUBROUTINE FOGEIN
Ċ
                TO PROVIDE NEW INDICES FOR THE CONTROL POINTS AND DOUBLET
(
      PUSPCSE
ŗ
                -S SO THAT THE COPRESPONDING EQUATIONS(DOWNASH CONDITION
C
                ) AND DOUBLETS AT EDGES OF NETWORK WILL PRECEDE ALL THE
C
                OTHERS
C
C
                COMMON BLOCK
      INPUT
0
                /BDYCS/ - ITC
C
                /INDEX/ - NOTRY
C
C
      OUTPUT
               COMMON PLOCK
C
                /NINDX/ - NEQ.NUC.IUC
C
C
      SUPRCUTINES
      CALLED
               MONE
C
      DISCUSSION THE ROUTINE OBTAINS THE NUMBER OF EQUATIONS CORRESPOND
C
                -ING TO CONTROL POINTS AT EDGES. THEN IT ASSIGNS INDICES
C
                ACCORDING TO WHETHER CONTROL POINTS ARE AT EDGE OF INTER-
C
C
                IOP.
( ****
      COMMON/PDYCS/7C(3,125),ZCC(3,125),7CP(125),ZDC(125),IPC(125),
                    ITC(125)
      COMMON/INDEX/NT(9).NM(9).NN(9).NP(9).NS(9).NC(9).NZ(9).
     CNPA(10).NSA(10),NCA(10).NZA(10).NNETT.NPANT.NSNGT.NCTRT.NZMPT
      COMMON /NINDX/NEQ.NUC(125), TUC(125)
                          TO OBTAIN THE NUMBER OF EDGE DOWNWASH FOS.
(
      NEO = 0
      DO 10 JC=1,NCTRT
   10 NEQ = NEQ + ITC(JC)
C
                          TO ASSIGN THE INDICES
      LF = 0
      LC = NEQ
      DO 30 JC=1.NCTRY
      IF(ITC(JC).NE.1)
                         GO TO 20
      LE = LE + 1
      NJC(JC) = LE
      IJC(LEI = JC
      CC TC 30
   20 \text{ LC} = \text{LC} + 1
      NJC(JC) = LC
      IJC(LC) = JC
   30 CONTINUE
      FETURN
      FND
```

SURFCUTINE FIVE(ZC, ZNC, ZDC, IPINE) C *: * * * * * SUBPCUTINE EIVC (ZC, ZNC, ZOC, IPINE) C TO CALCULATE THE VELOCITY INDUCED BY A DOUBLET PANEL ON A NETWORK EDGE CONTROL POINT CCALLING SEQUENCE INPUT ZC - COORDINATES OF CONTPOL POINT ZNC - UNIT NORMAL TO SURFACE AT CONTROL POINT C ZDC - DISTANCE FROM CONTROL POINT TO PANEL EDGE COMMON BLOCK /IPPINT/ - IPEIVC /ZIP/ - IPZ.IP.JCZ /PANDQ/ - CP.PC.PG.AR.P.DIAM /SYMM/ - NSYMM CUTPUT CALLING SEQUENCE IPINE - INDICATES WHETHER PANEL IS CLOSE ENUUGH TO CONTROL POINT TO INDUCE A SUBSTANTIAL DOWNWASH C C COMMON - BLOCK /PIVM/ - DVDS SUPPOUTINES CALLED ZERO, CROSS, UNIPAN DISCUSSION THE POUTINE CALCULATES THE VELOCITY INDUCED BY A C C DOUBLET PANEL (AND ITS IMAGE IF CONFIGURATION IS SYMMETRICAL) ON A NETWORK EDGE CONTROL POINT. THE C INFLUENCE IS COMPUTED BY ACCUMULATING THE INFLUENCE OF C EACH PANEL EDGE. THE INFLUENCE OF A PANEL EDGE IS IGNORED UNLESS A POINT ON THE EDGE IS WITHIN A SMALL SPHERE AROUND THE CONTPOL POINT. IN THIS CASE THE INFLUENCE DUE TO BOTH THE DOUBLET STRENGTH AND ITS DERIVATIVE PERPENDICULAR TO THE EDGE (EVALUATED AT THAT EDGE POINT) IS COMPUTED. THE RESULTANT VELOCITY IS THEN DISTRIBUTED AMONG THE COEFFICIENTS OF THE DOUBLET DISTRIBUTION ON THE PANEL. · **** COMMEN/PIVM/DVDS(3.6) COMMON/PANDQ/CP(3,4),PC(3),FC(3),AR(3,3),ART(3,3),P(2,4),A,B,DIAM, 10(6,6),AST(6,16),IIS(16),INS,ITS,NPDQ COMMON/SYMM/NSYMM COMMON /ZIP/IPZ, IP, ITZ, JCZ COMMON /IPRINT/IPNPUT, IPGEOM, IPSING, IPCNTR, IPEIVC, IPOUTP DIMENSION P1(3), P2(3), DF(3), Q(6), W(3), Z(3) DIMENSION ZC(1).ZNC(1) DATA EX /1.1/ TPINE=C EXZDC=EX*ZDC

```
CALL ZEPO(DVDS,19)
      W(1) = ZC(1)
      W(3) = 70(3)
          COMPUTE INFILIENCE OF PANEL AND IMAGE IF NSYMM=1
      DO 200 ISYMM=1.2
       S1CN=3-2*15YMM
      W(2) = SIGN * ZC(2)
      DIST=SOFT((W(1)-PC(1))**2+(W(2)-PC(2))**2+(W(3)-PC(3))**2+
          IGNORE INFLUENCE IF PANEL IS NOT IN
C
          PERXIMITY OF CONTROL POINT
       IF(DIST.GT.DIAM) GO TO 500
          CALCULATE POINT ON PANEL EDGE CLOSEST TO CONTROL POINT
      DD 100 TS=1.4
       ISP1=IS+1
       IF(ISP1.GT.4) ISP1=1
      DO 50 J=1.3
      F1(I)=CP(I,IS)-W(I)
      F2(I)=CP(I, ISP1)-W(I)
      DP(I)=CP(I,ISPI)-CP(I,IS)
 50
      CONTINUE
      DF M = SQPT (DP (1) * #2+DP (2) * *2+DP (3) * #2)
       TE(DEM.LT.ZDC) GO TO 100
      R1M = SOFT(R1(1) + 2 + R1(2) + 2 + F1(3) + 2)
      P2M = SQFT(P2(1) * *2 + P2(2) * *2 + P2(3) * *2)
      T = -(R1(1) + OR(1) + R1(2) + OR(2) + R1(3) + OR(3))/(ORM + + 2)
       IF((RIM.GT.EXZDC).AND.(T.LT.O.)) GO TO 100
       IF((F2M.GT.EXZDC).AND.(T.GT.1.)) GO TO 100
      DO 55 I=1,3
      Z(I) = CP(I \cdot IS) + T \neq DR(I)
 55
      CONTINUE
      CALL CROSS(P1, P2,Q)
      AM=SCRT(C(1) **2+Q(2) **2+Q(3) **2)/DFM
          IGNORE INFLUENCE OF PANEL EDGE IF FOGE IS
          NOT IN PROXIMITY OF CONTROL POINT
C
       IF(AM.GT.EXZDO) GO TO 100
      SP1 = (F1(1) * DF(1) + P1(2) * DF(2) + F1(3) * DF(3)) / (P1M * DFM)
      SP2=(R2(1)*DR(1)+R2(2)*DR(2)+F2(3)*DF(3))/(R2M*DRM)
          CALCULATE MAGNITUDE OF DOWNWASH INDUCED BY DOUBLET
C
          STRENGTH AT PANEL EDGE POINT CLOSEST TO CONTROL POINT
      TF(SP1#SP2.GE.O.) F1=AM#(1./P2M##2-1./F1M##2)/(SP1+SP2)
      IF(SP1*SP2.LT.).) F1=(SP1-SP2)/AM
      T=O(1)*ZNC(1)+O(2)*ZNC(2)+O(3)*ZNC(3)
      IF(T.LF.O.) F1=-F1
      F1 = 700 *F1
          CALCULATE MAGNITUDE OF DOWNWASH INDUCED BY DEFIVATIVE
(
          OF DOUBLET STRENGTH PERPENDICULAR TO FOGE AT PANEL
Ć
          EDGE POINT CLOSEST TO CONTROL PROINT
      IF (SP1.GE.O.) F=ALOG((P2M*(1.+SP2))/(F1M*(1.+SP1)))
       IF(SP2.LE.O.) F=-ALOG((F2M#(1.-SP2))/(F1M#(1.-SP1)))
      IF ((SP1.1T.G.).AND.(SP2.GT.C.))
     CF = \Delta L DG (R2M + (1. + SP2) + F1M + (1. - SP1) / (\Delta M + + 2))
      F = ZDC \neq F
```

```
DP = SQFT((P(1, ISP1) - P(1, IS)) **2+(P(2, ISP1) - P(2, IS)) **2)
      F2=-F*(P(2, ISP1)-P(2, IS))/DP
       F3=F*(P(1,ISP1)-P(1,IS))/DP
       CALL UNIPAN(AP, RO, Z, Z)
C
          CALCULATE DOWNWASH INDUCED BY EACH COEFFICIENT OF
          QUADRATIC DOUBLET DISTRIBUTION ON PANEL
       Q(1)=F1
       Q(2) = F2 + F1 + Z(1)
      O(3) = F3 + F1 * Z(2)
       F4=F2+.5=F1=Z(1)
      F5=F3+.5*F1*Z(2)
       O(4) = 7(1) * F4
       Q(5)=Z(1)*F5+Z(2)*F4
       Q(6)=7(2)*E5
       DO 75 J=1,6
       DVDS(1,J)=DVDS(1,J)+ZMC(1)*Q(J)
       DVDS(2,J) = DVDS(2,J) + SIGN + ZNC(2) + O(J)
       DVDS(3,J) = DVDS(3,J) + 7NC(3) *Q(J)
 75
      CONTINUE
       IF(TPEIVC.NE.O)
      $WRITE(6,1000) JCZ, IPZ, IP, IS, W, F1, F2, F3
 1000 FOPMAT(415,6E15.6)
       IPINF=1
       CONTINUE
 100
       IF(NSYMM.FQ.O.) GO TO 500
       CONTINUE
 200
       PETUEN
 500
       FND
```

```
SUBFCUTINE FMNCAL
( ******
C
      SUBPCUTINE FMNCAL
Ç
C
      PUPPCSE
                TO CALCULATE CERTAIN F INTEGRALS USED TO COMPUTE THE H
C
                INTEGRALS INVOLVED IN THE FORMULAS FOR THE SOURCE AND
C
                DOUBLET PAMEL INDUCED VELOCITY INFLUENCE COEFFICIENTS.
                (SEE SECTION 8.3 OF APPENDIX B OF THE ENGINEERING
C
                DOCUMENT.)
C
C
      IMPUT
                COMMON BLOCK
                /INTQ/ - MXQ
C
                /SKATCL/ - LMXQ2,LMXQ3
                /SKAICI/ - AKSI,AETI,AKS2,AET2,ANK,ANE,A,AA,S1,S2,HH
C
Ç
      CUTPUT
                COMMON BLOCK
C
                /SKATCZ/ - GKMN, GEMN, GAMN
C
C
      SUBREUTINES
C
              ECAL
      CALLED
C
      DISCUSSION
                   THE POUTINE COMPUTES THE INTEGRALS F(M. N. 1) FOR
                N=1,MXQ AND M=1,MXQ-N+1 WHEFF
                F(M,N,1)=I(L,KSE**(M-1)*ET&**(N-1)/RHO,DL). A DESCRIPTION
Ç
                OF THE CALCULATIONS PERFORMED IS CONTAINED IN SECTION 0.3
C
                OF APPENDIX 8 OF THE ENGINEEPING DOCUMENT. THE PELEVANT
C
                FQUATIONS APE (8.62). (8.63). (8.64) AND (8.65). THE
                RELEVANT PROCEDURES ARE 4 AND 5. THE CODE CLOSELY
C
                FULLOWS THE DEVELOPMENT AND NOTATION OF SECTION 8.3.
                NOTE THAT FMN(M.N)=F(M.N.1).
C
LMXO2, LMXO3, LMXG4, LMXK3, LMXK5, LMKEX
      LOGICAL
      COMMON/INTO/H(6,6,7), HZ, IH, MXQ, MXK
      COMMON/SKAICL/LMXG2,LMXG3,LMXG4,LMXK3,LMXK5,LMKEX
      COMMON/SKAIC1/AKS1,AFT1,AKS2,AET2,DPM,EL1,EL2,ELM,ANK,AME,A,AA,
     CGG, S1, S2, S11, S21, HM, HH
      CCMMCN/SKAIC2/GAK(21).GKNK(5.5).GENK(5.5).GKMN(6.6).GEMN(6).
     CGAMN(6,6),H111,FK(37),FNK(6,5),FMN(6,6),F(37)
          INITIALIZE F(M.M.I) INTEGRALS
C
      FMN(1,1) = FK(1)
      IF(LMYQ2) GO TO 500
          BRANCH TO STEP (3.A) OF (3.B) OF PROCEDURE 4 PESPECTIVELY
Ç
      IF(ABS(ANE)-ABS(ANK)) 100,100,200
 100
      CONTINUE
      C1=A *ANE
      C3 = 4NK
         EXECUTE STEP (3.A.I) (EQUATION (8.62)) OF PROCEDURE 4
C
      CALL FCAL (AFT1. AFT2, S1. S2. F. MXQ-1)
      FMN(1,2) = C1 * FMN(1,1) + C3 * E(1)
      IF(LMXQ3) GO TO 150
      C2 = -(\Delta \Delta + HH + \Delta NK + \Delta NK)
      DO 130 N=3, MXQ
```

```
FMN(1,N)=(FLOAT(2*N-3)*Cl*FMN(1,N-1)+FLOAT(N-2)*C2*FMN(1,N-2)
      C+C3*E(N-1))/FLGAT(N-1)
 150
       Al =- ANE/ANK
       \Delta 2 = \Delta / \Delta N K
C
           EXECUTE STEP (3.4.II) (EQUATION (8.63)) OF PROCEDURE 4
       DO 170 M=2,MXQ
       MXN=MXC-M+1
       DO 170 N=1, MXN
       FMN(P,N)=\Delta! \neq FMN(M-1,N+1)+\Delta2\neq FMN(M-1,N)
       GO TC 500
       CONTINUE
 200
       C1=A*ANK
       C3=-ANE
          EXECUTE STEP (3.8.1) (EQUATION (8.64)) OF PROCEDUPE 4
C
       CALL SCAL(AKS1, AKS2, S1, S2, E, MXQ-1)
       FMN(2,1)=C1*FMN(1,1)+C3*E(1)
       IF(LMXQ3) GD TO 250
       C2 = -(AA + HH + ANE + ANE)
       DO 230 M=3, MXQ
      -\text{FMN}(M,1) = (\text{FLOAT}(2 \pm M - 3) \pm C1 \pm \text{FMN}(M + 1, 1) + \text{FLOAT}(M - 2) \pm C2 \pm \text{FMN}(M - 2, 1)
     C+C3*E(M-1))/FLD4T(M-1)
 250
      Al =- ANK/ANE
       A2=A/ANE
          EXECUTE STEP (3.R.II) (EQUATION (8.65)) OF PROCEDURE 4
       DO 270 N=2. MXO
       MXM=MXQ-N+1
       DO 270 M=1, MXM
 270
       FMN(N,N) = A1 + FMN(M+1,N-1) + A2 + FMN(M,N-1)
 500
       CONTINUE
           ACCUMULATE CONTRIBUTION OF QUADPILATERAL SIDE TO F
C
           INTEGRALS FOR USE IN STEP 3 (EQUATION (8.43)), STEP 4
Ç
C
          (EQUATION (8.44)) AND STEP 5 (EQUATION (8.45))
C
          OF PROCEDURE 1
       DG 690 N=1, MXQ
       GEMN(N)=GEMN(N)+ANE*FMN(1.N)
       M \times M = M \times Q - M + 1
       PO 680 M=1, MXM
       GKMN(M,N)=GKMN(M,N)+ANK*FMN(M,N)
       GAMN(M,N)=GAMN(M,N)+A*FMN(M,N)
 680
 690
       CONTINUE
       PETUPN
 999
       END
```

```
SUBROUTINE FAKCAL
C ****
C
      SUPPOUTINE FORCAL
ς,
      PUPPCSE
                TO CALCULATE CEFTAIN F INTEGRALS USED TO COMPUTE THE H
                INTEGRALS INVOLVED IN THE FORMULAS FOR THE SOURCE AND
                DOUBLET PANEL INDUCED VELOCITY INFLUENCE COEFFICIENTS.
C
                (SEE SECTION 8.3 OF APPENDIX 8 OF THE ENGINEERING
^
                DOCUMENT.)
      INPUT
                COMMON BLOCK
C.
                /SKATCL/ - LMXQ3,LMXQ4,LMXK5
                /SKAICI/ - ANK, ANF, AA, SII, S2I, HH
C.
                /SKAICI/ - MXKM2.MXQM1
      GUTPUT
                COMMON BLOCK
                /SKAIC2/ - GKNK.GENK
      SUBFOUTINES
Ç
      CALLED
               FC4L
Ċ
      DISCUSSION THE POUTINE COMPUTES THE INTEGRALS E(1, N, K) FOR .
                N=2, MXQ AND K=3, MXK-2, 2
                                          MHERE
                F(1,N,K)=I(L,FTA**(N-1)/9HO**K,DL). A DESCRIPTION OF THE
                CALCULATIONS PERFORMED IS CONTAINED IN SECTION 8.3 OF
                APPENDIX B OF THE ENGINEERING COCUMENT. THE RELEVANT
                FOUATIONS ARE (P.66) AND (B.67). THE RELEVANT PROCEDURES
C
                ARE PROCEDURES 4 AND 5. THE CODE CLOSELY FOLLOWS THE
                DEVELOPMENT AND NOTATION OF SECTION 8.3. NOTE THAT
C
^
                FNK(N,K)=F(1,N,K).
(, * * * * * *
      LOGICAL
                     LMXQ2,LMXQ3,LMXQ4,LMXK3,LMXK5,LMKEX
      COMMON/SKAICL/LMXQ2,LMXQ3,LMXQ4,LMXK3,LMXK5,LMKEX
      COMMON/SKATC1/4KS1,AET1,AKS2,AET2,DRM,EL1,EL2,ELM,ANK,ANE,A,AA,
     CGG, SI, S2, S1I, S2I, HM, HH
      COMMCN/SKAIC2/GAK(21), GKNK(5,5), GENK(5,5), GKMN(6,6), GEMN(6),
     CGAMN(6,6),H111,FK(37),FNK(6,5),FMN(6,6),E(37)
      COMMON/SKAICI/MXFK, MXFKN, MXFNK, MXKM2, MXKM4, MXQM1
C
         EQUATIONS AND PROCEDURED REFERENCED IN THIS ROUTINE
C.
         ARE CONTAINED IN APPENDIX B IN ENGINEERING DOCUMENT
C
         INITIALIZE THE ARRAY FNK USING PREVIOUSLY COMPUTED INTEGRALS
C
      DO 100 K=1.MXKM2.2
 100
      FNK(1,K)=FK(K)
      TE(LMXG3) GO TO 500
      DO 150 N=2, MXOM1
      FNK(N,1)=FMN(1,N)
 150
      TE(LMXK5) GO TO 500
C
         EXECUTE STEPS 4 AND 5 OF PROCEDURE 4 OF 5
      CALL FCAL(SII,SZI,I.,I.,E,MXKM2-1)
      DD 250 K=3, MXKM2, 2
      C1 = 4 * 4NE
```

```
Ç
          STEP 4 (EQUATION 8.66)
      FNK(2,K)=C1*FNK(1,K)-ANK*E(K-1)/FLOAT(K-2)
       IF(LMX04) GO TO 250
      (1=2.*(1
      C3=ANK#ANK
      C2 = -(\Delta A + C3 + HH)
C.
          STEP 5 (EQUATION B.67)
      DO 200 N=3.MXQM1
 200
      ENK(N,K) = C1 + ENK(N-1,K) + C2 + ENK(N-2,K) + C3 + ENK(N-2,K-2)
 250
      CONTINUE
 500
      CONTINUE
          ACCUMULATE F INTEGRALS OVER ALL FOUR SIDES OF QUADRILATERAL
Ć
          FOR USE IN STEPS 6 (FQUATION, B.46) AND 7 (EQUATION 8.47)
Ç
C
          OF PROCEDURES 1, 2 AND 3
      DO 690 K=1, MXKM2, 2
      DO 680 N=1, MXQM1
       GKNK(N,K)=GKNK(N,K)+ANK*FNK(N,K)
 680
      GENK(N,K)=GENK(N,K)+ANE*FNK(N,K)
 690
      CONTINUE
 999
      RETURN
       FND
```

```
SURFCUTINE FKCAL
( *****
      SUBFICUTINE FROAL
Ç
C
                TO CALCULATE CERTAIN E INTEGRALS USED TO COMPUTE THE H
      PURPOSE
C
                INTEGRALS INVOLVED IN THE FORMULAS FOR THE SOURCE AND
                DOUBLET PANEL INDUCED VELOCITY INFLUENCE COEFFICIENTS.
                (SEE SECTION B.3 OF APPENDIX B OF THE ENGINFERING
                DOCUMENT.1
      IMPUT
                COMMON BLOCK
                /SKAICL/ - LMKEX
C
                /SKAIC1/ - EL1, EL2, ELM, A, AA, GG, S1, S2, S11, S21, HM
C
                /SKAICI/ - MXFK
C
      CUTPUT
                COMMON BLOCK
C
                /SKAICI/ - MXFKN
r
                /SKAIC2/ - GAK, HIII
C
Č
      SUPPOUTINES
Č
      CALLED
               ECAL
C
      DISCUSSION THE ROUTINE COMPUTES THE INTEGRALS F(1,1,K) FOR
                K=1.MXFK WHERE F(1,1.K)=I(L,1./PHD**K,DL). A DESCRIPTION
                OF THE CALCULATIONS PERFORMED IS CONTAINED IN SECTION 8.3
                OF APPENDIX B OF THE ENGINEERING DOCUMENT. THE RELEVANT
                EQUATIONS ARE (8.50), (8.61), (8.68) AND (8.69). THE
Ç
                RELEVANT PROCEDURES ARE 4 AND 5. THE ROUTINE ALSO
Ç
                COMPUTES THE APCTANGENT TERMS OF STEP 1 (EQUATION (8.41))
                OF PROCEDURE 1. THE CODE CLOSELY FOLLOWS THE DEVELOPMENT
C
                AND NOTATION OF SECTION 8.3. NOTE THAT FNK(N,K)=F(1,N,K).
( * * * * * *
      LOGICAL
                     LMXQ2,LMXQ3,LMXQ4,LMXK3,LMXK5,LMKEX
      COMMON/SKAICE/LMXQ2.LMXQ3.LMXQ4.LMXK3.LMXK5.LMKEX
      COMMON/SKAIC1/AKS1.AET1.AKS2.AET2.BRM.EL1.EL2.ELM.ANK.ANE.A.AA.
     CGG, S1, S2, S11, S21, HM, HH
      COMMEN/SKAIC2/GAK(21).GKNK(5.5).GENK(5.5).GKMN(6.6).GEMN(6).
     CGAMN (6,6), H111, FK (37), FNK (6,5), FMN (6,6), E(37)
      COMMON/SKAICI/MXFK.MXFKN,MXFNK,MXKM2.MXKM4.MXQM1
      DATA DELEKS, NEK 1.01, 16/
C
         EQUATIONS AND PROCEDURES REFERENCED IN THIS ROUTINE
¢
         ARE CONTAINED IN APPENDIX B OF THE ENGINEERING DOCUMENT
\mathbf{C}
         EXECUTE STEP 1 OF PROCEDURE 4 (EQUATION (8.60))
      IF(EL2) 10,10,20
 10
      FATIC=(S1-EL1)/(S2-EL2)
      GC TC 50
 20
      IF(EL1) 30,30,40
 30
      FATIC=(S1-EL1)*(S2+EL2)/GG
      GO TO 50
 40
      PATIC=($2+EL2)/($1+EL1)
 50
      FK(1)=ALCG(PATIO)
```

```
IF(LMKEX) 60,55
 55
      C1=GG+HM*S1
      C2=GG+HM*S2
         CALCULATE AND ACCUMULATE CONTRIBUTION OF QUADFILATERAL
          SIDE TO ARCTANGENT TERM OF H(1,1,1) AS DEFINED BY
C
          STEP 1 (EQUATION (8.41)) OF PROCEDURE 1
C
      P111=H111+A*FK(1)-HM*ATAN2(A*(C1*FL2-C2*EL1),C1*C2+AA*FL1*FL2)
      JF(MXFK.LT.3) GO TO 500
 60
          BRANCH TO PROCEDUPE 5 OF 4 RESPECTIVELY
C .
      IF(GG.LT.DELFKS*(FLM*ELM+GG)) 400,200
      CONTINUE
 200
      MXFK N=MXFK
          EXECUTE STEP 2 (FOUATION (B.61)) OF PROCEDURE 4
С
      CALL ECAL(SIT, S2I, EL1, EL2, F, MXFK-1)
      DO 250 K=3, MXFK, 2
      FK(K) = (FLOAT(K-3) \neq FK(K-2) + F(K-1)) / (FLOAT(K-2) \neq GG)
 250
      GO TO 500
 400
      CONTINUE
      MXFKN=MXFK+NFK
          EXECUTE STEPS 1 AND 2 (EQUATION (9.68) AND (8.69))
C
          OF PROCEDURE 5
      CALL ECAL(SII, S2I, EL 1, EL 2, E; MXFKN-1)
      FK(MXFKN)=0.
      DO 450 KP=5, MXFKN, 2
      K=MXFKN+5-KP
      FK(K-2)=(FLGAT(K-2)*GG*FK(K)-E(K-1))/FLGAT(K-3)
 450
 500
      CONTINUE
          ACCUMULATE CONTRIBUTION OF QUADRILATERAL SIDE TO F
          INTEGRALS FOR USE IN STEP 1 (EQUATION (8.411) AND 2
C
         (EQUATION (B.42)) OF PROCEDURE 1 AND STEP 2
C
          (FOUATION (8.50)) OF PROCEDURE 2
C
      DO 600 K=1, MXFK, 2
      GAK(K) = GAK(K) + A \neq FK(K)
 600
      PETURN
 999
      END
```

```
SUBFOUTINE GCPCAL (NM, NN, NM1, NN1, ZM, ZA)
· *****
      SUPPOUTINE GCPCAL (NM, NN, NM1, NN1, ZM, 7A)
C
Ç,
                TO CONSTRUCT AN NM+1 BY NM+1 GRID OF POINTS FROM CORNER
€
      PURPOSE
C
                POINT DATA
      THPUT
                CALLING SEQUENCE
                NM - NUMBER OF CORNER POINTS IN A ROW
                NN - NUMBER OF CORNER POINTS IN 4 COLUMN
                NMI - NUMBER OF GRID POINTS IN A ROW (NM+1)
                NNI - NUMBER OF GRID POINTS IN A COLUMN (NN+1)
                ZM - COUPDINATES OF CORNER POINTS:
               CALLING SEQUENCE
C
      CHIPUT
                ZA - COORDINATES OF GRID POINTS
      SUBSCUTINES
C
      CALLED
               NONE
      DISCUSSION THE ROUTINE COMPUTES AN NM+1 BY NN+1 GRID OF POINTS
               DEPIVED FROM CORNER POINT DATA. THE POINTS IN THE GRIC
                CONSIST OF THE AVERAGE OF TACH SET OF FOUR ADJACENT
               CORNER POINTS, THE AVERAGE OF EACH SET OF THO ADJACENT
                EDGE CORNER POINTS AND THE EGUR EXTREME CORNER POINTS.
                THESE POINTS ARE OBTAINED BY COMPUTING APPROXIMATE
                AVERAGES OF THE CORNER POINTS.
      DIMENSION ZM(3.NM, NN), ZA(3, NM1, NN1)
      DO 99 N=1,NN1
      NI = MAXO(N-1,1)
      NZ=MINC(N.NN)
      1M1.1=M 80 00
      M1 = MAXO(M-1,1)
      M2=MINO(M.NM)
      ne 90 t=1.3
      ZA(L,M,N)=.25*(ZM(L,M1,N1)+ZM(L,M2,N1)+ZM(L,M1,N2)+ZM(L,M2,N2))
 an
      CONTINUE
 0.8
      CONTINUE
 99
      CONTINUE
      RETURN
      E NO
```

```
SUBROUTINE GEOMC(NT, NM, NN, NPA, ZM)
( *******
      SUPROUTINE GEOMO (NT.NM.NN.NPA.ZM)
C
C
Ç
      PUFPOSE
                TO CALCULATE GEOMETRIC DEFINING QUANTITIES FOR EACH PANEL
C.
                IN A NETWORK
C
C
                CALLING SEQUENCE
      INPUT
Ç
                NT - NETWORK TYPE
C
                NM - NUMBER OF SPANWISE CUTS IN NETWORK
                NN - NUMBER OF TRANSVERSE CUTS IN NETWORK
C
                NPA - TOTAL NUMBER OF PANELS IN ALL PREVIOUS NETWORKS
                ZM - COORDINATES OF CORNER POINTS IN THE NETWORK
C
C
                COMMON BLOCK
                /IPFINT/ - IPGEOM
C
      TUPTUD
                COMMON BLOCK
C
                /PANDO/ - CP,PC,RC,AR,ART,P,A,B,DIAM,C
C
      SUPPOUTINES
C
                SURFIT, CCAL, IPTRNS
      CALLED
C
      DISCUSSION THE POUTING CALCULATES AND STORES GEOMETRIC DEFINING
                QUANTITIES FOR EACH PANEL OF A NETWORK. FIRST THE FOUR
C
C
                GRID POINTS DEFINING THE PANEL CORNER POINTS ARE FOUND.
C
                TOGETHER WITH ADJACENT GRID POINTS THESE CORNER POINTS
C
                ARE FED INTO SURFIT WHICH DEFINES THE ACTUAL PANEL
Ç
                SURFACE AND THE LOCAL PANEL COORDINATE SYSTEM. THEN COAL
C
                IS CALLED TO CALCULATE PANEL MOMENTS. FINALLY. ALL THE
C
                PANEL DEFINING QUANTITIES ARE STORED ON A FILE.
· ******
      CCMMON/LSQSFC/ZK(3,16),WTK(16),AK(6,16),NO,NPK
      COMMON/PANDO/CP(3,4),PC(3),FO(3),AF(3,3),AFT(3,3),P(2,4),A,R,DTAM,
     CC(6,6),AST(6,16),IIS(16),INS,ITS,NPDQ
      COMMON / IPRINT/IPNPUT, IPGECM, IPSING, IPCNTP, IPOUTP
      DIMENSION ZM(3.NM.NN)
      DATA WT /1.E5/
      IF(IPGEOM.NE.O) PRINT 1001
 1001 FORMAT(1H1)
         CYCLE THROUGH ALL PANELS IN THE NETWORK
      DO 199 N=2.NN
      DC 198 M=2.NM
      IP=M-1+(NM-1)\neq (N-2)+NPA
         ASSEMBLE FOUR GRID POINTS DEFINING THE PANEL
C
      DO 110 L=1.3
      CP(L,1) = ZM(L,M-1,N-1)
      CP(L,2)=ZM(L,M-1,N)
      CP(1..3) = ZM(L.M.N)
      CP(L,4)=ZM(L,M,N-1)
 110
      CONTINUE
         ASSEMBLE ADJACENT GRID POINTS AND RESPECTIVE
```

```
C
         WEIGHTS FOR DEFINING CURVED PANEL SURFACE
      NPK=0
      no 129 J=1.4
      NJ=MING(MAXO(N+J-3,11,NN)
      00 128 1=1,4
      MI = PINO(MAXO(M+I-3.1).NM)
      NPK=NPK+1
      WIK(NPK)=1.
      TF(((I.EQ.2).09.(I.EQ.3)).AND.((J.EQ.2).09.(J.EQ.3))) WTK(NPK)=WT
      DO 120 L=1.3
      ZK(L,NPK)=ZN(L,MI,NJ)
      IF((NN.EQ.2).AND.((J.EQ.1).OF.(J.FQ.4)))
     C7K(L,NPK)=.5*(ZM(L,MT,1)+ZM(L,MI,2))
      IF((AM.FQ.2).AND.((I.FQ.1).OR.(1.EQ.4)))
     CZK(L,NPK) = .5*(ZM(L,1,NJ) + ZM(L,2,NJ))
 120
     CONTINUE
123
     CONTINUE
      CONTINUE
 129
      IF(IPGECM.ME.O) PRINT 2002, IP
 2002 FOFMAT(//# PANEL*, 14)
         DEFINE PANEL SURFACE
      CALL SUFFIT
      CALL TRANS (AR. ART, 3, 3)
C
         CALCULATE PANEL CHARACTERISTIC LENGTH
      D13= SORT((P(1,3)-P(1,1)) \neq 2+(P(2,3)-P(2,1)) \neq 2)
      024=SQRT ((P(1,4)-9(1,2))**2+(P(2,4)-9(2,2))**2)
      DIAM=AMAX1(D13.024)
C
         CALCULATE PANEL MOMENTS FOR LATER USE IN
         INFLUENCE COEFFICIENT CALCULATIONS
      CALL COAL(P.C)
C
         STORE PANEL DEFINING QUANTITIES ON A FILE
      CALL IPTENS(IP)
                       PRINT 1002, CP,PC,PO,AR,P,A,B,DIAM
      IF (IPGEOM.NE.O)
 1002 FORMAT(6F15.6)
 198
     CONTINUE
 199
      CONTINUE
      PETURN
      END
```

```
SUBFOUTINE GROIND(NM, NN, Z, I, IS)
C ****
C
      SUBFCUTINE GROIND (NM.NN.Z.I.IS)
                TO ORDER NON-IDENTICAL POINTS OF AN NM BY NN GRID OF
      PURPOSE
C
                POINTS VIA AN INDEX ARRAY
C
      IMPUT
                CALLING SEQUENCE
                NM - NUMBER OF GRID POINTS IN A ROW
                NN - NUMBER OF GRID POINTS IN A COLUMN
C
                Z - COORDINATES OF GRID POINTS
C
      OUTPUT
                CALLING SEQUENCE
                I - INDEX APRAY CONTAINING SEQUENCE NUMBER OF FACH GRID
C
                    POINT
                IS - TOTAL NUMBER OF NON-IDENTICAL POINTS IN A GEID
C
C
C
      SUBROUTINES
              PIDENT
      CALLED
C
C
C
      DISCUSSION THE FOUTINE SEQUENCES AN NM BY NN GRID OF POINTS.
                THE SEQUENCING PROCEEDS IN THE OPDER ((M=1,NM),N=1,NN)
                WHERE (M.N) IS THE POINT IN POW M AND COLUMN N. ANY POINT
C
                IDENTICAL WITH THE POINT IN THE SAME ROW AND PREVIOUS
                COLUMN OR WITH THE POINT IN THE SAME COLUMN AND PREVIOUS
                ROW IS ASSIGNED THE SAME SEQUENCE NUMBER AS THAT POINT.
C
                THE SEQUENCE NUMBERS OF THE GRID POINTS ARE STORED IN AN
C
                NM X NN INDEX ARRAY AND RETURNED AS DUTPUT ALONG WITH THE
C
                TOTAL NUMBER OF NON-IDENTIFIED POINTS.
C
C *****
      LOGICAL IDENT
      DIMENSION Z(3,NM,NN), I(NM,NN)
C
         INITIALIZE SEQUENCE NUMBER
      15=0
         CYCLE THROUGH GRID POINTS COLUMN-WISE
      DO 99 N=1.NN
         CYCLE THROUGH COLUMN FOW-WISE
      DO 98 M=1,NM
      IDENT= . FALSE.
         CHECK IDENTITY WITH POINT IN SAME COLUMN AS PREVIOUS FOW
C
      IF(M.GT.1) CALL PIDENT(Z(1, M.N),Z(1, M-1,N),IDENT)
      IF(IDENT) I(M,N)=I(M-1,N)
      IF(ICENT) GC TO 98
(
         CHECK IDENTITY WITH POINT IN SAME ROW AND PREVIOUS COLUMN
      IF(N.GT.1) CALL PIDENT(Z(1, M, N), Z(1, M, N-1), IDENT)
      IF(IDENT) I(M,N) = I(M,N-1)
      IF(IDENT) GO TO 98
         RUMP SEQUENCE NUMBER IF POINT IS NEW
      IS= IS+-1
      I(M, N)=IS
      CONTINUE
 QB
 99
      CONTINUE
      RETURN
      END
```

```
SUBPCUTINE INTOAL
( ****
Ç
      SUBPEUTINE INTOAL
C
C
      PHRPCSE
                TO COMPUTE THE HINTEGRALS INVOLVED IN THE FORMULAS FOR
C
                THE SOURCE AND DOUBLET PANEL INDUCED VELOCITY INFLUENCE
C
                COEFFICIENTS. (SEE SECTION 8.3 OF APPENDIX 8 OF THE
C
                ENGINEERING DOCUMENT.)
      TNPUT
                COMMON BLOCK
Ċ
                /INTO/ - MXO.MXK
C
                /PIVINT/ - X.P.AC.BC.DIAM
C
Ç
                COMMON BLOCK
      CUTPUT
C.
                /INTQ/ - H.H7.IH
      SUBPOUTINES
C
      CALLED
                SIDECL, 7 FRO, TRNSFR, FKCAL, FMNCAL, FNKCAL
C
C
      DISCUSSION THE ROUTINE CALCULATES THE INTEGRALS
C
                H(M,N,K)=I(SIGMA,KSE**(M-1)*ETA**(N-1)/RHO**K,DKSE*DFTA)
¢
                FOR M=1.MXQ AND N=1.MXQ+M+1 AND K=1.MXK.2.
C
                A DESCRIPTION OF THE CALCULATIONS PERFORMED IS CONTAINED.
ŗ
                IN SECTION 8.3 OF APPENDIX 8 OF THE ENGINEERING
C
                DOCUMENT. THE POUTINE CAN BE DIVIDED INTO THREE PARTS.
C
                IN THE FIRST PART PRELIMINARY QUANTITIES CONCERNING THE
                GEOMETRIC RELATIONSHIP OF THE FIELD POINT TO THE
C
                QUADRILATERAL ARE CALCULATED. IN THE SECOND PART THE
C
               F INTEGRALS ARE CALCULATED FOR EACH SIDE OF THE
Ċ
                QUADRILATERAL AND ACCUMULATED. IN THE THIFD PART
C.
                PROCEDURE 1.2 OR 3 IS EXECUTED.
C *** ***
                     LMXC2.LMXQ3.LMXC4.LMXK3.LMXK5.LMKEX
      LOGICAL
      COMMON/INTO/H(6,6,7), HZ, IH, MXQ, MXK
      COMMON/PIVINT/X(3),P(2,4),4C,BC,D14M,C(6,6),DV(3,6),NTST,NCF
      COMMON/SIDEQ/QSIDE(12.4)
      COMMON/SKATCL/L 4XQ2, LMXQ3, LMXQ4, LMXK3, LMXK5, LMKFX
      COMMON/SKAICI/AKS1,AET1,AKS2,AFT2,DPM,FL1,EL2,FLM,ANK,ANF,A,AA,
     CGG, S1, S2, S11, S21, HM, HH
      COMMON/SKAIC2/GAK(21),GKNK(5,5),GENK(5,5),GKMN(6,6),GEMN(6),
     CGAMN(6,6),H111,FK(37),FNK(6,5),FMN(6,6),E(37)
      COMMON/SKAICT/MXFK, MXFKN, MXFNK, MXKM2, MXKM4, MXQMI
      DIMENSION Q(2)
      DATA DELTH /.01/
      DATA DELTHY /1.E-8/
      DATA NHKEX /16/
         FCUATIONS AND PROCEDURES REFERENCED IN THIS ROUTINE ARE
         CONTAINED IN APPENDIX 8 OF THE ENGINEERING DOCUMENT
C
         CALCULATE QUANTITIES ASSOCIATED WITH GEOMETRICAL PELATIONSHIP
         OF FIELD POINT TO QUADRILATERAL
```

CALL SIDECLIQ.DSMIN.D)

```
CALCULATE H OF EQUATION (8.14)
C
      HZ = X(3) - AC \neq O(1) \neq O(1) - BC \neq O(2) \neq O(2)
       TECABS(H7).LT.DELTHZ*DIAM) HZ=0.
      HM=ABS(H7)
      HH=H7*H7
      LMKEY=HM.LT. (DELTH*DSMIN)
      TH=0
       IF(LMKEX.AND.(D.EQ.O.)) IH=1
(,
          SET INDICES AND LOGICAL VAPIABLES FOR FUTURE BRANCHES
      MXKM2=MXK-2
      MXKM4=MXK-4
      MXCMI=MXC-I
      LMYQZ=MXG.LT.2
      LMXQ3=MXQ.LT.3
      LMXO4=MXQ.LT.4
      LMXK3=MXK.LT.3
      LMXK5=MXK.LT.5
      MXFK=MXK-2
      IF(LMKEX) MXFK=MXFK+NHKEX
      CALL ZEFO(GAK, 150)
          CALCULATE AND ACCUMULATE F INTEGRALS OVER FOUR SIDES
C
C
          OF QUADRILATERAL
      DO 500 IS=1.4
      CALL TENSEF(QSIDE(1, IS), AKS1, 12)
C
           IGNORE SIDE IF LENGTH IS ZERO
      IF(DPM.EQ.O.) GO TO 500
          CALCULATE FURTHER QUANTITIES ASSOCIATED WITH
C
          RELATIONSHIP OF FIELD POINT TO QUADRILATERAL
C
      GG=AA+HH
      S1S=FL1*EL1+GG
      S2S=EL 2*EL 2+GG
      S1 = SCRT(S1S)
      S2 = SORT(S2S)
      S11=1./S1
      S2I=1./S2
          CALCULATE F(1,1,K) INTEGRALS
      CALL FKCAL
      IF(LMXQ2) GO TO 500
          CALCULATE F(M.N.1) INTEGRALS
C
      CALL FMNCAL
      IF(LMXK3) GO TO 500
         CALCULATE F(1, N,K) INTEGRALS
C
      CALL FNKCAL
 500
      CONTINUE
C
          BRANCH TO PROCEDURE 1 OF PROCEDURE 2
      IF(LYKEX) 675,625
          EXECUTE STEP 1 OF PROCEDURE 1
 525
      H(1,1,1)=H111
      IF(LMXK3) GO TO 700
         EXECUTE STEP 2 (EQUATION (8.42)) OF PROCEDURE 1
C
      DO 650 K=3, MXK,2
 650
      H(1,1,K)=(FLOAT(K-4)*H(1,1,K-2)+G\Delta K(K-2))/(FLOAT(K-2)*HH)
```

```
GO TO 700
C
          EXECUTE STEP 1 (EQUATION (8.49)) OF PROCEDURE 2
 575
C.
          FXECUTE STEP 2 (EQUATION (B.50)) OF PROCEDURE 2
      DO 580 KP=2,NHKEX.2
       K=NHKEX+MXK-KP+2
      7 = (HH + FLOAT(K-2) + Z - GAK(K-2)) / FLOAT(K-4)
      H(1, 1, MYK) = Z
       IF(LMXK3) GO TO 700
      DO 650 KP=3.MXK.2
      K=MYK-KP+3
 690
      H(1,1,K-2) = (HH \neq F \cup GAT(K-2) \neq H(1,1,K) + GAK(K-2)) / F \cup GAT(K-4)
 700
       TELL MX G21 GO TO 999
C
          EXECUTE STEPS 3 AND 4 (EQUATION (8.43) AND (8.44))
C
          OF PROCEDURE 1
      H(1, 2, 1) = .5 + (HH + GFMN(1) + GAMN(1, 2))
      MYN=MXQ-1
      DO 750 N=1.MXN
      H(2, N, 1) = (HH*GKMN(1, N)+GAMN(2,N))/FLOAT(N+1)
 760
       IF(LYXQ3) SO TO 800
      DG 770 N=3.MXQ
      H(1,N,1)=(HH*(-FLGAT(N-2)*H(1,N-2,1)+GEMN(N-1))+GAMN(1,N))/.
 770
     CELCAT(N)
C
          EXECUTE STEP 5 (EQUATION (8.451) OF PROCEDURE 1
      DO 790 M=3.MXQ
      M \times N = M \times Q - M + 1
      DO 780 N=1.MXN
     H(M,N,1)=(HH\pm(-FLOAT(M-2)\pm H(M-2,N,1)\pm GKMN(M-1,N))\pm GAMN(M,H))/
     CELCAT(M+N-1)
      CONTINUE
 700
 800
       IF(LMYK3) GD TO 999
          EXECUTE STEPS 5 AND 6 (EQUATIONS (R.46) AND (B.47))
C
          OF PROCEDURE 1
C
      DO 890 K=3.MXK.2
      FACTK=1./FLMAT(K-2)
      MXN=MXO-1
      00 970 N=1.MXN
 870
      H(2,N,K) = -EACTK * GKNK(N,K-2)
      H(1,2,K)=-FACTK*GENK(1,K-2)
      IF(LMXQ3) GC TO 890
      DD 880 N=3.4X0
 880
      H(1,N,K) = FACTK*(FLOAT(N-2)*H(1,N-2,K-2)-GENK(N-1,K-2))
 990
      CONTINUE
 900
      IF(LMXQ3) GO TO 999
          EXECUTE STEP 8 (FQUATION (8.48) OF PROCEDURE 1
C
      DO 990 K=3, MXK, 2
      00 990 M=3, MXO
      MYN = MXQ - M + 1
      DC 990 N=1.MXN
      H(M,N,K)=-H(M-2,N+2,K)-HH+H(M-2,N,K)+H(M-2,N,K-2)
 990
 999
      RETURN
      END
```

```
SUBREUTINE KSORT (A, M, N, KEY, W)
C ****
      SUBPOUTINE KSORT
C
C
C
               TO SORT THE COLUMN OF A TWO-DIMENSIONAL ARRAY USING THE
C
                GIVEN KEY INDEX ARRAY
С
C
      INPUT
                CALLING SEQUENCE
Ć
                4 - ARRAY OF WHICH THE COLUMN IS TO BE SORTED
                M - NUMBER OF ROWS OF A
C
                N - NUMBER OF COLUMNS OF A
C
                KEY - AFRAY CONSISTS OF GIVEN KEY INDICES
Ç
                W - WORKING ARRAY OF SAME DIMENSION AS A
C
C
      CUTPUT
C
                CALLING SEQUENCE
                A - THE SORTED ARFAY
C
Ċ
      SUBROUTINES
      CALLED
               NONE
      DISCUSSION THE CONTENTS OF ARRAY A AFE STORED IN A WORKING ARRAY
C
                USING THE INDICES GIVEN IN KEY ARRAY. WORKING APRAY IS
C
                THEN TPANSFERED BACK TO APRAY A.
C
~***
      DIMENSION A(M,1), KEY(1), W(M,1)
      00 10 J=1.N
      K = KEY(J)
      DO 10 T=1.M
   10 W(I,K) = \Delta(I,J)
      DO 20 J=1.N
      DO 20 I=1.M
   20 \Delta(I,J) = W(I,J)
      RETURN
      FND
```

```
SURROUTINE LSQSF
( *****
      SUBROUTINE LSOSE
C.
C
C
                TO FIND THE GENERALIZED INVERSE FROM A LEAST SQUAFES FIT
      PURPCSE
\mathbf{C}
C
      IMPUT
                COMMON BLOCK
C
                /LSQSEC/ - ZK.WTK.NO.NPK
C
C
      OUTPUT
                COMMON BLOCK
C
                /LSQSFC/ - AK
C
      SUBROUTINES
      CALLED
              TRANS, MMULT, PDSFCS
      DISCUSSION THE POUTINE FIRST FORMS THE WEIGHTED NORMAL EQUATIONS.
                IT THEN CALLS ROUTINE USING CHOLESKY SCHEME TO SOLVE THE
                SYSTEM OF EQUATIONS AND FINDS THE GENERALIZED INVERSE. IF
                THE SYSTEM OF EQUATIONS IS NOT POSITIVE DEFINITE. AN EPP-
C
C
                OR MESSAGE WILL BE PRINTED AND EXECUTION OF THE COMPUTER
0
                PROGRAM WILL BE TERMINATED.
( ******
      CEMMCN/L SQSFC/ZK(3,16),WTK(16),AK(6,16),NO,NPK
      DIMENSION V(96), C(961, B(36)
      NJ = 6
      IF((NO.LT.2).OP.(NPK.LT.6)) NI=3
      IF((NO.LT.1).DR.(NPK.LT.3)) NI=1
                               FORMS A RECTANGULAR SYSTEM OF EQUATIONS V
C
                               FROM LEAST SQUARES FIT
\mathbf{C}
      DO 250 K=1, NPK
      L=N[+(K-1)]
      V(1+1)=1.
      IF(NI-LT-2) GD TC 200
      V(L+2)=ZK(1,K)
      V(L+3) = ZK(2,K)
      IF(NI.LT.4) GD TO 200
      V(L+4)=.5*7K(1.K)*7K(1.K)
      V(L+5)=7K(1,K)*2K(2,K)
      V(L+6) = .5 * 7 K(2 . K) * Z K(2 . K)
 200
      CONTINUE
                               MULTIPLIES V RY A DIAGONAL MATEIX WTK
C
Ç.
                              LONSISTS OF GIVEN WEIGHTS
      DD 225 I=1.NI
      L=[+N]*(K-1)
      C(L) = WTK(K)*V(L)
 225
      CONTINUE
 250
      COMT INUE
                               FORMS THE WEIGHTED NORMAL EQUATIONS
C
      CALL TRANS(V, AK, MI, MPK)
      CALL MMULT(C,AK,P,NI,MPK,NI)
                               CALLS POUTINE USING CHOLESKY SCHEME TO
•
                               SOLVE THE NORMAL EQUATIONS AND OBTAINS
C
```

```
C
                              THE GENERALIZED INVERSE
      CALL PDSEQS(B.NI.NI.V.C.NPK.DI)
      IF(D1.NE.O.O) GO TO 350
      PRINT 300
  300 FORMAT(//* NORMAL EQUATIONS APPEARS SINGULAR*)
      PETURN
  350 CONTINUE
                              STORES THE GENERALIZED INVERSE IN APPAY AK
C
      DC 499 K=1.NPK
      00 475 I=1.6
 475
      AK([,K]=0.
      DO 450 T=1.NI
      L=I+NI*(K-1)
      \Delta K(I,K) = C(L)
      CONT INUE
 450
      CONTINUE
 499
      PETURN
      END
```

```
SUBROUTINE PIDENT(P,Q,IDENT)
C *****
\mathbf{C}
      SUBPCUTINE PIDENT (P.Q.IDENT)
C
               TO DETERMINE WHETHER THE POINTS P AND Q ARE TO BE
      PUPPESE
(.
               CONSIDERED NUMERICALLY IDENTICAL
Ç.
Ċ
      INPUT
               CALLING SEQUENCE
C
               P - COORDINATES OF FIRST POINT
               Q - COORDINATES OF SECOND POINT
C
      CUTPUT
               CALLING SEQUENCE
٢
               IDENT - LOGICAL VARIABLE EQUAL TO TRUE IF P AND Q APE
Ċ
                        CONSIDERED IDENTICAL AND FALSE OTHERWISE
      SUBRCUTINES
C
      CALLED
               NONE
      DISCUSSION THE ROUTINE DETERMINES WHETHER THE POINTS P AND Q AFE
C
               CONSIDERED NUMERICALLY IDENTICAL. THE CRITERIA FOR
               IDENTITY IS THAT THE DISTANCE FROM P TO O MUST BE SMALLER
               THAN OR EQUAL TO 1.5-12 TIMES THE SUM OF THE LENGTHS OF
Ċ
C
               P AND Q.
( *****
      LOGICAL IDENT
      DIMENSION P(3),Q(3)
      DATA DELTA /1.E-12/
      SCALF=SQRT(P(1) **2+P(2)**2+P(3)**2)+SQRT(Q(1)**2+Q(2)**2+Q(3)**2)
      IDENT=((P(1)-Q(1))**2+(P(2)-Q(2))**2+(P(3)-Q(3))**2).LF.
     C((SCALE*CELTA)**2)
      RETURN
      END
```

```
SUBFCUTINE PIVC(Z)
( *****
C
      SUBFCUTINE PIVC
C
C
      PURPOSE
                TO OBTAIN DOUBLET PANEL INFLUENCE COEFFICIENTS FOR A GIV-
C
                EN CONTROL POINT
C
•
      INPUT
                CALLING SEQUENCE
C
                Z - X,Y,Z COORDINATES OF A GIVEN CONTROL POINT
                COMMON BLOCK
C
C
                /PANDQ/ - RO.AF.AFT,P,A,B,DIAM,C
                /SYMM/ - NSYMM
C
Ç.
                /ZIP/ - IPZ, IP
C
      OUTPUT
                COMMON BLOCK
C
                /PIVM/ - DVDS
C
C
      SUBPCUTINES
C
               UNIPAN, DIPV, MMULT
      CALLED
      DISCUSSION THE ROUTINE FIRST TRANSFERS SOME OF PANEL INFORMATION
C
                TO BE USED BY THE INTEGRATION ROUTINE. IT THEN CALLS THE
C
                INTEGRATION FOUTINE TO PROVIDE INFLUENCE COEFFICIENTS FOR
C
                A GIVEN CONTROL POINT INDUCED BY DOUBLET DISTRIBUTION OF
                THE SPECIFIED PANEL AND ITS IMAGE (WHEN NSYMM IS SET TO 1
C
                ). THE INFLUENCE COFFFICIENTS ARE MODIFIED TO ACCOUNT FOR
                THE CASE WHEN THE GIVEN CONTROL POINT IS LOCATED ON THE
                INFLUENCING PANEL ITSELF (SEF ENGINEERING DOCUMENT - AFRO
C
                -DYNAMIC INFLUENCE CREFFICIENTSI.
C
( *****
      COMMON/PANDQ/CP(3.4).PC(3).PG(3).AR(3.3).ART(3.3).P(2.4).A.B.DIAM.
     CC(6,6), AST(6,16), IIS(16), INS, ITS, NPDQ
      COMMON /PIVINT/XX(3),PP(8),4A,BR,DDIAM,CC(36),DVDV(3,6),NTST,NCF
      COMMON/PIVM/DVDS(3,6)
      COMMON/SYMM/NSYMM
      COMMON /ZIP/IPZ, IP, ITZ, JCZ
      DIMENSION Z(3), W(3), DVS(3,6), GDVDV(3,6)
                               SETS NUMBER OF TERMS OF LEAST SQUARES FIT
C
                               FOR DOUBLET DISTRIBUTION
C
      NTST = 6
0
                               TRANSFERS SOME OF PANEL INFORMATION TO BE
                              USED BY THE INTEGRATION ROUTINE
      \Delta \Lambda = \Delta
      BB=B
      DDIAM = DIAM
      pn 20 f=1,36
 20
      CC(I)=C(I)
      00 100 I=1.8
      PP(I)=P(I)
 100
                               SETS ARPAYS DVS AND DVDS TO ZERO
      CALL ZERG(DVS, 18)
      CALL ZEFO(DVDS, 18)
```

```
OBTIANS INFLUENCE COEFFICIENTS FOR A
C
                              GIVEN CONTROL POINT INDUCED BY DOUBLET
                              DISTRIBUTION OF THE SPECIFIED PANEL AND
                               ITS IMAGE (WHEN NSYMM=1)
      W(1) = Z(1)
      W(3) = Z(3)
      DO 200 ISYMM=1,2
      SIGN=3-2*ISYMM
      W(?) = SIGN \neq ?(2)
      CALL UNIPAN(AR, RO, W, XX)
      IF(ITS.FQ.2) CALL DPIV
      CALL MMULT(ART, DVDV, GDVDV, 3, 3, 6)
      IF(ISYMM.NE.1.OR.IP.NE.IPZ) GO TO 160
C
                               TO ACCOUNT FOR THE CASE WHEN THE GIVEN
0
                              CONTROL POINT IS LOCATED ON THE INFLUENCE
                               ING PANEL ITSELF
      HALF = -0.5
      HXI = HALF * XY(1)
      HETA = HALF*XX(2)
      DVS(1,2) = HALF
      DVS(1,4) = HXI
      DVS(1.5) = HETA
      DVS(2,3) = HALF
      DVS(2,5) = HXI
      DVS(2.6) = HETA
      CALL MMULT(ART, DVS, DVDS, 3, 3, 6)
  160 CONTINUE
      DO 175 I=1.6
      DVDS(1,I) = DVDS(1,I) + GDVDV(1,I) -
      DVDS(2,1) = DVDS(2,1) + SIGN*GDVDV(2,1)
      DVDS(3,I) = DVDS(3,I) + GDVDV(3,I)
 175 CONTINUE
     IE(NSYMM.EQ.O) GO TO 400
 200
      CONTINUE
 400
      CONTINUE
      PETURN
      END
```

SUBROUTINE SIDECL(W.DSMIN.D) C * * * * * * SUBROUTINE SIDECL (W.DSMIN.D) C C TO COMPUTE GEOMETRIC QUANTITIES ASSOCIATED WITH THE PURPOSE Ċ RELATIONSHIP OF THE FIELD POINT TO THE QUADRILATERAL C SIGMA FOR USE IN COMPUTING THE H INTEGRALS. (SEE FIGURE 30 C AND SECTION P.3 OF APPENDIX B OF THE ENGINEERING C DOCUMENT.) C COMMON BLOCK Ç INPUT Ċ /PIVINT/ - X.P C C QUTPUT CALLING SEQUENCE C W - POINT ON QUADFILATERAL CLOSEST TO PROJECTION OF FIELD C POINT ONTO QUADRILATERAL PLANE C. DSMIN - MINIMUM DISTANCE OF PROJECTION OF FIELD POINT C ONTO QUADRILATERAL PLANE TO PERIMETER OF C QUADRILATERAL C D - DISTANCE FROM W TO PROJECTION OF FIELD POINT ONTO C QUADRILATERAL PLANE C C COMMON BLOCK Ç /SIDEQ/ - QSIDE C /SKATC1/ - AKS1,AFT1,AKS2,AET2,DRM,EL1,EL2,ELM,ANK,ANE, C C C SUBFOUTINES C CALLED TRNSFR C DISCUSSION THE ROUTINE COMPUTES GEOMETRIC QUANTITIES ASSOCIATED C C WITH THE RELATIONSHIP OF THE QUADRILATERAL SIGMA TO THE PROJECTION OF THE FIELD POINT ONTO THE QUADRILATERAL C C PLANE. IN PARTICULAR THE ROUTINE DETERMINES WHETHER THE C PROJECTION LIES INSIDE OR OUTSIDE OF THE QUADRILATERAL AS WELL AS CALCULATES THE MINIMUM DISTANCE FROM THE C C PROJECTION TO THE PERIMETER OF THE QUADRILATERAL. C OTHER QUANTITIES COMPUTED INCLUDE THOSE QUANTITIES C DISPLAYED IN FIGURE 31 AND DISCUSSED IN SECTION C 3.3 OF APPENDIX B OF THE ENGINEERING DOCUMENT. THE C QUANTITIES ASSOCIATED WITH THE QUADRILATERAL IN GENERAL ARE RETURNED VIA THE CALL LIST WHEREAS THE QUANTITIES ASSOCIATED WITH EACH SIDE OF THE QUADPILATERAL ARE C STORED IN A COMMON BLOCK ARRAY A SIDE AT A TIME. C (***** COMMON/PIVINT/X(3),P(2,4),AC,BC,DIAM,C(6,6),DV(3,6),NTST,NCF COMMON/SIDEQ/QSIDE(12,4) COMMON/SKAICI/AKS1,AET1,AKS2,AET2,DPM.FL1,EL2,ELM,ANK,ANE,A,AA,

DIMENSION W(2)

DUANTITIES AND PROCEDURES REFERENCED IN THIS ROUTINE APE DISCUSSED IN APPENDIX B OF THE ENGINEERING DOCUMENT

CGG, S1, S2, S11, S21, HM, HH

Ç.

C

```
D=0.
       NNC T=0
       NPST=0
       ISA=C
          CYCLE THROUGH SIDES OF QUADRILATERAL
       DO 500 IS=1.4
       ISP1=MOD(IS.4)+1
          CALCULATE QUANTITIES DISPLAYED IN FIGURE 31
(
       \Delta KS1=P(1,IS)-X(1)
       \DeltaET1=P(2,IS)-X(2)
       \Delta KS2=P(1,ISP1)-X(1)
       \Delta ET2=P(2,ISP1)-X(2)
       DKS=AKS2-AKS1
       DET=AFT2-AFT1
       DF"=SQRT (DKS*DKS+DET*DET)
C
          IGNORE SIDE IF LENGTH IS ZERO
       IF(DRM.EQ.O.) GO TO 500
       ISA=ISA+1
       DPMI=1./DPM
       A=DPMI*(AKS1*AFT2-AKS2*AET1)
       \Lambda \star \Delta = \Lambda \star \Lambda
       ANK=DPMI *DET
       ANF=-DRMI*DKS
       EL1=DRMI*(AKS1*DKS+AET1*DET)
      EL2=OFMT *(AKS2*DKS+AET2*DET)
          COMPUTE INCREMENT OF INTEGERS WHICH WILL EVENTUALLY
C
C
          DETERMINE WHETHER THE FLELD POINT PROJECTION ONTO THE
C
          QUADRILATERAL PLANE LIES INSIDE OF OUTSIDE THE QUADRILATERAL
       IF(A.GT.O.) NPST=NPST+1
       B=AKS1 #AKS2 +AFT1 #AET2
       IF((A.GT.G.).AND.(B.LT.C.)) NNCT=NNCT+1
          CALCULATE MINIMUM DISTANCE FROM FIELD POINT TO QUADRILATERAL
C
C.
          SIDE
       TF(EL1#EL2) 75,75,85
      FLM=C.
 75
      GO TO 90
 95
      FLM=SIGN(AMINI(ABS(FL1),ABS(EL2)),EL1)
 90
      DIS=FLM#FLM+AA
      IF((ISA.GT.1).AND.(DIS.GT.D)) GO TO 500
      D=D!S
      155=15
          STORE CALCULATED QUANTITIES FOR EACH SIDE
 500
      CALL TENSER (AKS1, OSIDE(1, IS), 12)
      D=SQPT(D)
      DSMIN=D
          BRANCH TO 700 OF 800 DEPENDING UPON WHETHER FIELD POINT
C
          PROJECTION LIES INSIDE OF OUTSIDE QUADRILATERAL
      IF((NPST.E0.4).OR.((NPST.EQ.3).AND.(NMCT.GE.2))) 700,800
 700
      Ŭ=0.°
      W(1)=X(1)
      W(2) = X(2)
      PETURN
C
          RETRIEVE CALCULATED QUANTITIES FOR SIDE CONTAINING POINT
```

C CLOSEST TO FIELD POINT PROJECTION AND CALCULATE C CGORDINATES OF THAT POINT 8CO CALL TRNSFP(QSIDE(1.ISS),AKS1.12) W(1)=X(1)+A*ANK-ELM*ANK W(2)=X(2)+A*ANE+ELM*ANK PETURN END

SUBFICUTINE SING(NT, NM, NN, NS, NSA, NPA, ZM) C SUBROUTINE SING (NT.NM.NN.NS.NSA.NPA.ZM) C C TO CALCULATE THE SINGULARITY DISTRIBUTION DEFINING PHEPISE ŗ QUANTITIES FOR A GIVEN NETWORK C CALLING SEQUENCE INPUT C NT - NETWORK TYPE € NM - NUMBER OF SPANWISE CUTS IN THE NETWORK C NN - NUMBER OF TRANSVERSE CUTS IN THE NETWORK MSA - TOTAL NUMBER OF SINGULARITY PARAMETERS IN ALL PREVIOUS NETWORKS NPA - TOTAL NUMBER OF PANELS IN ALL PREVIOUS METWORKS C ZM - COORDINATES OF COPNER POINTS IN THE NETWORK Ç Ċ COMMON BLOCK C /IPPINT/ - IPSING C /PANDQ/ - FC.4P Ċ C CUTPUT CALLING SEQUENCE C NS - NUMBER OF SINGULARITY PARAMETERS IN THE NETWORK C COMMON BLOCK C /PANDO/ - AST, IIS, INS, ITS C C SUBROUTINES C CALLED GCPCAL, GRDIND, PTRMS, UNIPAN, LSQSF, IPTRMS ٢ C DISCUSSION THE ROUTINE CALCULATES THE DEPENDENCE OF EACH PANEL SINGULARITY STRENGTH DISTRIBUTION ON THE FREE SINGULARITY PARAMETERS OF THE NETWORK. SEPARATE COMPUTATIONS ARE C PERFORMED FOR EACH NETWORK TYPE. FIRST THE LOCATIONS OF C THE FREE SINGULARITY PARAMETERS ON THE NETWORK APE Ċ COMPUTED AND INDEXED. FOR EACH PANEL THE SINGULARITY C PAPAMETERS AFFECTING THE DISTFIBUTION OF SINGULARITY ŗ STRENGTH ON THAT PANEL ARE ISCLATED. EACH SUCH Ċ PARAMETER IS ASSIGNED A WEIGHT (LARGE IF THE PARAMETER (ACTUALLY LIES ON THE PANEL). THE PANEL SINGULAFITY Ċ, DISTRIBUTION IS THEN OBTAINED BY FITTING A QUADEATIC C FORM (IF THE SINGULARITY IS OF DOUBLET TYPE) TO THE -Ċ PARAMETERS BY THE METHOD OF LEAST SQUARES. THE MATRIX C WHICH RELATES THE COEFFICIENTS OF THE DISTRIBUTION TO C THE SINGULARITY PARAMETERS IS THEM STORED ON A PILE ALCHO C WITH INDICES IDENTIFYING THE PARAMETERS. C * * * * * *

COMMON/LSQSFC/ZK(3,16).WTK(16),AK(6,16).NO,NPK
COMMON/PANDQ/CP(3,4),PC(3),FC(3),AF(3,3),ART(3,3),P(2,4),A,8,DIAM,
CC(6,6),AST(6,16),IIS(16),INS,ITS,NPDQ
COMMON /SKPCHI/ZA(3,175),IA(175)
COMMON /IPPINT/IPNPUT,IPGEOM,IPSING,IPCNTR,IPFIVC,IPOUTP
DIMENSION ZM(3,NM,NN)

```
DIMENSION ZPK(3)
      DATA WT /1.E5/
      IF(IPSING.NF.O) PPINT 1001
 1001 FORMAT(1H1)
      NN1 = NN + 1
      NMI = NM + 1
C
          CALCULATE LOCATION OF SINGULARITY PARAMETERS
      CALL GCPCAL(NM, NM, NMI, NNI, 7 M, ZA)
          OPDER NON-IDENTICAL SINGULARITY PARAMETERS
C
      CALL GRDIND(NM1, NN1, 74, TA, MIA)
C
          TRANSFER TO CODE FOR APPROPRIATE METWORK TYPE
      GO TO (100,200,300,400,500,600,600) NT
 100
      CONTINUE
          SCURCE/ANALYSIS NETWORK CALCULATIONS
C
C
          (NOT AN OPTION IN PRESENT PROGRAM)
      DO 199 N=2,NN
      DO 198 M=2.NM
      IP=M-1+(NM-1)*(N-2)+NPA
      CALL PTRNS(IP)
      ITS=1
      MPK=0
      DO 129 J=1,3
      NJ=N+J-2
      IF((NJ.LT.2).DR.(NJ.GT.NN)) GO TO 129
      DO 128 [=1.3
      MI = M + I - 2
      IF((MI-LT-2).OR.(MI.GT-NM)) GO TO 128
      MPK=MPK+1
      IIS(NPK)=MI-1+(NM-1)*(NJ-2)+NSA
      LMN=MI+NMI * (NJ-I)
      nn 125 L=1,3
      ZPK(L)=ZA(L,LMN)
      CONTINUE
      CALL UNIPANIAR, RO, ZPK, ZPK)
      ZK(1,NPK)=7PK(1)
      ZK(2,NPK)=ZPK(2)
      WTK(NPK)=1.
      TF((I.EQ.2).AND.(J.EQ.2)) WTK(NPK)=WT
 128
      CONT INUE
      CONTINUE
 129
      INS=NPK
      NO=1
      CALL LSGSF
      DO 149 K=1, NPK
      DO 148 I=1.3
      \Delta ST(I,K) = \Delta K(I,K)
148
      CONTINUE
      CONTINUE
149
      CALL IPTRNS(IP)
      CONTINUE
198
199
      CONTINUE
      NS=(NM-1)*(NN-1)
```

```
GO TO 800
 200
      CONTINUE
C
          DOUBLET/ANALYSIS (WING) NETWORK CALCULATIONS
C
          CYCLE THROUGH ALL PANELS IN THE NETWORK
      DO 299 N=2.NN
      DO 298 M=2,NM
      IP = M - 1 + (NM + 1) * (N - 2) + NPA
C
          RETRIEVE PANEL GEOMETRY DEFINING QUANTITIES
      CALL PTENS(IP)
      ITS=2
      MPK=C
         CALCULATE LOCATIONS OF SINGULARITY PARAMETERS
C
         AFFECTING PANEL SINGULARITY DISTRIBUTION
      DO 229 J=1.3
      NJ=N+J-2
      DO 228 I=1.3
      MI=M+I-2
      LMN=NI+NNI*(NJ-1)
      MPK=NPK+1
      IIS(NPK)=IA(LMN)+NSA
      CALL UNITPAN(AR .RO .ZA(I.LMN) .ZPK)
      ZK(1,NPK)=ZPK(1)
      ZK(2,NPK)=ZPK(2)
         WEIGHT CONTRIBUTION OF SINGULARITY PARAMETER
C
      WTK(NPK)=1.
      IF(((MI.EQ.1).OR.(MI.EQ.NM1).CR.(I.EQ.2)).AND.
     C((NJ.EQ.1).OR.(NJ.EQ.NN1).OP.(J.EO.2))) WTK(NPK)=WT
 228
      CONTINUE
 229
      CONTINUE
      INS=NPK
      NO=2
C
         LEAST SQUARE PANEL SINGULARITY DISTFIBUTION
         TO SINGULARITY PAPAMETERS
C
      CALL LSGSF
      DO 249 K=1.NPK
      DC 248 T=1.6
      \Delta ST(I.K) = AK(I.K)
 248
      CONTINUE
 249
      CONTINUE
C
         STORE SINGULARITY DEFINING QUANTITIES ON A FILE
      CALL IPTENS(IP)
      IF(IPSING.NE.O)
     $WPITE(6,1000) IP, INS, IIS, NO, AST, ZK
 298
     CONTINUE
      CONTINUE
 299
      MS=NIA
      006 DT 00
C
         SCUPCE/DESIGN NETWORK CALCULATIONS
         (NOT AN OPTION IN PRESENT PROGRAM)
      CONTINUE
 300
      GO TC 800
 400
      CONTINUE
```

```
C
          DCUBLET/DESIGN (FREE SHEET) NETWORK CALCULATIONS
Ç
          OFDER NON-IDENTICAL SINGULARITY PARAMETERS
      CALL GRDIND(NM,NN,ZM,IA,NIA)
          CYCLE THROUGH ALL PANELS IN THE NETWORK
      DO 499 N=2,NN
      DO 498 M=2,NM
       TP=M-1+(NM-1)*(N-2)+NP\Delta
          RETRIEVE PANEL GEOMETRY DEFINING QUANTITIES
\mathcal{C}
      CALL PTPNS(IP)
      ITS=2
      MPK=C
          CALCULATE LOCATIONS OF SINGULARITY PARAMETERS
C
C
          AFFECTING PANEL SINGULARITY DISTRIBUTION
      DO 429 J=1.4
      NJ=N+J-3
      IF((NJ.LT.1).OR.(NJ.GT.NN)) GO TO 429
      DO 428 I=1.4
      MI = M + I - 3
      IF((MI.LT.1).OR.(MI.GT.NM)) GO TO 428
      LMN = MI + NM*(NJ-1)
      MPK=NPK+1
      IIS(MPK)=IA(LMN)+NSA
      CALL UNIPAN(AR, RO, ZM(I, MI, NJ), ZPK)
      ZK(1,NPK)=ZPK(1)
      7K(2,NPK)=ZPK(2)
C
          WEIGHT CONTRIBUTION OF SINGULARITY PARAMETER
      WTK( NPK)=1.
      IF(((I.EQ.2).OP.(I.EQ.3)).AND.((J.EQ.2).OP.(J.EQ.3))) WTK(NPK)=WT
 428 CONTINUE
 429
      CONTINUE
      INS=NPK
      N0=2
C
          LEAST SQUARE PANEL SINGULARITY DISTRIBUTION
C
          TO SINGULARITY PARAMETERS
      CALL LSGSF
      DO 449 K=1,NPK
      DO 448 J=1.6
      \Delta ST(I,K) = \Delta K(I,K)
      CONTINUE
 448
      CONTINUE
 449
          STORE SINGULARITY DEFINING QUANTITIES ON A FILE
C
      CALL IPTRNS(IP)
      IF (IPSING NE.O)
     $WFITE(6,1000) IP, INS, TIS, NO, AST, ZK
 498
      CONTINUE
 499
      CONTINUE
      NS=MTA
      GD TO 800
 500
      CONTINUE
          DOUBLET/DESIGN (WAKE) NETWORK CALCULATTIONS
C
          CYCLE THROUGH ALL PANELS IN THE NETWORK
C
      DO 599 N=2.NN
```

```
DO 598 M=2,NM
       IP = M - 1 + (NM - 1) + (N - 2) + NPA
          RETPIEVE PANEL GEOMETRY DEFINING QUANTITIES
C
      CALL PTRNS(IP)
       IT.S=2
      MPK = C
Ç
          CALCULATE LUCATIONS OF SINGULARITY PAPAMETERS
C
          AFFECTING PANEL SINGULAPITY DISTRIBUTION
      no 529 J=1.3
      NJ=N+J-2
      DO 528 I=1.3
      MI = M + I - 2
      (1-LN) \neq (MN+IM=NM)
      NPK=NPK+1
      TIS(NPK)=IA(MI)+NSA
      CALL UNIPAN (AR, RO, ZA(1, LMN), ZPK)
      ZK(1,NPK)=7FK(1)
      7K(2.NPK)=ZPK(2)
C
          WEIGHT CONTEXBUTION OF SINGULARITY PARAMETER
      WTK(NPK)=1.
      IF(((MI.EQ.1).OR.(MI.EQ.NM1).OR.(I.EQ.2)).AND.
     C((NJ.EQ.1).OR.(NJ.EQ.NN1).OF.(J.EQ.2))) WTK(NPK)=WT
 523
      CONTINUE
 529
      CONTINUE
      INS=NPK
      NO=2
          LEAST SQUARE PANEL SINGULARITY DISTRIBUTION
C
          TO SINGULARITY PARAMETERS
C
      CALL LSGSF
      00 549 K=1,NPK
      DO 548 I=1.6
      \Delta ST(I,K) = \Delta K(I,K)
 548
      CONTINUE
 549
      CONTINUE
C
          STORE SINGULARITY DEFINING QUANTITIES ON A FILE

    GALL IPTENS(IP)

      IF (IPSING.NE.O)
     SWPITE(6,1000) IP, INS, ITS, NO, AST, ZK
 598
     CONTINUE
      CONTINUE
 599
      NS=IA(NM1)
      GO TC 800
 600
      CONTINUE
          DOUBLET/DESIGN (FED SHEET) METWORK CALCULATIONS:
C
C
          CYCLE THROUGH ALL PANELS IN THE NETWORK
      DC 699 N=2,NN
      DO 698 M=2,NM
      IP = M - 1 + (NM - 1) * (N - 2) + NP\Delta
          RETRIEVE PANEL GEOMETRY DEFINING QUANTITIES
C
      CALL PTFNS(IP)
      1 T S = 2
      MPK = C
```

```
C
          CALCULATE LOCATIONS OF SINGULARITY PARAMETERS
C
          AFFECTING PANEL SINGULARITY DISTRIBUTION
      DO 629 J=1.3
      NJ=N+J-2
      DD 628 I=1,3
      MI = M + I - 2
      (1-UM) * IMM+IM=MMJ
      NPK=NPK+1
      IIS(NPK)=NJ+NSA
      IF(NT.EQ.7) IIS(NPK) = 1 + NSA
      CALL UNIPAN (AR, RO, ZA(1, LMN), ZPK)
      ZK(1.NPK)=ZPK(1)
      ZK(2.NPK)=ZPK(2)
          WFIGHT CONTRIBUTION OF SINGULARITY PARAMETER
C
      WIK(NPK)=1.
      IF(((MI.EQ.1).OR.(MI.EQ.NMI).GR.(I.EQ.2)).AND.
     C((NJ.EQ.1).OF.(NJ.EQ.NN1).OF.(J.EQ.2))) WTK(NPK)=WT
 628
      CONTINUE
 629
      CONTINUE
      INS=NPK
      N\Omega = 2
C
          LEAST SQUARE PANEL SINGULARITY DISTRIBUTION
C
          TO SINGULARITY PARAMETERS
      CALL LSQSF
      DO 649 K=1, NPK
      00 648 [=1.6
      \Delta ST(I,K) = \Delta K(I,K)
 648
      CONTINUE
      CONTINUE
 649
\mathbf{C}
          STORE SINGULARITY DEFINING QUANTITIES ON A FILE
      CALL IPTRNS (IP)
      IF(IPSING.NE.O)
     SWRITE(6,1000) IP, INS, IIS, NO, AST, ZK
 1000 FORMAT(//,1915,/(6E15.6)//)
 698
      CONTINUE
 699
      CONTINUE
      NS=MN1
      IF(NT.EQ.7)
                    NS = 1
      CONTINUE
 800
      RETURN
      END
```

```
SUBPCUTINE SURFIT
(, ****<u>*</u>
      SUPPCUTINE SURFIT
C
               TO DEFINE PANEL SURFACE AND LOCAL PANEL COORDINATE SYSTEM
      PUSPOSE
1
      INPUT
               COMMON BLOCK
                /FLATP/ - NFLTP
C
                /LSQSEC/ - ZK,WTK, MO,NPK
               /PANDQ/ - CP
               /IPRINT/ - IPGEOM
C
      CUTPUT
               COMMON BLOCK
               PANDON - PC.PO.AP.P.A.B
      SHAPCUTINES
      CALLED
               CROSS, UVECT, TRANS, UNIPAN, LSQSF, MMULT
                  THE ROUTINE DEFINES A PANEL SUFFACE AND LOCAL PANEL
      DISCUSSION
Ċ
               COORDINATE SYSTEM. AS A FIRST APPROXIMATION TO THE PANEL
               SUPFACE THE FOUTINE TAKES THE QUADRILATERAL FORMED BY
               PROJECTING THE PANEL CORNER POINTS ONTO THE PLANE THEOUGH,
               THE MIDPOINTS OF THE LINE SEGMENTS JOINING THESE CORNER
               POINTS. A LOCAL COOPDINATE SYSTEM IS CONSTRUCTED WITH
               THE ORIGIN AT THE AVERAGE OF THE QUADRILATERAL CORNER
Ċ
               POINTS AND WITH ONE AXIS NORMAL TO THE QUADRILATERAL. TO
               OBTAIN A SECOND ORDER APPROXIMATION TO THE PANEL SURFACE
Ç
               THE POUTINE CALCULATES A PARABOLOID PASSING THROUGH THE
€.
               CORNER POINTS WITH CURVATURE ORTAINED BY LEAST SQUARING
Ç
C
               THE PARABOLOTO TO ADJACENT CORNER POINTS. THE LOCAL
Ç
               COORDINATE SYSTEM IS THEN ROTATED AND TRANSLATED IN SUCH
C
               A MANNER THAT THE PARABOLOID CAN BE SEPRESENTED IN
C
               CANONICAL FORM. AN ITERATIVE PROCESS IS REQUIRED TO
               ELIMINATE LINEAR TERMS WITHOUT TRANSLATING THE ORIGIN.
C *****
      COMMEN/FLATP/NFLTP
      CCMMCN/LSQSFC/ZK(3,16).WTK(16).AK(6,16).NO.NPK
      COMMON/PANDQ/CP(3,4),PC(3),PC(3),AR(3,3),ART(3,3),P(2,4),A,B,DIAM,
     CC(6,6),AST(6,16),ITS(16),IMS,ITS,NPDQ
      COMMON /IPFINT/IPNPUT, IPGEOM, IPSING, IPCNTR, IPEIVC, IPUUTP
      DIMENSION H(3,3), HT(3,3), U(3), V(3), W(3), ZETA(16), COF(6), POP(3)
      DIMENSION WK(3.16)
      FOUTVALENCE \{U(1),HT(1)\},\{V(1),HT(4)\},\{h(1),HT(7)\}
      DATA NIT, DELTA /10,1.E-8/
         CALCULATE BISECTING DIRECTIONS AND CENTER POINT
      DO 50 T=1.3
      U(T) = CP(T,1) + CP(T,4) - CP(T,2) - CP(T,3)
      V(I) = CP(I,1) + CP(I,2) - CP(I,3) + CP(I,4)
      PC(I) = .25 * (CP(I, 1) + CP(I, 2) + CP(I, 3) + CP(I, 4))
      00 49 K=1,NPK
      WK(I.K)=ZK(I.K)
```

49

CONTINUE

```
50
      CONTINUE
0
          CENSTRUCT ORTHOGONAL U.V.W COOFDINATE SYSTEM
          WITH W PERPENDICULAR TO PANEL PLANE
C
      CALL CROSS(U, V, W)
      CALL CROSS(W.U.V)
      CALL UVECT(U)
      CALL UVECT(V)
      CALL UVECT(W)
C
          CALCULATE ORTHOGONAL MATRIX WHICH TRANSFORMS
          COORDINATES FROM GLOBAL TO LOCAL
C
      CALL TRANS(HT, AP, 3,3)
          ITERATE TO FIND PANEL CURVATURES
C
      00 170 JT=1,NIT
      DO 100 K=1.NPK
          TRANSFORM ADJACENT COPNER POINTS TO LOCAL COORDINATES
r
      CALL UNIPAN(AR, PC, WK(1, K), ZK(1, K))
      ZETA(K)=ZK(3.K)
      IF(NFLTP.EQ.1) ZETA(K)=C.
      CONT INUE
 100
      MO= 2
          CONSTRUCT LEAST SQUARES PARABOLOID THROUGH CORNER POINTS
(
      CALL LSQSF
      CALL MMULT(AK.ZETA.COF.6.NPK.1)
      IF (IPGECM.NF.C)
     $WRITE(6,1000) COF
 1000 FORMAT(/ 4X5HCOF , (6F2C.12))
C
          POTATE COORDINATE SYSTEM ABOUT NORMAL TO PANEL
Ç
          TO GET RID OF QUADRATIC CROSS TERM
      COF46=.5*ABS(COF(4)-CCF(6))
      DP=SGFT(COF(5)*+2+COF46**2)
      IF(DP.EQ.(O.)) SPSI=O.
      IF(DP.NE.(O.)) SPSI=SORT(.5*ABS(1.-COF46/DP))
      IF((CDF(5)*(CDF(4)-COF(6))).LT.(O.)) SPSI=-SPSI
      CPSI=SORT(ABS(1.-SPSI**2))
      \Delta PT(1,1) = CPSI
      ART(2,1) = -SPSI
      APT(3,1)=C.
      ART(1,2)=SPSI
      AFT(2,2)=CPSI
      APT[3,2]=C.
      ART(1.3)=0.
      \Delta PT(2.3) = 0.
      \Delta F T (3, 3) = 1.
          CALCULATE PRINCIPAL CURVATURES
      A=.5*(CDF(4)*CPS1**2+CDF(6)*SPS1**2)+CDF(5)*SPS1*CPS1
      E=.5*(COF(4)*SPSI**2+COF(6)*CPSI**2)-COF(5)*SPSI*CPSI
      D=C\cap F(2)*CPSI+C\cap F(3)*SPSI
      IF (ABS(D).LT.DELTA) D=0.
      E=-CCF(2)*SPSI+COF(3)*CPSI
      IF(ABS(E).LT.DELTA) F=0.
      F = COF(1)
          CALCULATE OFIGIN OF NEW LOCAL COOFDINATE SYSTEM
C
```

```
IF(A.EQ.(O.)) ROP(1)=C.
       IF(A.NE.(O.)) ROP(1)=-.5*D/A
       IF(8.EQ.(0.)) ROP(2)=0.
       IF(B.NE.(O.)) ROP(2)=-.5*E/8
      ROP(3) = CGF(1) - A + ROP(1) + + 2 - B + ROP(2) + + 2
       IF(IPGEDM.NE.O)
     $WRITE(6,2000) A.B.D.E.F.POP
 2000 FORMAT((8E15.6))
C
          POTATE COORDINATE SYSTEM ABOUT AXES IN PANEL PLANE
C
          TO TRY TO ELIMINATE LINEAR TERMS
      CA=1./SORT(1.+D*D)
       SA = D * CA
      C8=1./SQRT(1.+E*E)
       SB=E *CB
      HT(1,1)=CA
      HT(1.2)=0.
      HT(1,3) = SA
      HT(2,1) = -SB * SA
      HT(2,2)=CB
      HT(2,3)=SB*CA
      HT(3,1)=-CB*SA
      HT(3.2) = -SB
      HT(3,3)=CB*C4
C
         CALCULATE ORTHOGONAL TRANSFORMATION MATPIX
         FOR NEW LOCAL COORDINATE SYSTEM
      CALL MMULT(ART, AR, H, 3, 3, 3)
      CALL MMULT(HT, H, AR, 3, 3, 3)
      IF((D.EQ.O.).AND.(E.EQ.O.)) GO TO 175
 170
      CONTINUE:
 175
      CONTINUE
      CALL MMULT(POP, AR, W, 1, 3, 3)
C
         CALCULATE ORIGIN OF LOCAL PANEL COORDINATE SYSTEM
      DO 200 I=1.3
 200
      PO(I)=PC(I)+W(I)
Ċ
         CALCULATE LOCAL COORDINATES OF PROJECTIONS OF
¢
         CORNER POINTS ONTO PANEL PLANE
      DO 300 I=1.4
      CALL UNIPAN(AR.RO.CP(1.I).W)
      P(1, I)=W(1)
      P(2, I)=W(2)
 300
      CONTINUE
      RETUPN
      END
```

```
SUBFCUTINE SURPRO(Z,ZP,UN)
(****
C
      SUBROUTINE SURPRO (Z.ZP.UN)
C
C
      PURPOSE
                TO FIND THE LOCATION OF THE PROJECTION OF A POINT ONTO
C
                A PANEL SURFACE AS WELL AS THE SURFACE NORMAL AT THIS
C
                LUCATION.
C
      INPUT
C
                CALLING SEQUENCE
C
                Z - GLOBAL COORDINATES OF POINT TO BE PROJECTED
C
                COMMON BLOCK
C
C
                /PANDQ/ - RO, AR, ART
C.
C
      DUTPUT
                CALLING SEQUENCE
                ZP - GLOBAL COORDINATES OF LOCATION OF PROJECTION
C
                UN - GLOBAL COORDINATES OF UNIT NORMAL TO PANEL SURFACE
(
C
                     AT THIS LOCATION
C
      SUBPRUTINES
      CALLED
C
               UNIPAN, UVECT, PANUNI, MMULT
r
      DISCUSSION
                   THE ROUTINE CALCULATES THE PROJECTION OF A POINT ONTO
                A PANEL SURFACE AS WELL AS THE SURFACE NORMAL VECTOR AT
(
                THE PROJECTED POINT. ALL INPUT AND OUTPUT VECTORS ARE
C
                ASSUMED TO BE GIVEN IN GLOBAL COORDINATES. THE ROUTINE
C
                CONVERTS TO LOCAL COORDINATES, PROJECTS AND CONVERTS
                BACK TO GLOBAL COORDINATES. IN THE EVENT THAT THE GIVEN
C
                POINT DOES NOT LIE ABOVE OR BELOW THE PANEL THE
                PROJECTION IS MADE ONTO THE PARABOLDID OF WHICH THE
C
                PANEL IS A PART.
( ****
      COMMON/PANDQ/CP(3,4),PC(3),PO(3),AR(3,3),ART(3,3),P(2,4),A,B,DIAM,
     CC(6,6), AST(6,16), IIS(16), INS, ITS, NPDQ
      DIMENSION Z(3), ZP(3), UN(3), ZN(3)
C
         TRANSFORM REPRESENTATION OF POINT FROM GLOBAL TO LOCAL
         PANEL COORDINATE SYSTEM
C
      CALL UNIPAN (AR . RO. 7 . ZP)
         CALCULATE VERTICAL COORDINATE OF POINT ON PANEL HAVING SAME
C
         HEPTZONNTAL LOCATION
C
      ZP(3)=A*ZP(1)*ZP(1)+B*ZP(2)*ZP(2)
         CALCULATE SURFACE NORMAL VECTOR AT THIS POINT
ſ.
      ZN(1)=-2.*A*ZP(1)
      7N(2)=-2.*P*ZP(2)
      ZN(3)=1.
         CENVERT NORMAL VECTOR TO UNIT NORMAL VECTOR
C
      CALL UVFCT(ZN)
         CONVERT PROJECTION TO GLOBAL COORDINATES
C
      CALL PANUNI (ART, RO, ZP, ZP)
C
         CONVERT NORMAL VECTOR TO GLOBAL COORDINATES
      CALL MMULT(ART, ZN, UN, 3, 3, 1)
      RETURN
      END
```

```
SUBFRUTINE TONTAL
( ******
r
      SUBROUTINE TONTRL
C
C
      PUSPESE
               TO DESIGNATE THE LOCATION OF CONTEDE POINTS FOR ALL NET-
۲.
               WORK PANELS AND TO COMPUTE THE UNIT NORMAL VECTOR AND THE
               MORMAL COMPONENT OF FREE STREAM VELOCITY VECTOR AT EVERY
               CONTROL POINT
C
      INPUT
               COMMON BLOCK
•
               /INDEX/ - NT.NM.NM.NPA.N7A.NNETT
r,
               /MSPNTS/ - ZM
(
      CUTPUT
               COMMON BLOCK
               /BDYCS/ - ZC,ZCC,ZCF,ZDC,IPC,ITC
C
               /INDEX/ - MCA.NCTPT
(
C
      SUBFCUTINES
C
      CALLED
               CONTPL
Ç
      DISCUSSION THE ROUTINE CALLS CONTRUTO CALCULATE THE LOCATION OF
(
               CONTROL POINTS FOR ALL PANELS AND TO COMPUTE THE UNIT NOS
                -MAL VECTOR AND THE NORMAL COMPONENT OF FREE STREAM VELC-
C
               CITY VECTOR AT EVERY CONTROL POINT ON ALL PANELS FOR EACH
C
               NETWORK. IT ALSO FINDS THE CUMULATIVE NUMBER OF CONTROL
C
               POINTS AND THE TOTAL NUMBER OF CONTROL POINTS.
( ****
      COMMON/BDYCS/ZC(3,125),ZCC(3,125),ZCR(125),ZDC(125),IPC(125),
                    ITC(125)
      COMMON/INDEX/NT(9), NM(9), NM(9), NP(9), NS(9), NC(9), NZ(9),
     CMPA(10).NSA(10).MCA(16).NZA(10).NMETT.NPANT.NSNGT.NCTRT.NZMPT
      COMMON /MSPNTS/ZM(3,175),ZL(75)
      NCA(1)=0
      00 200 K=1, NNETT
      NZMPAL=NZA(K)+1
      NCTRAI=NCA(K)+1
      CALL CONTPL(NT(K),NM(K),NN(K),NC(K),NPA(K),ZM(1,NZMPA1),
     17C(1,NCTRA1),ZCC(1,NCTRA1),ZCR(NCTRA1),ZDC(NCTRA1),IPC(NCTRA1),
     2ITC(NOTPA1))
      MCA(K+1)=MCA(K)+MC(K)
      CONTINUE
200
                              CRIAINS THE TOTAL NUMBER OF CONTROL POINTS
      NCTPT=NCA(NNETT+1)
      FETURN
      FNO
```

```
SUBFOUTINE TGEOMC
(*****
      SUBPOUTINE TGEOMO
\mathbf{c}
C
C
      PURPOSE
                TO GENERATE ESSENTIAL GEOMETRY INFORMATION FOR FACH PANEL
C
                OF ALL THE NETWORKS
(
C
      INPUT
                COMMON BLOCK
Ċ
                /INDEX/ - NT, NM, NN, NPA, NZA, NNETT
                /MSPNTS/ - ZM
C
C.
      CUTPUT
                SEE OUTPUT OF SUBROUTINE GEOMC
C
C.
      SUBFICUTINES
C
      CALLED
                GERMO
(
      DISCUSSION THE ROUTINE CALLS GEOMO TO CALCULATE ESSENTIAL GEOME-
                TRY FOR ALL PANELS OF FACH NETWORK.
C.
C*****
      CEMMEN/INDEX/NT(9);NM(9);NN(9);NF(9);NS(9);NC(9);NZ(9);
     CNPA(10), NSA(10), NCA(10), NZA(10), NNETT, NPANT, NSNGT, NCTPT, NZMPT
      COMMON /MSPNTS/7M(3,175),ZL(75)
      DO 200 K=1.NNETT
      NZMP41=NZA(K)+1
      MPANA1=NPA(K)+1
      CALL GEOMO(NT(K), NM(K), NN(K), NPA(K), ZM(1, NZMPA1))
 200
      CONTINUE
      FETURN
      END
```

```
SUBPCUTINE TSING
( ******
      SUBROUTINE TSING
C
Ĺ
C
      PUPPOSE
               TO DESIGNATE THE LOCATION OF DOUBLETS ON ALL NETWORK
(
               PANELS AND TO COMPUTE THE MATRIX FOR COEFFICIENTS OF QUAD
C
               -PATIC DOUBLETS DISTRIBUTION FOR EACH PANEL
C
ŗ
      IMPUT
               COMMON BLOCK
C
               /INDEX/ - MT.NM.NM.NPA.MZA.NNETT
               /MSPNTS/ - ZM
      CUTPUT
               COMMON BLOCK
C
              /INDEX/ - MS.NSA.NSNGT
C
      SUPPCUTINES
C
      CALLED
               SING
C
C
      DISCUSSION. THE ROUTING CALLS SING TO CALCULATE THE LOCATION OF
               DOUBLETS ON PANELS AND TO COMPUTE THE MATRIX FOR COEFFI-
r
               CLENTS OF QUADRATIC DOUBLET DISTRIBUTION FOR EVERY PANEL
               OF EACH NETWORK. IT ALSO FINDS CUMULATIVE NUMBER OF
               DOUBLETS. FINALLY THE TOTAL NUMBER OF DOUBLETS IS OB-
C
               TAINED.
C.
( *****
      COMMON/INDEX/NT(9).NM(9).NN(9).NS(9).NC(9).NZ(9).
     CNPA(10).NSA(10).NCA(10).NZA(10).NNETT.NPANT.NSNGT.NCTRT.NZMPT
      COMMON /MSPNTS/ZM(3,175),ZL(75)
      MSA (1)=0
      DO 200 K=1.NNETT
      NZMP 41 = NZA(K)+1
      CALL SING(NT(K),NM(K),NN(K),NS(K),NSA(K),NPA(K),ZM(1,NZMPA1))
      MSA(K+1)=NSA(K)+NS(K)
200
      CONTINUE
                              OBTAINS THE TOTAL NUMBER OF DOUBLETS
      MSNGT=NSA(NMETT+1)
      FFTUFN
      FND
```

SUBFOUTINE VINECC(Z.ZN.ZD.JPC) (**** SUBECUTINE VINECO (PURPOSE TO GENERATE THE THREE COMPONENTS OF AERODYNAMIC INFLUENCE COEFFICIENTS FOR A GIVEN CONTROL POINT INDUCED BY ALL PAN -FLS DOUBLET DISTRIBUTION C Ć CALLING SEQUENCE INPUT C Z - X.Y.Z COORDINATES OF A GIVEN CONTROL POINT ZN - NORMAL VECTOR AT THE CONTROL POINT ON PANEL SURFACE ZD - PERTURBATION DISTANCE FOR CONTROL POINT AT EDGES C JPC - INDEX OF PANEL OF WHICH COMPONENTS OF AIC ARE TO BE TRANSFORMED TO ITS LOCAL COORDINATES COMMON BLOCK /CMC3/ - NPIF /INDEX/ - NPANT.NSNGT C Ç CUTPUT COMMON BLOCK \mathbf{C} /PINC/ - DVDES C C SUPFCUTINES (CALLED PTRNS, FIVC, PIVC, MMULT DISCUSSION FOR EVERY PAMEL, THE POUTINE CALLS PTRNS TO TRANSFER (PANEL INFORMATION. DEPENDING ON THE GIVEN CONFOL POINT IS C AT EDGE OF INTERIOR OF THE PANEL, IT CALLS EIVE OF PIVE C TO EVALUATE THE INTEGRALS. THE LATTER IS THEN MULTIPLIED C BY THE GENERALIZED INVERSE FROM LEAST SQUARES FIT OF QUAD Ċ -DRATIC DOUBLET DISTRIBUTION OBTAINED IN SUBROUTINE SING TO FORM THE THREE COMPONENTS OF AERODYNAMIC INFLUENCE COEFFICIENTS. IF JPC IS SPECIFIED, THE COMPONENTS OF AIC. C WILL BE TRANSFORMED TO LOCAL CODRDINATES OF THAT PARTI-CULAR PANEL. C (***** CGMMCN /CMC3/NTSIN.NTSOUT.NTGD.NPIF.NAIC3,NAIC.NJAC.NSCR COMMON/INDEX/NT(9),NM(9),NM(9),NP(9),NS(9),NC(9),NZ(9), CMPA(10).NSA(10).NCA(10).NZA(10).NNETT.NPANT.NSNGT.NCTRT.NZMPT COMMON/PANDQ/CP(3,4),PC(3),PO(3),4P(3,3),ART(3,3),P(2,4),A,B,DIAM, CC(6,6),AST(6,16),IIS(16),INS,ITS,NPDQ COMMON /PIMC/DVDFS(3,125) COMMON /PINDX/KP.KQ.NPWR.NPPD COMMON/PIVM/DVDS(3.6) COMMON /ZIP/IPZ,IP,ITZ,JCZ DIMENSION VF(3). VS(3,16), Z(3), ZN(3) SETS ARRAY DVDFS TO ZERO (CALL ZEPC(DVDFS, 3*MSNGT) OBTAINS THE 3 COMPONENTS OF AERODYNAMIC C INFLUENCE COEFFICIENTS FOR A GIVEN CONTROL C POINT INDUCED BY ALL DOUBLET PANELS OF HALF C THE CONFIGURATION AND THEIR IMAGES

KO = 0

```
REWIND NPIF $ NPFD = NPIF
      DO 700 IP=1, NPANT
      CALL PTFNS(IP)
      IF(ZD.EQ.O) GO TO 600
      CALL EIVC(Z,ZN,ZD,IPINF)
      IF(IPINF) 625,700,625
  600 CALL PIVC(Z)
  625 CALL MMULT(DVDS, AST, VS, 3, 6, INS)
      DO 650 IC=1.INS
      IS=IIS(IC)
      DVDFS(1, IS) = DVDFS(1, IS) + VS(1, IC)
      DVDFS(2, IS) = DVDFS(2, IS) + VS(2, IC)
      DVDFS(3.IS)=DVDFS(3.IS)+VS(3.IC)
 650
      CONTINUE.
 700
      CONTINUE
      IF(JFC.EC.O) GD TO 900
C
                               TRANSFORMS AIC TO LOCAL PANEL (JPC) COORD.
      CALL PTRNS(JPC)
      DO 850 IS=1.NSNGT
      CALL MMULT(AR, DVDFS(1, IS), VR, 3, 3, 1)
      00 900 T=1,3
      OVDES(I.IS)=VR(I)
 800
 850
      CONTINUE
 900
      PETURN
      END
```

```
OVERLAY(VORTEX, 3, 0)
      PROGRAM SOLVER
C *****
      PROGPAM
                SOLVER
C
C
      PUPPESE
                TO SOLVE A LINEAR SYSTEM OF EQUATIONS A#X=8
C
      INPUT
                COMMON BLOCK
C
                INFOS/ - NE, NR, NMAT, NPHS
•
      OUTPUT
                COMMON BLOCK
                INEQS/ - NRHS
      SUBRUTINES
C
      CALLED
               LINEOS
C
C
      DISCUSSION SEE PROGRAM OCCUMENT 1.3 DESCRIPTION AND FLOW CHART OF
                OVEPLAY PROGRAMS.
Ċ
                   THE PROGRAM HAS BEEN SET UP WITH THE CONSIDERATION
                THAT AN OUT-OF-CORE EQUATION SOLVER CAN BE REPLACE THE PF
                SENT IN-CORE ONE WITHOUT CHANGING THE DATA STRUCTURE .
C
C
                SIGNIFICANTLY.
C *****
      COMMON /NEQS/NE, NR. NMAT, NPHS
      DIMENSION A(130,130), B(130), [PR(130)
      NM = 130
C
                              READS OUT COEFFICIENT MATRIX AND RIGHT-
C.
                               HAND SIDE AND STORES THEM IN ARRAYS A $ 8
      PEWIND NMAT
      FEWIND NRHS
      00 10 T=1,NE
      READ (NMAT) (A(I,J),J=1,NE)
   10 READ(MRHS) B(I)
      CALL LINEQS (A.NM. NE. IPR. B. NF. DI)
      IF(D1.NE.C.) GO TO 20
      PPINT 15
   15 FORMAT(///* THE MATRIX APPEARS SINGULAR*)
      STOP
C
                              WRITES SOLUTION VECTOR ON THE FILE
   20 REWIND NRHS
      WPITE(NPHS)
      RETURN
      END
```

```
OVERLAY(VORTEX,4,0)
PROGRAM OUTPUT
```

```
C * * * * * *
C
      PEDGRAM
                OUTPUT
C
C
      PUPPOSE'
                TO CALCULATE AND PRINT THE FOLLOWING RESULTS
C
                PANEL INDICES OF THE WING, FREE AND FED SHEETS AND WAKE
C
                X.Y.Z COORDINATES, PANEL NUMBER AND CIRCULATION AT POINTS
C
                   ALONG THE TERMINATED FOGE OF THE FED SHEET
ŗ
                X,Y,Z COOPDINATES, PANEL NUMBER AND CIRCULATION AT POINTS
                   ALONG THE WING TRAILING EDGE
C
                PANEL NUMBER. X.Y.Z COORDINATES OF PANEL CENTER POINT.
C
                   UPPER AND LOWER VELOCITY, DELTA CP. UPPER AND LOWER
Ç
                   CP. AND PANEL AREA
C
                NORMAL FORCE COEFFICIENT
C
                PITCHING MOMENT COEFFICIENT
Ç
                PITCH AXIS
C
                ROOT CHORD
C
                WING AREA
C
                X.Y.Z COOFDINATES OF PANEL COPNER POINTS IN THE FREE
ņ
                   SHEET NETWORK
ŗ
                X.Y.Z COURDINATES OF PANEL CORNER POINTS IN THE FED
C
                   SHEET NETWORK
C
C
      TYPUT
                COMMON BLOCK
C
                /BDYCS/ - IC
                /CMO3/ - NPIF, NAIC3
Ç
                /FSVEL/ - FSV.XPITCH
                /INCEX/ - NM.NPA.NZA
C
                /MSPNTS/ - ZM
C
                /NEAJ/ - NEQ.NE.NG
C
                /PANDQ/ - AR, ART, C
C
                /PINC/ - DVDFS
C
                /SOLN/ - S
C
C
      CUTPUT
                SEE PURPOSE
C.
C
      SUBFCUTINES
C
               MMULT.PTRNS, SNGCAL, UVECT, VIP
      CALLED
C
C
      DISCUSSION SEE PROGRAM DOCUMENT 1.3 DESCRIPTION AND FLOW CHAST OF
               OVERLAY PROGRAMS.
C *** ***
              /CMG3/NTSIN,NTSOUT,NTGD,NPIF,NAIC3,NAIC,NJAC,NSCF
      COMMON
      COMMON/BDYCS/ZC(3,125),ZCC(3,125),ZCR(125),ZDC(125),IPC(125),
                    ITC(125)
      COMMON/INDEX/NI(9).NM(9).NN(9).NP(9).NS(9).NC(9).NZ(9).
     CNPA(10),NSA(10),NCA(10),NZA(10),NNETT,NPANT,NSNGT,NCTRT,NZMPT
      COMMON/MSPNTS/ZM(3,175),7L(75)
      COMMON/PANDQ/CP(3,4),PC(3),FC(3),AR(3,3),ART(3,3),P(2,4),A,B,DIAM.
     CC(6,6), AST(6,16), IIS(16), INS, ITS, NPDQ
```

COMMON /PINC/DVDFS(3,125)

```
COMMON /PINCX/KP, KQ, NPWF, NPPO
      COMMON/FSVEL/FSV(3), FSVM, ALPHA, XPITCH, RCHORD
      COMMON /NEAJ/NEQ,NE,NG
      COMMON /NITE/NEUN.JT.ITMX.KIT.ITPFIN
      SOMMON / SOUN/S(125), ZA(75)
      COMMON /IPRINT/IPNPUT.IPGEOM, IPSING, IPCNTE.IPEIVC.IPOUTP
      DIMENSION VEL(3), VELFS(3), 7(3), TSC(6), VU(3), VL(3)
      IF(IPOUTP.EQ.O.OR.NFUN.NE.100) GO TO 50
      PRINT 2010, NNETT, NPANT, NSNGT, NCTRT, NZMPT
 2010 FORMAT(#1FROM OUTPUT#/515)
      PRINT 2020, (S(I), I=1, NSNGT)
 2020 FORMAT(//# SOLUTION S#/(5E14.6))
   50 CONTINUE
C
                               PRINTS PANEL NO. FOR DIFFERENT NETWORKS
                         I2 = NPA(2)
      T3 = NPA(2)+1
                      $,
                         I4 = NPA(3)
                         I6 = NPA(4)
      15 = NPA(3)+1
                      $
                         18 = NPA(6)
      I7 = NP\Delta(4) + I
                     .$
      WRITE(NTSOUT,5010) I1,12,13,14,15,16,17,18
 5010 FDEMAT( ///48x,*WING PANEL NUMBER*,8x,14,* TD*,14/
                  48X, *FREE SHEET PANEL NUMBER*, 2X, 14, * TO*, 14/
     1
                  48X, *FED SHEET PANEL NUMBER*, 3X, 14, * TO*, 14/
     2
                  48X,*WAKE PANEL NUMBER*,8X,14,* TO*,14)
Ċ
                               PRINTS CIRCULATION ALONG TERMINATED FOGE
                               OF FED SHEET
      WRITE(NTSOUT, 5020)
 5020 FORMAT(///43X,*CIRCULATION ALONG TERMINATED EDGE OF FED SHEET#//
     142X,*X*,10X,*Y*,10X,*7*,10X,*PANEL*,6X,*CIFCULATION*/)
      KQ = Q
      REWIND NPIF $ NPRD = NPIF
      M3 = NM(3)
      1.1 = N7A(3) + M3
      DO 200 IP=15,16
      L2 = L1 + M3
      CALL PTFNS(IP)
      DO 100 L=1.3
      Z(L) = 0.5*(ZM(L,L1) + ZM(L,L2))
  100 CONTINUE
      CALL SNGCAL (Z. TSC)
      WPITE(NTSOUT, 5030) (Z(L), L=1,3), IP, TSC(1)
 5030 FOF MAT (34X, 3F11.4, 8X, I4, 4X, F11.4)
      11 = 12
  200 CONTINUE
C
C
                               PRINTS CIPCULATION ALONG WING TRAILING EDGE
      WPITE(NTSOUT, 5040)
 5040 FORMAT(//48×+*CIRCULATION ALONG WING TRAILING EDGE*//
     142x, *x*, 10x, *Y*, 10x, *Z*, 10x, *PANEL*, 6x, *CIFCULATION*/)
      INP = NPA(5) - (NM(2)-1)
      L1 = N7A(4) + 1
```

```
DU 400 IP=17, INP
      1.2 = 1.1 + 1
      CALL PTRNS(IP)
      00 300 L=1.3
      Z(L) = 0.5*(7M(L,L1) + ZM(L,L2))
  300 CONTINUE
      CALL SNGCAL(Z, TSC)
      WPITE(NTSGUT,5030)
                          (7(L), L=1,3), IP, TSC(1)
      L1 = L2
  400 CONTINUE
<u>ှ</u>
                              PRINTS V(UPPER), V(LOWER), CP(UPPER),
                              CP(LOWER), DELTA CP, ETC. FVALUATED AT THE
Ç
                              CONTROL POINTS CORPESPONDING TO CENTRAL
                              LOCATION OF PAMELS
      WRITE(NTSOUT, 5050)
 5050 FOPMAT(///4X,*PANEL*,5X,*ZCX*,6X,*ZCY*,6X,*ZCZ*,6X,*VUX*,6X,*VUY*,
     16×,÷VUZ÷,6×,÷VL×÷,6×,*VLY*,6×,*VLZ*,6×,*DCP÷,6×,*CPU*,6×,*CPL*,6×,
     2*APE 4*/)
      REWIND NAIC3
      KQ = 0
      PEWIND MPIF $ MPFD = MPIF
      NFW = NF - NG
      00 500 I=1.NEQ
      READ(NAIC3) DVDFS(1)
  500 CONTINUE
      SW = 0.
      CN = C.
      CM = 0.
      DO 900 [J=1,NF
      READ(NATC3) DVDFS
      IP = IJ $ JC = NEQ + IJ
      CALL PTRNS(IP)
C
                          CALCULATES V(TOTAL) AND GRAD(MU)
      CALL MMULT(DVDFS,S,VEL,3,MSNGT,1)
      DO 600 I=1.3
  600 VEL(I) = VEL(I) + FSV(I)
      CALL SNGCAL(ZC(1,JC),TSC)
      7(1)=TSC(2) $ 7(2) = TSC(3) $ 7(3) = 0.
      CALL MMULT(ART, Z, VELFS, 3, 3, 1)
\mathbf{C}
                              CALCULATES V(UPPER) AND V(LOWER)
      DO 700 I=1.3
      VU(I) = VEL(I) + 0.5*VELFS(I)
      VL(I) \approx VEL(I) - 0.5 * VELFS(I)
  700 CONTINUE
C
                          CALCULATES DELTA CP
      CALL VIP(VEL,1,VELFS,1,3,HDCP)
      DCP = 2.*HDCP
      IF(IJ.GT.NEW)
                     GO TO 800
                              CALCULATES CP(UPPER) AND CP(LOWEP) FOR WING
C
      CALL VIP(VEL,1,VEL,1,3,VSG)
      CALL VIP(VELFS, 1, VELFS, 1, 3, GMUSQ)
```

```
CPU = 1. - (VSQ + HDCP + 0.25*GMUSQ)
     CPL = 1. - (VSQ - HDCP + 0.25 *GMUSQ)
C
                            CALCULATES WING AREA, NORMAL FORCE COEFF.,
C.
                            PITCHING MOMENT COEFF.
     SP = C(1.1)
     SW = SW + SP
     CNF = \Delta F(3,3) * DCP * SP
     CN = CN + CNF
     CM = CM + CNF*(ZC(1,JC) - XPTTCH)
     5060 FORMAT(3X,14,2X,13F9.4)
      GO TC 900
  5070 FORMAT(3X,14,2X,10F9.4)
  900 CONTINUE
                            CALCULATES NORMAL FORCE COEFF.,
C
C
                            PITCHING MOMENT COEFF.
      SW = 2.*SW
     CN = 2.*CN/SW
     CM = 2.*CM/(RCHOPD*SW)
      WRITE(NTSOUT, 5080) CN, CM, XPITCH, FCHORD, SW
 5080 FORMAT(///47X.*NORMAL FORCE COEFFICIENT =*.3X.F9.4/
               47X, *PITCHING MOMENT COEFFICIENT =*, 59.4/
     1
               47X, *PITCH AXIS = *, 17X, F9.4/
     2
     3
               47X, *POOT CHORD = *,17X, E9.4/
               47X, #WING APFA =#, 18X, F9.41
C
C
                            PRINTS COPNER POINTS OF FREE SHEET NETWORK
C .
                            AND FED SHEET NETWORK
     WRITE(NTSOUT.5090)
 5090 FORMAT(///49X.*X Y Z COORDINATES OF CORNER POINTS*)
      J1 = NZA(2)+1    J2 = NZA(3)
     WRITE(NTSOUT,5100) (ZM(1,J),ZM(2,J),ZM(3,J),J=J1,J2)
 5100 FORMAT(/57X, *FREE SHEET NETWORK*//(15F8.3))
      J1 = NZA(3)+1 \qquad 5 \qquad J2 = NZA(4)
     WPITE(NTSOUT,5110) (ZM(1,J),ZM(2,J),ZM(3,J),J=J1,J2)
 5110 FORMAT(/57X,*FED SHEFT NETWORK*//(15F8.3))
     PETURN.
     END
```

```
SUBROUTINE SINFOC(Z)
C****
C
      SUBFOUTINE SINFOC (Z)
r
                GIVEN THE X.Y.Z COCRDINATES OF A POINT SINFOC DEFINES A
C
      PUPPOSE
                MATRIX (DSDES). WHICH WHEN MULTIPLIED BY A VECTOR CON-
Ç
C
                SISTING OF VALUES OF ALL DOUBLET PARAMETERS, GIVES THE
C
                VALUE AND 1ST, 2ND DERIVATIVES OF DOUBLET STRENGTH AT THE
                GIVEN POINT
C
      IMPUT
                CALLING SEQUENCE
€.
                Z - X,Y,Z COMPDINATES OF THE GIVEN POINT
C
                COMMON BLOCK
C.
                /INDEX/ - NSNGT
                /PANDQ/ - RO.AF.AST.IIS.INS
C
C
      CUTPUT
                COMMON BLOCK
C
                /SNGC/ - DSDES
Ç
ŗ
      SUBPCUTINES -
C
                UNIPAN
      CALLED
~
      DISCUSSION SUBPOUTINE UNIPAN CONVERTS THE INPUT POINT FROM THE
C
                UNIVERSAL TO LOCAL PANEL COOPDINATE SYSTEM.
                   A SIX BY SIX MATRIX IS FORMED BY THE GENERAL EQUATION
C
                REPRESENTING THE DOUBLET STRENGTH DISTRIBUTION AT THE GIV
                -EN POINT ON A PAMEL AND ITS DERIVATIVES.
C
                   A SIX BY SIXTEEN MATRIX (AST) FOR CHEFFICIENTS OF QUAD
C
C
                -FATIC DOUBLET DISTRIBUTION ON THE PANEL ALSO EXISTS. THE
                MATRIX IS COMPUTED IN SUBROUTINE SING.
(
                   THE MATRIX DSDES IS FORMED BY MULTIPLYING THESE TWO
C
                MATRICES.
C
( ****
      COMMON/INDEX/NT(9).NM(9).NN(9).NP(9).NS(9).NC(9).NZ(9).
     CNPA(10), NSA(10), NCA(10), NZA(10), NNETT, NPANT, NSNGT, NCTRT, NZMPT
      COMMCN/PANDQ/CP(3.4),PC(3),FO(3),AR(3.3),ART(3.3),P(2.4),A.B.DIAM,
     CC(6,6),AST(6,16),IIS(16),IMS,ITS,NPDQ
      COMMON /SNGC/ DSDFS(6,125)
      DIMENSION Z(3), W(3)
      EQUIVALENCE (X,W(1)), (Y,W(2))
C
                              TRANSFORMS THE INPUT POINT FROM GLOBAL TO
                              LOCAL PANEL COORDINATE SYSTEM
C
      CALL UNIPAN(AP, RO, Z, W)
                              SETS APRAY DSDES TO ZERO ...
C
      CALL ZEFO(DSDFS,6*MSNGT)
C
                              MULTIPLIES TWO MATRICES TO FORM THE MATRIX
C
                              DSDES
      DO 200 IC=1.IMS
      1S=11S(1C)
      DX = AST(4,IC) + X + AST(5,IC) + Y
      DY = AST(5,IC) \neq X + AST(6,IC) \neq Y
```

DSDFS(1.IS)=DSDFS(1.IS)+AST(1.IC)+(AST(2.IC)+.5*DX)*X

```
C+(AST(3,IC)+.5*DY)*Y
DSDFS(2,IS)=DSDFS(2,IS)+AST(2,IC)+DX
DSDFS(3,IS)=DSDFS(3,IS)+AST(3,IC)+DY
DSDFS(4,IS)=DSDFS(4,IS)+AST(4,IC)
DSDFS(5,IS)=DSDFS(5,IS)+AST(5,IC)
DSDFS(6,IS)=DSDFS(6,IS)+AST(6,IC)
CONTINUE
RETURN
END
```

```
SUBROUTINE SNGCAL(Z, TSC)
C *****
C
      SUBROUTINE SNGCAL (Z, TSC)
C
C
               TO CALCULATE THE VALUE AND 1ST, 2ND DEFIVATIVES OF DOUB-
      PURPOSE
C
               LET STRENGTH AT THE SPECIFIED POINT
C
      IMPUT
               CALLING SEQUENCE
                Z - X,Y,Z COOFDINATES OF THE GIVEN POINT
C
C
               COMMON BLOCK
                150LN/ - S
Ç
C
               CALLING SEQUENCE
      OUTPUT
Ç
               TSC - ARRAY CONSISTS OF THE VALUE AND IST, 2ND DERIVATIVES
C
                     OF DOUBLET STRENGTH
C
Ç.
      SUPPOUTINES
r,
      CALLED
               SINFCC, MMULT
C
      DISCUSSION SNGCAL CALLS SUBPOUTINE SINFCC TO PRODUCE THE MATRIX
C
Ç
               DSDES. MMULT MULTIPLIES THIS MATERX BY THE VECTOR CONSIST
C
               TINT OF VALUES OF ALL DOUBLET PARAMETERS PREVIOUSLY OB-
C
               TAINED TO PRODUCE THE VALUE AND 1ST, 2ND DERIVATIVES OF
               DOUBLET STRENGTH AT THE GIVEN POINT
C
C *****
      COMMON/INDEX/NT(9),NM(9),NN(9),NP(9),NS(9),NC(9),NZ(9),
     CNP4(10),NS4(10),NCA(10),NZ4(10),NNETT,NP4NT,NSNGT,NCTRT,NZMPT
      COMMON /SNGC/DSDFS(6,125)
      COMMON /SOLN/S(125),Z4(75)
      DIMENSION Z(3), TSC(6)
      CALL SINFCC(Z)
      CALL MMULT(DSDFS.S.TSC.6.NSNGT.1)
      RETURN
```

FND

```
SURPCUTINE BSUBSM(A, NP, N, IPR, B, M)
C ****
C
      SUBPCUTINE ESUSSM (A.NR.N.IPF.B.M)
C
C
               TO PERFORM BACK SUBSTITUTIONS USING THE FACTORIZATION OB-
      PUPPCSE
Ċ
               TAINED FROM A DECOMPOSITION ROUTINE AND FIND THE SOLUTION
C
                FOR A SYSTEM OF EQUATIONS
C
C
                CALLING SEQUENCE
      INPUT
C
                A - THE LOWER TRIANGLE OF THE ARRAY CONSISTS OF A LOWER
C
                    TRIANGULAR MATRIX L AND THE UPPER TRIANGLE CONSISTS
                    DE AN UPPER TETANGULAR MATRIX U. THEY ARE OBTAINED
C
C
                    FROM A DECOMPOSITION ROUTINE SUCH AS TOESOM
C
               NR - MAXIMUM FOW DIMENSION OF APRAYS A AND B
C
                N - ORDER OF THE COEFFICIENT MATRIX
                IPR - APRAY CONSISTS OF NUMBERS OF PIVOTAL ROW, AS DERIV-
C
C
                      ED FROM THE SUBROUTINE T-DECOM
                B - ARRAY CONSISTS OF M FIGHT-HAND SIDES OF THE LINEAR
C
C
                    SYSTEM
                M - NUMBER OF RIGHT-HAND SIDES
Ü
C
      GUTPUT
               CALLING SEQUENCE
Ç
                B - SOLUTION VECTORS
C
      SUBROUTINES
C
ŗ
      CALLED
               VIPS
C
C
      DISCUSSION THE ROUTINE FIRST USES PIVOTAL INFORMATION GIVEN IN
C
                THE ARRAY IPR TO EXCHANGE ELEMENTS OF RIGHT-HAND SIDES.
                IT THEN PERFORMS FORWARD SUBSTITUTION BY SOLVING THE LOW-
C
                ER TRIANGULAR SYSTEM OF EQUATIONS LY=8 AND BACKWARD SUB-
C
                STITUTION BY SOLVING THE UPPER TRIANGULAR SYSTEM OF EQUA-
C
                TIONS UX=Y. X IS THE DESIRED SOLUTION OF THE GIVEN SYSTEM
C
C
                OF EQUATIONS.
                   THE SOUTINE IS A MODIFIED VERSION OF A ROUTINE IN THE
C
                SUBROUTINE LIBRARY OF THE BOEING COMPUTER SERVICES CO.
C
( *****
      DIMENSION A(NR.1), IPR(1), B(NR.1)
                              USES PIVOTAL INFORMATION TO EXCHANGE
C
                              ELEMENTS OF RIGHT-HAND SIDES
C
      PO 10 [=1,N
      IF(IPR(I).EQ.I)
                        GO TO 10
      00 5 K=1,M
      X=B(I,K)
      J = IPF(I)
      B(I,K)=B(J,K)
    5 B(J.K)=X
   10 CONTINUE
                              PERFORMS FORWARD SUBSTITUTION
C
      NM1 = N - 1
      DO 50 K=1,M
      B(1,K) = B(1,K)/4(1,1)
```

```
IF(N.EQ.1) GD TO 30
      DO 20 I=2.N
      X=8(I,K)
      CALL VIPS(A(I,1), NF, B(1, K), 1, I-1, X)
   20 F(I,K) = X/A(I,I)
C
                               PERFORMS BACKWARD SUBSTITUTION
   30.8(N,K) = 8(N,K)
      TF(N.EQ.1) GO TO 50
      DG 40 IN=1, NM1
      I = N - IN
      X = P(I,K)
      [1 = 7+1]
      CALL VIPS(A(I+II) + NR + B(II+K) + I+ IN+X)
      9(T,K) = X
   40 CONTINUE
   50 CONTINUE
      PETURN
      EMD
```

THE FOLLOWING CODE IS EXECUTED IFF NOB IS DDD

SAVE ADDRESS OF F IN XO

SXO

83

```
LOOPBACK IS FOR EACH ROW IN A
FL
         MX6
                 0
                                   ZERO TO X6 AS ACCUMULATOR
         SAI
                 81
                                   FIRST ELEMENT OF ROW OF A TO X1
                                   FIRST ELEMENT OF COLUMN OF B TO XI
          542
                 82
         LOOPBACK IS FOR THE INNER PRODUCT (NOA TIMES)
                                   MULTIPLY FLEMENT A * ELEMENT B
T L
         FX5
                 X1 ± X2
         SRI
                                   PUMP ADDRESS IN 4 UP AS LOOP COUNTER
                 81+1
          542
                 42+B5
                                   LOAD NEXT ELEMENT COLUMN OF B
                                   LOAD NEXT ELEMENT ROW OF 5
         SAL
                 9.1
                                   ADD ON CURRENT CONT. TO INNER PRODUCT
         FX6
                 X5+X6
                                   DONE IF 91 IS POINTS TO NEXT ROW OF A
         LT
                 B1.34.IL
         NX6
                 X6
                                   STORE ELEMENT IN THE R MATRIX
         SA6
                 8.3
                                   BUMP INNER LOOP DONE COUNTER BY NCA
         584
                 84+85
         583
                                   BUMP P STORE BY NCB
                 83+86
         LE
                 84,87.FL
                                   TEST FOR ALL ROWS FIRST COLOF R DONE
                                   RESTORE ADDRESS OF A
         $81
                 40
                                   RESTORE R ADD. TO SECOND ELEMENT OF P
          SP3
                 X0 + 1
         SB2
                                   FESTORE B ADD. TO SECOND ELEMENT OF B
                 32+1
                                   RESTORE B4 TO LWA+1 FIRST FOW OF A
                 81+85
         SB4
                                   TEST FOR DONE AT THIS POINT
         SX1
                 86-1
                 X1,CMAB
         7 F
                                   DONE IF ONLY ONE COLUMN IN B
         PPIMARY PORTION OF CODE TO PROCESS MULTIPLY
         LOOPBACK IS FOR A PAIR OF COLUMNS IN P
                                   LOAD FIRST ELEMENT OF A FOR INNER LOOP
CLOOP
         SAI
                 81
         SXO
                 83
                                   SAVE ADDRESS OF & MATRIX COL IN XO
         LCOPBACK IS FOR ROWS OF A
                                   ZEFO TO X6 FOR ODD ACCUMULATOR
FLOOP
         MX 6
                 0
         SAZ
                 B2
                                   LOAD FIRST
                                               ELEMENT ODD COLUMN OF 8
                                   LOAD FIRST
                                               ELEMENT EVEN COLUMN OF B
         SA3
                 R2+1
         MX7
                                   ZERO TO X7 AS EVEN ACCUMULATOR
         LOOPBACK IS FOR INNER PRODUCT (NCA TIMES)
ILOOP
                                   START ODD MULTIPLY GOING
         FX4
                 X1*X2
                                   BUMP BL AS LOCP COUNTER
         SBI
                 81+1
                                   STAFT EVEN MULTIPLY GDING
         FX5
                 X1*X3
                                   LOAD NEXT ELEMENT OOD COLUMN OF B
         SA2
                 A2+36
         SAL
                 81
                                   LOAD NEXT ELEMENT ROW OF A
                                   ADD ON INNER PROD. ODD COL
         FX6
                 X6+X4
                                   LOAD MEXT ELEMENT EVEN COLUMN OF B
         SA3
                 42+1
```

ADD ON LINNER PROD. EVEN COL

FX7

X7+X5

T T NX6	81,84,ILOOP X6	DONE IF B1 POINTS TO NEXT POW OF A
584	84+85	ADVANCE 84 TO NEXT ROW OF A
546	93	STOPE ELEMENT R IN ODD COL
NX7	× 7	
\$83	B3+B6	BUMP THE F STOPE BY NCB
547	Δ6+1	STORE ELEMENT R IN EVEN COL
Į, T	81,97,8LOOP	DONE IF BI IS PAST THE A MATRIX
583	X0+2	ADVANCE INITIAL VALUE OF B3 BY TWO
\$81	40	RESTORE B1 TO FIRST ELEMENT OF A
542	B2+2	ADVANCE COL E POINTER BY TWO
594	91+B5	RESTORE B4 TO SECOND ROW OF A
SX2	44-83	LWA+1 OF F - NEXT COL OF F ADDRESS
NZ	X2,CLOOP	DONE IF NEXT COL OF R IS SECOND POW
FΩ	CMAB	GET OUT
EMD		

```
SUBROUTINE CROSS(A.B.C)
C****
Ç
       SUBFCUTINE CROSS (A,B,C)
ŗ
C
       PURPOSE
                 TO CALCULATE THE CROSS PRODUCT OF TWO VECTORS
C
C
       INPUT
                 CALLING SEQUENCE
C
                 A - FIRST VECTOR
                 B - SECOND VECTOR
C
      OUTPUT
                 CALLING SEQUENCE
C
                 C - PESULTANT VECTOR
Ç
C
       SUPFCUTINES
C
      CALLED
                 NONE
C
C
      DISCUSSION CROSS PERFORMS THE FOLLOWING CALCULATIONS-
\mathbf{C}
                          C(1) = (A(2) *B(3)) - (A(3) *B(2))
C
                          C(2) = (\Delta(3)*B(1)) - (\Delta(1)*B(3))
                          C(3) = (A(1)*B(2)) - (A(2)*B(1))
C *****
      DIMENSION A(3), B(3), C(3)
      C(1)=A(2)*B(3)-A(3)*B(2)
      C(2) = A(3) * B(1) - A(1) * B(3)
      C(2) = A(1) * B(2) - A(2) * B(1)
      RETURN
      END
```

```
SUBFICUTINE IPTENS (IP)
C * * * * * * *
      SUBROUTINE IPTPNS (IP)
Ç
C
      PURPOSE
               TO WRITE PANEL INFORMATION ON DISK
C
C
      INPUT
                CALLING SEQUENCE
                IP - PANEL NUMBER OF INFORMATION TO BE WRITTEN
C
C
                COMMON BLOCK
                /PANDQ/ - CP,PC,RO,AP,ART,P,A,B,DIAM,C,AST,IIS,INS,ITS
Ç
Ç
                /PINDX/ - KP.NPWR
C
      OUTPUT
                COMMON BLOCK
C
                /PINDX/ - KP
      SUBROUTINES
C
      CALLED.
                NONE
      DISCUSSION WRITES 197 WORDS OF PANEL INFORMATION FROM COMMON
C
                BLOCK PANDO ONTO DISK FILE SPECIFIED BY NPWR
( * * * * * * *
      COMMON /PANEO/ PDQ(197), NPDQ
      COMMON /PINDX/ KP-KDUM-NPAN-NDUM
C
      ID = IP - KP
      TF (ID) 200,300,100
 100
      IBFANCH = ID
      GO TO 250
 200
      IBFANCH = IP
      PEWIND NPAN
      IF (IBRANCH .EQ. 1) GO TO 290
 250
      MAX = TEFANCH - 1
      DO 275 I=1, MAX
 275
      WRITE(NPAN)
                     PDQ(1)
      WRITE (NPAN)
                     PDQ
 290
 300
      KP = IP
      RETUPN
      END
```

```
SUBPOUTINE LINEQS(A,NF,N,IPR,B,M,D1)
C ******
C
      SUPROUTINE LINEOS (A.MR.N. TPR.B.M.D1)
C
C
      PUFPCSE
                TO SOLVE A SYSTEM OF LINEAR EQUATIONS A*X = 8
C
C
      INPUT
                CALLING SEQUENCE
ŋ
                A - ARRAY CONSISTS OF ELEMENTS OF THE COEFFICIENT MATRIX
                NR - MAXIMUM ROW DIMENSION OF APRAYS A AND B
                N - ORDER OF THE COEFFICIENT MATRIX
                B - ARRAY CONSISTS OF M RIGHT-HAND SIDES OF THE LINEAR
                    SYSTEM
Ć
                M - NUMBER OF RIGHT-HAND SIDES
                CALLING SEQUENCE
C
      OUTPUT
                A - THE LOWER TRIANGLE OF THE AFRAY CONSISTS OF A LOWER
                    TRIANGULAR MATRIX L AND THE UPPER TRIANGLE CONSISTS
C
                    OF AN UPPER TRIANGULAR MATRIX U (SINCE U IS UNIT UP-
C
                    PEP TRIANGULAR, ITS DIAGONAL ELEMENTS ARE NOT STORED)
                IPR - APRAY GIVES NUMBERS OF PIVOTAL POW (A RECORD OF IN-
C
C
                      TERCHANGES)
C
                B - SOLUTION VECTORS
C
                DI - = +1 OR -1 ACCORDING AS THE NUMBER OF INTERCHANGES
Ċ,
                     IS EVEN OR ODD. IT ALSO INDICATES SUCCESSFUL FETURA
                     = O INDICATES THAT THE COEFFICIENT MATRIX APPEARS
C
C
                     SINGULAR
C
      SUPRCUTINES
C
      CALLED
               TDECOM, BSUBSM
C
      DISCUSSION FOUTINE TOECOM IS FIRST CALLED BY LINEQS TO PERFORM
C
C
               THE DECOMPOSITION OF THE COEFFICIENT MATRIX A INTO A LOW-
C
                EF TRIANGULAR MATRIX L AND AN UPREF TRIANGULAR MATRIX U.
                THE RESULT IS THEN USED IN BSUBSM FOR CARRYING OUT BACK
                SUBSTITUTIONS AND COTAINING THE SOLUTION TO THE SYSTEM OF
C
C.
                EQUATIONS.
C
                   THIS POUTINE IS A MODIFIED VERSION OF A ROUTINE IN THE
Ċ
                SUBROUTINE LIBRARY OF THE BOEING COMPUTER, SERVICES CO.
( *****
      DIMENSION A(NR.1), IPR(1), B(NP.1)
                              CALLS POUTINE TO DECOMPOSE THE GIVEN
C
                              COEFFICIENT MATEIX
C
      CALL TDECOM(A,NF,N,IPF,IPR,D1)
      IF(D1.EQ.O.) GO TO 10
                              CALLS ROUTINE TO PERFORM BACK SUBSTITUTIONS
C
C
                              AND OBTAIN THE SOLUTION FOR THE SYSTEM OF
                              FQUATIONS
      CALL BSUBSM(A, NR, N, IPR, B, M)
   10 RETURN -
      END
```

```
SUPPOUTINE MMULT(A,8,C,L,M,N)
      SUPPOUTINE MMULT (A.B.C.L.M.N)
€
r
C
      PURPOSE
                TO MULTIPLY TWO MATRICES
Ċ
C
      INPUT
               CALLING SEQUENCE
C
                A - ARPAY CONTAINING ELEMENTS OF MATRIX A
C
                B - ARRAY CONTAINING ELEMENTS OF MATRIX 3
Ċ,
                L - NUMBER OF POWS IN A AND C
C
                M - NUMBER OF COLUMNS IN A AND ROWS IN 8
                N - NUMBER OF COLUMNS IN 8 AND C
C
Ç
      OUTPUT
               CALLING SEQUENCE
Ċ
               C - RESULTANT MATRIX
C
      SUBFCUTINES
C
      CALLED
              CMAB
      DISCUSSION MMULT CALLS CMAB TO CALCULATE (C) = (A) (B)
C *** ***
      DIMENSION A(L.MI.B(M.N).C(L.N)
      CALL CMAP(B,A,C,N,M,L)
      FETURN
      FND
```

```
SUBROUTINE PANUNI(ART, RO, Y, X)
C *****
C
      SUPRCUTINE PANUNI (ART, RO, Y, X)
Ċ
Ç
      PURPOSE
               TO TRANSFORM POINT COORDINATES FROM THE LOCAL PANEL
C
               SYSTEM TO THE UNIVERSAL SYSTEM
C
٢,
               CALLING SEQUENCE
      INPUT
C
               ART - LOCAL TO GLOBAL PANEL SYSTEM TRANSFORMATION MATRIX
C
                   - X,Y,Z COOPDINATES OF PAMEL CENTER (UNIVERSAL)
                   - X,Y,Z COORDINATES OF POINT TO BE TRANSFORMED/LOCAL)
               CALLING SEQUENCE
      DUTPLT
                  - X,Y,Z COORDINATES OF TRANSFORMED POINT (UNIVERSAL)
C
      SUBRICUTINES
     CALLED
               MMULT
C
C
      DISCUSSION THE LOCAL PANEL COOPDINATES ARE MULTIPLIED BY THE
               MATRIX ART IN SUBPOUTINE MAULT TO PRODUCE THE GLOBAL
C
C
               PANEL COORDINATES WHICH, WHEN ADDED TO THE UNIVERSAL
               PANEL CENTER, PRODUCE THE UNIVERSAL COORDINATES.
( ****
      DIMENSION ART(3,3),RO(3),X(3),Y(3),W(3)
      CALL MMULT(ART, Y.W.3.3.1)
      DO 10 I=1,3
10
      X(I)=W(I)+PO(I)
      PETURN
      FND
```

```
SUBROUTINE PDSEQS(A.NR.N.DN.B.M.D1)
C
      SUBPCUTINE POSEOS (A,NP,N,DN,B,M,DI)
C
r
                TO SOLVE A SYSTEM OF EQUATIONS A*X = B. WHERE A IS A POST
      PUFPCSE
C
                -TIVE DEFINITE SYMMETRIC MATRIX. USING CHOLESKY DECOMPOSI
                -TION
                CALLING SEQUENCE
      INPUT
                A - ARRAY OF WHICH THE UPPER TRIANGLE IS THE UPPER TRIAN-
                    GLE OF A GIVEN POSITIVE DEFINITE SYMMETRIC MATRIX
C
                NE - MAXIMUM ROW DIMENSION OF ARRAYS A AND B
Ç.
C
                N - ORDER OF THE POSITIVE DEFINITE COEFFICIENT MATRIX
Ç
                B - APPAY CONSISTS OF M RIGHT-HAND SIDES OF THE LIMEAR
C
                    SYSTEM
C
                M - NUMBER OF PIGHT-HAND SIDES
Ç
C
      OUTPUT
                CALLING SEQUENCE
C
                R - SOLUTION VECTORS
                A - ARRAY OF WHICH THE UPPER TRIANGLE IS SAME AS INPUT,
                    THE LOWER TRIANGLE CONTAINS THE LOWER TRIANGULAR MAT-
C
                    RIX L FROM CHOLESKY DECOMPOSITION WITH DIACONAL ELF-
C
                    MENTS EXCLUDED
C.
                DN - THE PECIPEOCALS OF DIAGONAL ELEMENTS OF L
C
C
                         FOR SUCCESSFUL RETURN
                91 - = 1
C
                          INDICATES THAT THE GIVEN COEFFICIENT MATRIX AP-
                          PEARS NOT POSITIVE DEFINITE
C
C
C
      SUBROUTINES
      CALLED
               NONE
C
      DISCUSSION THE ROUTINE FIRST PERFORMS THE CHOLESKY DECOMPOSITION
C
                OF THE GIVEN MATRIX A INTO A LOWER TRIANGULAR MATRIX L
C
                AND ITS TRANSPOSE. IT THEN SOLVES THE GIVEN SYSTEM OF EQU
C
                -ATIONS BY BACK SUBSTITUTIONS.
C * * * * * *
      DIMENSION A(MR,1), DM(1), H(MR,1)
                              PERFORMS CHOLESKY DECOMPOSITION
      DO 20 I=1.N
      KI = I-1
      DO 20 J=I.N
      \{L+I\}\Delta = X
      IF(KI.GT.O) CALL VIPS(A(I.1).NF.A(J.1).NF.KI.X)
      JE(J.NF.I) GO TO 10
      IF(X.LE.A.) GO TO 80
      DN(T) = 1./SORT(X)
      00 TO 20
   I \cap A(J_*I) = X*DN(I)
   20 CONTINUE
      01 = 1.
                              BACK SUBSTITUTIONS
C
      NM1 = N - 1
```

```
DO 60 J=1.M
   B(1,J) = B(1,J)*DN(1)
   TF(N.EQ.1) GD TD 40
   DO 30 T=2.N
   Y = B(I,J)
   CALL VIPS(A(I,1),NR,8(1,J),1,I-1,Y)
   P(I,J) = Y \neq DN(I)
   IF(N.EQ.1) GO TO 60
30 CONTINUE
40 B(N,J) = B(N,J)*DN(N)
   00 50 IN=1, NM1.
   I = N - IN
   Y = B(I,J)
   I1 = I+1
   CALL VIPS(A(II.I),1,B(II,J),1,IN,Y)
   B(I,J) = Y*DN(I)
50 CONTINUE
60 CONTINUE
70 RETURN
80 D1 = 0.
  GO TC 70
   FND
```

```
SUBROUTINE PTRMS (IP)
( *****
      SUBPCUTINE PTRNS (IP)
(.
C
C
      PURPOSE TO READ PANEL INFORMATION FROM DISK
               CALLING SEQUENCE
      INPUT
                IP - PANEL NUMBER OF INFORMATION TO BE READ
C
                COMMON BLOCK
(
                /PINDX/ - KO.NPRD
C
C.
      CUTPUT
               COMMON BLOCK
                /PANDQ/ - CP.PC.RC.AR, AFT.P.A.B.DIAM, C.AST. IIS. INS. ITS.
                /PINDX/ - KQ
C
      SUBROUTINES
C
      CALLED
               NONE
      DISCUSSION FEADS 197 WORDS OF PANEL INFORMATION FROM DISK FILE
                SPECIFIED BY NPRD INTO COMMON BLOCK PANDO.
Ç
· *****
C
C
          READS PANEL INFORMATION FROM DISK
C
      COMMEN /PANDO/ PDG(1971, NPDQ
      COMMON /PINCX/ KDUM, KP, NDUM, NPAN
C
      ID = IP - KP
      IF (ID) 200,300,100
 100
      IBRANCH = ID
      GO TC 250
 200
      IBGANCH = IP
      PEWIND NPAN
 250
      IF (IBRANCH .EQ. 1) GD TO 290
      MAX = IBRANCH - 1
      PO 275 T=1, MAX
 275
      READ (NPAN)
                    PDQ(1)
 290
      PEAD (NPAN)
      KP = IP
 300
      RETURN
      END
```

SUBROUTINE TOECOM(A,NR,N,V,IPP,D1) (****** C SURFCUTINE TOECOM (A.NF.N.V.IPR.D1) • Ç **FUFPCSE** TO DECOMPOSE A SQUARE MATRIX INTO LOWER AND UPPER TRIAN-C GULAR MATRICES WITH PARTIAL PIVOTING AND ROW FOUILIBRA-C TION C INPUT CALLING SEQUENCE C A - ARRAY CONSISTS OF FLEMENTS OF A GIVEN MATRIX C NR - MAXIMUM FOW DIMENSION OF ARPAY A N - ORDER OF THE GIVEN MATRIX V - SCRATCH ARRAY, MAY BE SAME ARRAY AS IPR TO SAVE STOR ſ -AGE C (GUTPLT CALLING SEQUENCE C A - THE LOWER TRIANGLE OF THE AFRAY CONSISTS OF A LOWER TRIANGULAR MATRIX L AND THE UPPER TRIANGLE CONSISTS OF AN UPPER TRIANGULAR MATRIX U (SINCE U IS UNIT UP-PFF TRIANGULAR, ITS DIAGONAL ELEMENTS ARE NOT STORED) IPP - ARRAY GIVES NUMBERS OF PIVOTAL ROW (A RECORD OF IN-TERCHANGES) D1 - = +1 OF -1 ACCORDING AS THE NUMBER OF INTERCHANGES IS EVEN OR ODD. IT ALSO INDICATES SUCCESSFUL DECOM-C **POSITION** = 0 INDICATES THAT THE GIVEN MATRIX APPEARS SINGULAR C SUBPOUTINES C CALLED VIP.VIPS C C DISCUSSION THE FOUTINE PEPEOFMS THE CPOUT FACTORIZATION OF A GIV-C EN MATRIX WITH PARTIAL PIVOTING AND ROW EQUILIBRATION. THE UPPER AND LOWER TRIANGULAR MATRICES RESULTED FROM THE C C DECOMPOSITION ARE STORED IN THE ARRAY A WHICH ORIGINALLY C CONSISTS ELEMENTS OF THE GIVEN MATRIX. IF ONE OF THE PI-C VOTS APPEARS TO BE TOO SMALL. DI IS SET TO ZERO AND AN C ERROR EXIT IS TAKEN. C THIS ROUTINE IS A MODIFIED VERSION OF A ROUTINE IN THE \mathbf{C} SUBPOUTINE LIBRARY OF THE BOEING COMPUTER SERVICES CO. C ***** DIMENSION A(NR,1),V(1),IPP(1) DATA EPS/16407777777777777768/ E8=8. * EPS CALCULATES LENGTH OF ROW VECTORS DO 10 I=1.N CALL VIP(A(I,1),NR,A(I,1),NR,N,Y) IF(Y.LE.O.) GO TO 70 10 V(I)=1./SQRT(Y) C PERFORMS THE DECOMPOSITION 0.1 = 1.DO 50 K=1,N L=K

```
X=?.
       K1=K-1
       00 20 I=K.N
       Y = \Delta(1,K)
       IF(K1.GT.0) CALL VIPS(A(1,1),NF,A(1,K),1,K1,Y)
       \Delta(T,K) = Y
       V = \Delta B S (Y * V([]))
       IF(Y.LE.X) GO TO 20
       X = Y
      [ = [
   20 CONTINUE
       IF(L.EQ.K) GO TO 35
       D1 = -D1
       DO 30 J=1.N
       \lambda = V(K^*J)
       \alpha(k, J) = A(L, J)
   30 \Delta(1,J)=Y
       V(L) = V(K)
   35 [PR[K]=L
0
                                  CHECKS IF THE PIVOT IS TOO SMALL
       IF(X.LT.E8) GO TO 70
       X = 1./\Delta(K.K)
       J=K+1
   40 IF(J.GT.N) GO TO 50
       Y = \Delta(X,J)
       TF(K1.GT.O) CALL VIPS(A(K.1), NP, A(1, J), 1.K1, Y)
       \Delta(K,J) = X*Y
       J=J+1
       GO TO 40
   50 CONTINUE
   60 PETURN
   70 D1 = 0.
       50 TC 60
       END
```

```
SUBFCUTINE TRANS(A.AT, M.N.)
C *****
C
      SUPECUTINE TRANS (A, AT, M, N)
ŗ
C
               TO FORM THE TRANSPOSE OF A MATRIX A AND STORE
      PURPOSE
Ç
                THE RESULT IN A MATRIX B
C
7
                CALLING SEQUENCE
      INPUT
Ü
                4 - ARRAY CONTAINING MATRIX ELEMENTS TO BE TRANSPOSED
(
                M - NUMBER OF FOWS IN A AND COLUMNS IN B
C
                N - NUMBER OF COLUMNS IN A AND POWS IN B
      CUTPUT
                CALLING SEQUENCE
C
                AT - APRAY CONTAINING ELEMENTS OF THE TRANSPOSE OF
•
                     THE GIVEN MATRIX
ŗ
Ċ
      SUBFOUTINES
C
      CALLED
              NONE
Ċ
      DISCUSSION AT(J,I) IS SET TO A(I,J) AS I VARIES FROM I TO M AND
C
                   J VARIES FROM 1 TO N.
(****
      DIMENSION A(M,N), AT(N,M)
      DO 100 I=1, M
      DO 50 J=1,N
      (L, I)\Delta = (I, L)T\Delta
 50
      CONTINUE
 100
      CONTINUE
      RETURN
      END
```

```
SURFCUTINE TENSER (X,Y,N)
C
      SUPPCUTINE TENSER (X,Y,N)
Ç.
Ċ.
      PUFPESE
               TO MOVE A NUMBER OF ELEMENTS FROM ONE APPAY TO ANOTHER
C
                CALLING SEQUENCE
(
      INPUT
                X - LOCATION OF THE FIRST ARRAY ELEMENT TO BE MOVED
                N - NUMBER OF ELEMENTS TO BE MOVED
ŗ
      GUTPUT
                CALLING SEQUENCE
C
                Y - ARRAY OF FLEMENTS IDENTICAL TO THE FIRST N FLEMENTS
€.
                    IN ARFAY X
C
      SUBPICUTINES.
C
      CALLED NONE
C
      DISCUSSION Y(I) IS SET TO X(I) AS I VARIES FROM 1 TO N.
C *****
      DIMENSION X(N), Y(N)
      00 100 I=1,N
  100 Y(1) = X(1)
      RETURN
      END
```

```
SUPPCUTINE UNIPAN(AR. PC. X.Y)
      SUBROUTINE UNIPAN (AR. PO.X.Y)
C
C
               TO TRANSFORM POINT COORDINATES FROM THE UNIVERSAL
€
      PHEPESE
Ü
                SYSTEM TO THE LOCAL PANEL SYSTEM
C
                CALLING SEQUENCE
      INPUT
                AP - GLOBAL TO LOCAL PANEL SYSTEM TRANSFORMATION MATRIX
C
                RO- X,Y,Z COOPDINATES OF PANEL CENTER (UNIVERSAL)
C
C
                X - X.Y.Z COOPDINATES OF POINT TO BE TRANSFORMED
€.
                    (UNIVERSAL)
C
C
      CUTPUT
                CALLING SEQUENCE
C
                Y - X.Y.Z COORDINATES OF TRANSFORMED POINT (LOCAL)
C
      SUBFOUTINES
Ç
      CALLED
               MMULT
C
      DISCUSSION THE COORDINATES OF THE PANEL CENTER ARE SUBTRACTED
C
                FROM THE COOPDINATES OF THE POINT TO BE TRANSFORMED. THIS
C
C
                GLOBAL APRAY IS THEN MULTIPLIED BY THE MATRIX AP USING
                SUBPOUTINE MMULT TO PRODUCE THE LOCAL PANEL COGRDINATES.
C
C ****
      DIMENSION AR(3,3), RO(3), X(3), Y(3), W(3)
      00 10 1=1.3
 10
      W(I) = X(I) - PO(I)
      CALL MMULT(AR, W, Y, 3, 3, 1)
      FETURN
      END
```

```
SUPECUTINE UVECT(A)
C ****
Ũ
       SUBFOUTINE UVECT (A)
C
C
       PUPPESE
               TO CALCULATE THE DIRECTION COSINES OF A VECTOR
C
Ċ
       IMPUT
                CALLING SEQUENCE
C.
                 A - DIRECTION NUMBERS OF A VECTOR
С
                CALLING SEQUENCE
      PUTPUT
C
                 A - DIRECTION COSTNES OF A VECTOR
C
C
       SUBREUTINES
Ç
      CALLED
               NONE
C
      DISCUSSION UVECT PEFFORMS THE FOLLOWING CALCULATIONS-
                  A(1) / SQFT(A(1)*A(1)+A(2)*A(2)+A(3)*A(3)) .WHERE
C
C
                    I VARIES FROM 1 TO 3.
( *****
       DIMENSION A(3)
       7 = SOFT(\Delta(1) **2+\Delta(2) **2+\Delta(3) **2)
       DO 10 I=1.3
 10
       \Delta(I) = \Delta(I)/Z
       RETURN
       END
```

```
IDENT
                 VIP
                        (A.INCA.B.INCB.N.C)
* * * * * * * *
¢
      SUBREUTINE VIP (A, INCA, B, INCB, N, C)
                  VIPA (A.INCA.R.INCE.N.C)
                  VIPS (A.INCA.B.INCB.N.C)
      PURPOSE
               TO PERFORM VECTOR INNER PRODUCT CALCULATION (VIP) AND TO
                ADD (VIPA) TO OR SUBTRACT (VIPS) FROM AN INCOMING VALUE
                (COMPASS)
      INPUT
               CALLING SEQUENCE
                A - VECTOR A
                INCA - INCREMENT BETWEEN SUCCESSIVE ELEMENTS OF A
                B - VECTOR B
                INCB - INCREMENT BETWEEN SUCCESSIVE ELEMENTS OF B
                N - NUMBER OF ELEMENTS TO BE MULTIPLIED
                C - AN INCOMING VALUE TO BE ADDED TO (VIPA) OF TO SE SUB-
                    TRACTED FROM (VIPS)
      CUTPUT
               CALLING SEQUENCE
                C + RESULT C = A.S (VIP), C = C + A.B (VIPA), AND
                    C = C - A.B. (VIPS)
      SUBFICUTINES
      CALLED
               NONE
                 THE INNER PRODUCT OF TWO VECTORS A AND B IS CALCULATED
      DISCUSSION
                AND STORED IN C (VIP). THE RESULT IS ADDED TO (VIPA) OR
                SUBTRACTED FROM (VIPS) AN INCOMING VALUE CHAND THE SUM OF
                THE DIFFERENCE IS STORED BACK IN C.
                   THIS ROUTINE IS A MODIFIED VERSION OF A COMPASS ROUT-
                INE IN THE SUPPOUTINE LIBRARY OF THE BORING COMPUTER SEF-
                VICES CO.
*****
                     VIP, VIPA, VIPS
          ENTRY
          VFD
                     36/OHVIPA, 24/6
VIPA
          ESSZ
                     1
          544
                     FIDVA
                                     FETCH TRANSFER
          SAI
                     81
                                     FETCH PRE-CP
          ZF
                     80,GD
          VEC
                     36/0HVIPS, 24/6
VIPS
          85 SZ
                     1
          SA4
                     ENDVS
                                     FETCH TRANSFER
                                     FETCH PRE-OP
          SA1
                     Bl
                     80.60
          ZP
          VED
                     35/9HVIP,24/6
          BSSZ
VIP
                     1
          SA4
                     FNDV
                                    FETCH TRANSFER
          SAI
                     81
                                     FETCH PRE-CP
                                     FETCH POST-OP
CO
          542
                     33
```

PY.7

IXO

X4 XQ-X0 PUT TRANSFER IN X7

CLEAP PRODUCT REGISTER

```
5×6
                      BC
                                       CLEAP SUMMING REGISTER
          SA7
                      THRU
                                       STORE TRANSFER
           543
                      B2
                                 .GET INCA IN X3
           544
                      94
                                 .GET INCB IN X4
                                       GET N IN X5
           SA5
                      85
           S82
                      X 3
                                 .PUT INCA IN B2
           584
                      X.4
                                 .PUT INCB IN B4
           SB5
                      X 5
                                       PUT N IN B5
                                       CLEAR FOR FIFST ADD OF X6+Y7
          S×7
                       30
                                       GET 2 FOR DECP N.
           587
                       80+2
          SYC
                      80+1
                                       MASK TO DETERMINE ODD/EVEN
          BX0
                       X0*X5
                                       MASK LOWER BIT
          7.9
                       MAVA. CX
                                       IF EVEN, BY PASS ADD ELEM SETUP
                                       ODD. DO FIRST ELEMENT
          FXO
                       X1*X2
                                       DECR N
          535
                      85-1
          70
                      35, DUNE
                                       IF N=1.DONE
          FX5
                       X0+X6
                                       ADD FIRST TERM IN DOD CASE
           SAI
                       A1+82
                                       GET NEXT ELEM OF PRE-OP
                                       GET NEXT ELEM OF POST-OP
                       42+84
           SA 2
                                       NORMALIZE FIRST ADD
          NY6
                       X5
EVEN
                                       GET INCA#2
          LX3
                       1
                                       GET INCB#2
          L X 4
                       1
          SB 1
                       X 3
                                       B1= 2*INCA
                                       83= 2*INCB
           533
                       X4
                                       GET 2ND FLEM OF PRE-OP
          SA3
                       41+B2
                                       GET 2ND ELEM OF POST-OP
          SA4
                       42+84
           SB 2
                       81
                                       82= 2 * I MC A
           584
                       23
                                       84= 2*INCR
          ZP
                       BO.START
OVER
          S ± 1
                      41+82
                                 .LOAD PRE-OP
          RX5
                                       SUM FIRST MULTIPLY
                       X0+X6
                                 .LCAD POST-OP
          SA2
                      A2+84
                                       LOAD 2ND PRE-OP
          SA3
                       43+B2
                                       NORMALIZE FIRST ADD
          1.×6
                       X 5
          SA4
                       A4+B4
                                       LOAD 2ND POST-OP
STAFT
          SB5
                      85-87
                                       DECREMENT N
                                       SUM 2ND MPY (DUMMY FIRST TIME)
          ₽X5
                       X6+X7
          \bigcirc X \bigcirc
                       X1*X2
                                       FIRST MULTIPLY
          9 X 7
                                       SECOND MULTIPLY
                       X3*X4
          1.X6
                       X 5
                                       NORMALIZE SECOND ADD
          ٧7
                      B5, OVER
                                       DONE WHEN N=C
DONE
                                       FINAL ADD - FIRST MPY
          PX5
                       X0+¥6
                       X5
                                       MORM
          NX6
                                       FINAL ADD - 2ND MPY(IF N=1, X7=0.)
                       X7+X6
          2 X 5
                                       MROA
          NX6
                       Y 5
THPU
          BSSZ
                                       STUFFED WITH A TRANSFER
                      1
CUTVA
                                       FETCH C
          541
                      86
          PX7
                                       ADD C
                      X1+X6
          NX6
                      X 7
                                       STOFE
          S46
                      85
          7 P
                      BO, VIPA
OUTVS
          SAI
                      B5
```

	PX7	x1-X6	SUB	INNER	PRODUCT
	NX6	X 7			
	SA6	86			
	ZR	BO, VIPS			
ENDVA	7 P	BO∙OUTV∆			
ENDVS	ZP	RO, OUTVS			
EΝÜΛ	642	86			
	ZR	BO, VIP			
	END				

```
ZERO
                               (\Delta, N)
           IDENT
* * * * * * * *
      SUBFCUTINE ZERD (A.N.)
*
*
                TO SET THE ELEMENTS OF AN APPAY TO ZERO (COMPASS)
*
      PUPPOSE
      INPUT
                CALLING SEQUENCE
                A - LOCATION OF FIRST ELEMENT TO BE SET TO ZERO
                N - NUMBER OF ELEMENTS TO BE SET TO ZERO
*
                CALLING SEQUENCE
      OUTPUT
                A - ARRAY OF ZERO ELEMENTS
      SUBROUTINES
      CALLED
                NONE
      DISCUSSION
                   A(I) IS SET TO ZERO AS I VARIES FROM 1 TO N.
*****
           VED
                      36/OHZERO, 24/6
           ENTRY
                      ZERO
           BSSZ
 ZERO
                      1
                      B 2
           SA2
                      X2
           584
           SP3
                      BO.
           SB 5
                      1
           SX6
                      BO.
CYCLE
           546
                      81 + 33
           SB 3
                      83+85
                      83,84,CYCLE
           LT
```

Boeing Commercial Airplane Company P.O. Box 3707 Seattle, Washington 98124 September 24, 1975

EQ

END

ZERO

APPENDIX

ENGINEERING AND PROGRAM VARIABLES

Engineering variable	Description	Program variable	Reference program or subroutine
a	Parameter of Smith's conical solution	Α	SHEGEN
A _{kj}	Aerodynamic influence coefficient	DVDFS	VINFCC
[B]	Matrix defined by eq. (42) of Engineering Document	VS	VINFCC
c _m	Pitching moment coefficient	CM	OUTPUT
c _N	Normal force coefficient	CN	OUTPUT
^c P	Pressure coefficient	CPU,CPL	OUTPUT
$\Delta c_{ extbf{P}}$	Jump in pressure coefficient	DCP	OUTPUT
[c]	Matrix for coefficients of quadratic doublet distribution on a panel, defined by eq. (23) of Engineering Document	AST	SING
[D]	Matrix, defined by eq. (19) of Engineering Document	DVDV	PIVC
(DK)	Matrix, defined by eq. (40) of Engineering Document	DVDS	PIVC
E	Function, see eq. (46) of Engineering Document	EMUE, EMU	FGCAL
f(i)	Vector, defined by eq. (52) of Engineering Document	RX	ITFLOW
F	Function, see eq. (46) of Engineering Document	FVZ	FGCAL
G	Function, see eq. (46) of Engineering Document	GVZ	FGCAL
J	Jacobian	AJ	ITFLOW

Engineering variable	Description	Program variable	Reference program or subroutine
[K]	Matrix, defined by eq. (37) of Engineering Document	DVS	PIVC
l _{i'm}	Chord length of panel segment in transverse geometry cut	ZL	INPUT
M	Number of panels on one-half of configuration	NPANT	INPUT
N	Number of doublet parameters in neighborhood of panel	INS	SING
иD	Number of doublet parameters on one-half of configuration	NSNGT	TSING
N _{FS}	Number of free sheet panels on one-half of the configuration	NP(2)	INPUT
$N_{f W}$	One-half of the number of wing panels	NP (1)	INPUT
P_{ij}	Panel corner point	CP	GEOMC
$P_{\mathbf{o_{ij}}}$	Panel center	PC	SURFIT
$Q(\xi,\eta)$	Position of elementary doublet	ZPK	SING
S(X)	Local wing semispan	YLE	INPUT
S	Panel area	SP	OUTPUT
$s_{f w}$	Wing area	sw	OUTPUT
Ū∞	Freestream velocity	FSV	INPUT
\vec{v}	Velocity	VEL VG	OUTPUT FGCAL
$ec{ m V}^{ m s}$	Average sheet velocity	VEL VG	OUTPUT FGCAL
$X_{\mathbf{P}}$	Pitch axis	XPITCH	INPUT

Engineering variable	Description	Program variable	Reference program or subroutine
α	Angle of attack	ALPHA	INPUT
$ar{m{\gamma}}$	Constant in quasi-Newton method	GAMA	ITFLOW
$\vec{\sigma}$	Vorticity -	Z	OUTPUT
L	Strength of line vortex along terminated edge	TSC(1)	OUTPUT
δ ⁽ⁱ⁾	Scaling parameter	CALFA	ITFLOW
θ	Panel inclination in transverse cut	ZA	INPUT
μ _e	Doublet parameters along edges of networks	S(1), S(NEQ)	FGCAL
μ _r	Doublet parameters not located along edges of networks	S(NEQ+1), . S(NSNGT)	FGCAL
$\mu_{\mathbf{j}}$	Doublet parameters on one-half of configuration	S	TEA378 FGCAL OUTPUT

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